Application of Systems Engineering Methods to Traffic Forecasting

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Systems engineering techniques can be used in predicting trip distributions in urban road networks. To deal quantitatively with the interaction of components, each component must be describable mathematically and must be incorporated into the system in accordance with the re quirements of linear graph theory. If the traffic system components can be identified, the traffic problem can be solved.

This paper discusses the principles of linear graph theory and the general requirements for using these methods. The most significant contribution comes from applymg these techmques to traffic interchange. By using a hypothetical community, the techniques of systems engineermg are compared with the gravity model and the electrostatic model for predicting the distribution of work trips.

• TH E WORK described in this paper shows the application of systems engineering techniques to a traffic distribution problem. This method is a rigorous technique for computing the system of traffic flow in a road network. Precise and balancing results **are obtained in one step by this method. Systems engineering techniques thus offer an extremely powerful tool for the analysis of systems when the system components and their measurements ar e adequately defined. This technique will be even more powerful when a computer solution for the routme matrix evaluation becomes available. It I S excepted that this technique will not only be refined for application to traffi c flow computation but will also be used for the analysis of other traffic engineermg system problems.**

BACKGROUND

The trend in the many studies of traffic engineering is toward a more mathematical and theoretical approach. This fact is evidenced by the writings of Herman, Schneider, Howe, Bevis, and others. One has only to refer to the bibliography of the special re**port by Haight** *(1)* **to conclude that traffic engineering is on the verge of a breakthrough. In spite of the as yet uncontrollable element of human choice or behavior, many phases of the traffi c problem will evolve to a scientific level comparable to that of the physical sciences. The traffic engmeermg profession will probably have to settle for somewhat** less replicability than the physical sciences because only two of their ingredients are **physical, the vehicle and the facility, whereas the third, the user, presents different and still unsolved problems. This does not imply that the user problem is insur mountable. Although the individual has shown immumty to prediction, groups of many such individuals have shown that patterns can be observed.**

Evolution has come to the other sciences by a slow but orderly progression. First, trial and error techniques were used and the effects were noted. The practitioner, who was faced with a series of difficult tasks, slowly added to his store of engineering **judgment, and this he utilized on future problems as they developed. This was followed by a concentrated effort to collect and evaluate data. Analysis of data in the field of traffic flow has shown that groups of people are predictable and that mathematical form ulas can be developed to express various travel habits and patterns. In the last stage of this evolution, the theory is established. In other fields, new theories have been developed by building on the terminology and theories defined previously and by critical-** Iv analyzing the work of others in order to find a more direct approach.

So far the traffic theorists have concentrated their work on car-following theory, queuing and waiting line theory, and traffic simulation. Some work dealing with techniques such as the gravity model, the opportunity model and linear programing has been done in the area of theoretical origin and destination studies.

The work reported in this paper deals with development of a methodology for solving traffic flow in a road network by a mathematical model. The necessary preliminary theoretical testing of systems analysis as a technique for theoretical origin and destination studies has been accomplished during the study, but many simplifying assumptions were necessarily made. The theoretical results obtained with this technique are shown to compare encouragingly well with those available with other techniques. In the analysis of systems as a means for achieving a simple systematic procedure for formulating the system equations, the theory of oriented linear graphs, developed as an abstract mathematical topic, is valuable. Because the work with this technique is in its early stages, primary attention in this paper is given to the network description and only secondary **primarish primarily primarily** consideration to the characteristics of the basic data.

The next step in the continuing research under way at Michigan State University will utilize these established concepts of systems engineering for predicting traffic flow in actual urban road networks. **actual urban road networks.**

SYSTEMS ENGINEERING THEORY

The techniques presented here have sometimes been referred to as "linear graph theory" and "network topology." Thes e terms can be used interchangeably (2). A system can be defined as an orderly arrangement of mterrelated elements acting together to achieve a specific purpose. Thus a system must have an avowed purpose, be free of extraneous or mathematically redundant parts, and have the elements or com**ponents joined in an orderly fashion. Discussion here is limited to systems made up of components havmg only two terminals, although there is no limit on the number of termmals the component may have m general systems theory.**

For the computation of the system characteristics two steps are necessary:

1. To establish a mathematical model of the relevant physical characteristic s of the system components expressed in terms of measurements.

2. To establish in mathematical form and in terms of measurements from a knowledge of the component characteristic s and their mode of interconnection, the character istics of the system; i.e., a mathematical model of the system.

Components are described mathematically by relating two measurements of the component in "isolation" from other components. (Fo r a more detailed explanation see Appendix.) These measurements must be such that one is a "through" (or series) mea**surement called y, which when summed at each vertex must equal zero, and the other IS an "across" (or parallel) measurement called x, which when summed around each circuit must equal zero. The relationship between measurements x and y is expressed mathematically and called the terminal equation of the component. The component is represented by an oriented line segment called the component terminal graph. The collection of component termmal graphs obtained by joining the vertices of each terminal graph in a one-to-one correspondence with the union of the physical components is called a system graph.**

A "tree" is selected and the elements of the system graph ar e classified into either branches of the tree or chords. The "vertex postulate" or the "circuit postulate" is then applied to the system graph to establish the graph equations. The graph equations along with the terminal equations of the system components are defined as the system equations. The system equations represent a complete mathematical description of the system. Thes e simultaneous equations are independent and can now be solved.

APPLYIN G TECHNIQUE S TO TRAFFI C FLO W COMPUTATION

Although the techniques of system analysis were developed primarily in electrical network analysis, during the past several year s this fundamental discipline of analysis has been applied usefully to many other areas, such as mechamcal, hydraulic, and heat-transfer systems. Predictmg traffic flow in an urban network also seems amenable to this techmque, if the characteristic s of the traffic problem can be defined in the form of suitable components and measurements which can be assembled into workable system graphs. The following discussion demonstrates how systems analysis can be applied to the traffic problem.

The selection of the units that will serve as components depends first on what type of system is being analyzed (i.e. , transportation, sewage treatment, electrical, etc.), and second, on the specific question to be answered by the analysis of the system. For example, in the study of mass transit, the definition of components and measure**ments for a study of the system of servic e areas would probably be different than the definitions for a study of the effect of street capacities on the system.**

In selecting the components for the system analysis of traffic flow in a road network it seemed at first feasible to consider the user , the vehicle, and the facility. "User" can be defined as one individual. An individual moves from place to place and this movement could be defined as flow or "through" variable (y). This movement or flow IS related to a desire or "pressure" which can serve as the across variable (x). However, analyzing traffic flow on the basis of the individual user would lead to systems far too voluminous and too difficult to evaluate. Considering the vehicle as a basic component, a y measurement could be assigned to flow, but the x variable as desire or pressure is meaningless for a vehicle.

The dwelling unit and the family are the next possible basic components inasmuch as they combine the user and the vehicle. Both will afford the same x and y measure ments as suggested for the individual. But even for the smaller urban areas, the **number of dwelling units and families involved in the system would still be too large to provide a workable model, so that it will be more desirable to use even larger units, such as zones.**

A zone, similar or identical to those used in origin and destination surveys, seems to be the best component evaluated to date. Thes e zones should be defined so that the traffic characteristic s within the zones are as homogeneous as possible. It is now assumed that the traffic characteristic s of the entire zone can be computed from a limited number of parameters. For example, given a homogeneous residential zone **contaming a certain number of dwelling units or families and with known parameters such as residential density, income level, and car ownership, one should then be able** to establish some value that would express the desire or pressure of that zone to generate a number of trips for a specific purpose. This pressure to make the trips from **the given residential area to, say, the central business district (CBD) must be large enough to overcome the resistances against making these trips. The resistance is generated by the previous experience of traveling to the CBD , of parking difficulty and general congestion while in the CBD , and of returning home. If the pressur e is not sufficient the trips will not be made. The number of trips that will be made is a function of pressur e and resistance.**

Research thus far has indicated that in the theoretical computation of traffic flow the classification of trip generation by trip purpose is essential. The percentage of trips assignable to each purpose seems well established. Further studies beyond those cited in the references (3) have proved that there are only very small variations in the per centages within classe s of trips according to purpose. Accordingly, if it is assumed that in computing, say, shopping trips from a zone, one of the following three values can be determined from parameters, estimates, or in some other way:

1. Actual flow of shopping trips out of the zone in a given time period: y (t) or

2. Demand or pressure for such shopping trips to be made from the zone: $x(t)$ or

3. Relationship between demand and flow; i . e., the function relating x and y: $x = f(y(t))$ or $y = f(x(t))$,

then to solve the distribution problem of the trips generated in the zones, parts of the street network also must be defined as components with measurements suitable for systems analysis. In the preliminary stages only major arterials have been considered. Later developments might prove that, between any two zones, each group of streets of **a specific type should be defined as a component with certam characteristics. Also, is a specific type should be defined as a component with certain characteristics. Also iments could reflect such items as posted speed limit, parking, abutting land use, etc.**

In the example to be discussed in the next section, simplifications are made. All **routes between two zones are represented by two street components, one for each direction. No attempt was made to determme an x or y measurement, but rather an R value is used where** $x = Ry$ **.** In this equation R represents a parameter that is the **mathematical relationship between x and y. It defines the relationship between flow and desire and might be visualized as a function of resistance or friction. The best physical measurement to be used as a basis for R was determmed, at this stage only on an empirical basis, to be travel time. Preliminary work has led to a group of curves where the value R is a function of travel time and dependent on trip purpose** (Fig. 1). Each street is assumed to be one-way for proper orientation of the terminal **graph. The streets may also be viewed as two-way, but then each direction is repre sented as a separate component. The curve used has been obtained by substitution of a** resistance scale and plotting the "frequency of trips" table as reported by Carroll (4). Further examination of travel time vs trip purpose as indicated in some of the recent **comprehensive studies should reveal a stronger correlation than the curves presently used. This point, as well as many others, will require considerable research.**

Other possible components of the system are shopping areas, work or employment centers, the CBD , recreational areas, and others. Once agam the component must be described mathematically by x or y, or by some relationship between x and y. Early **trials have been limited to representing work trips to shoppmg areas and industrial areas, where a flow y has been estimated on the basis of number of employees. Other measure s of an area's attraction will be considered m future research. A possible relationship might come from comparing the specific area with some accepted standard area , just as a resistor is calibrated by comparing it with some standard. This type of approach is simila r to McGrath's work m New Haven, where trip attraction based on an effective acr e is established as a standard (5). Other possible component measure ments will be tried as the research progresses.**

SAMPLE PROBLEM

A s an example, a small hypothetical commumty where an origin and destmation survey is not available is assumed. The specific problem to be solved here by means of linear graph theory is one of determining the distribution of work trips from each residential zone to each employment zone. Initially, the community is separated into residential zones and zones of employment. The labor force of each nearly homogeneous residential zone might be determined from planning studies or from records of the local Chamber of Commerce . Work trips might be approximated by a correlation equation using driving time to the CBD and an estimate of car ownership. The number of auto driver trips could then be estimated from an average car occupancy value. The number **of auto drive r work trips arriving at each employment zone could be established by some simila r procedure or by a sampling of the known number of employees in that zone. An estimate of auto driving time between every pair of zones in question could be prepared by actual observation or from a travel time map. The validity of this approach is not the concern of this paper.**

Regardless of the techniques use, it may be assumed that the following information has been obtained concerning the small hypothetical community. There are four residential zones with a specified number of auto driver work trips as given in Table 1. The number of work trips that arrive at each of the three employment zones is also **given in Table 1. The number of trips destined for employment zone 7 (Element 1) is not defined, although it is clear that 3,000 trips must be destined for this zone unless there is an unbalance in the work trip generation vs attraction. The number has been**

 $\overline{1}$

TABL E 1

AUTO DRIVER WORK TRIPS TO AND FROM ZONES

Element	Zone	From	Tо		
26	$Res-1$	4,000			
27	$Res-2$	3.000			
28	$Emp-4$		3,000		
29	$Emp-5$		5,000		
30	$Res-3$	2.000			
31	$Res-6$	2,000			
1	$Emp-7$,		

TRAVEL TIMES BETWEEN ZONES IN MINUTES

	28	29	Zones		
10	10	14	26		
17	14	10	27		
10	17	14	30		
14	20	10	31		

Figure 1. Travel time resistance for **wor k trips.**

left open in the table because the method of solution requires that this number be computed. The correct answer serves as a check on the computation.

The estimated travel times between the centroids of each zone are given in Table 2. **The element number given for each zone is the number used for identification in the following analysis procedure.**

The flow of trips completes a cycle in one day. Thus the time for which this analysis is made is a 24-hr period. Trips to work and trips home are identical in number but **occur on different route components during different times of the day. The trips emanating from one zone also return to that zone during the study period.**

Component Representation

Each zone is represented as a component part of the urban network and its measure**ments are shown in Figure 2.**

Eac h residential zone, employment zone, and the system of routes that connect these zones can similarly be illustrated as components. Each component is represented **as an oriented line segment which is referred to as the terminal graph of the component.** For example, in Figure 2, a residential zone is shown schematically and as a terminal **graph.**

System Graph

With these components, the system graph can now be drawn in accordance with the following rules:

1. Components are joined in the system graph according to the manner in which the components ar e combined in the physical system.

2. The direction of flow is indicated by the direction of the Ime representing the components.

3. A "tree" is selected. This tree is a subgraph of the system graph containing a ll vertexes but no circuits. The tree is used in formulatmg the systems equations.

4. Specified desire (x values) are placed in the branches of the tree (B-1) (there are no specified x values here).

5. Specified flow (y values) are placed in the chord set, (C-2).

Figur e 3a shows the system graph and how it is built; Figur e 3b shows the tree chosen for this example. A tabulation of the values used as given measurements for the establishment and solution of this system is given in Table 3. In the matrix solution shown later, only R and y are

Figure 2. Component representation.

used. The other parameters are given only for information. The relation between travel time and R was discussed and shown earlier in Figure 1.

Circuit Equations

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T he numerical solution of the system requires the writmg of a set of equations (m matrix form) which is done here m accordance with the circuit postulate of linear graph theory.

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1. In accordance with the circuit postulate, the general equation for the kth circuit **i s:** \mathbf{a}

$$
\sum_{j=1}^{ } b_j x_j = 0
$$

in which

 $b_1 = 0$ if the jth element is not included in the kth circuit;

- b_1 = 1 **if the orientation of the jth element is the same as the orientation for the kth circuit;**
- **-1 if the orientation of the jth element is opposite to the orientation of the kth circuit.**

2. Eac h circuit will have one and only one chord, and the circuit equations will be written in such sequence that a unit matrix results for the entries C-1 and C-2 .

3. Equations using chords (C-1) are written first and chords (C-2) written last.

4. The x's are arranged in the column matrix in the following order X_{R-1} , X_{R-2} , X_{C-1} , and X_{C-2} .

5. The resulting matrix product is

Ţ

x l ::2 0 -1 1 _ 1 **0 0 0 0 0 0 0** *\J* **⁰ : 1 0 0 0 0 0 0 0 0 0 0 0 I ° 0 0 0 0 0 x3 0 -1 1 -1 1 -1 0 0 0 0 0 0 0 1 0 1 0 0 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 x4 0 -1 0 0 1 -1 0 0 0 0 0 0 0 1 0 0 1 0 0 0 0 0 0 0 0 0 t 0 0 0 0 0 0 x5 0 0 0 0 -1 1 -1 0 0 0 0 0 0 ' 0 0 0 1 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 x6 0 1 -1 0 -1 0 0 0 0 0 0 0 0 ' 0 0 0 0 1 0 0 0 0 0 0 0 1 0 0 0 0 0 0 x7 0 1 - i 0 -1 1 -1 0 0 0 0 0 0 ! 0 0 0 0 0 1 0 0 0 0 0 0 t 0 0 0 0 0 0 x8 0 0 0 0 0 0 0 1 -1 0 -1 0 0 ' 0 0 0 0 0 0 1 0 0 0 0 0 1 0 0 0 0 0 0 x9 0 0 0 0 0 0 0** *1* **-1 0 -1 1 -1 ' 0 0 0 0 0 0 0 1 0 0 0 0 1 0 0 0 0 0 0 xlO 0 0 0 0 0 0 0 0 0 0 -1 1 -1 ' 0 0 0 0 0 0 0 0 1 0 0 0 ' 0 0 0 0 0 0 x U 0 0 0 0 0 0 0 -1 1 -1 0 0 0 ' 0 0 0 0 0 0 0 0 0 1 0 0 ' 0 0 0 0 0 0 xl2** $= 0$ **0 0 0 0 0 0 0 -1 1 -1 1 -1 0 ' 0 0 0 0 0 0 0 0 0 0 1 0 ' 0 0 0 0 0 0 xl3 0 0 0 0 0 0 0 -1 0 0 1 -1 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 xl 4 xl 5 xl6 1 1 0 0 0 0 0 0 0 0 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 0 0 0 xl7 1 1 -1 1 0 0 0 0 0 0 1 -1 1 , 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 0 0 x24 -1 -1 1 0 0 0 0 -1 1 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 0 x25 -1 0 0 0 -1 1 0 0 0 0 -1 1 0 I 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 xl8 1 0 0 0 1 0 0 1 0 0 0 0 0 ' 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 xl 9 1 0 0 0 1 -1 1 1 -1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 ° ° 0 0 0 0 1 x20 x21 x22** $\overline{B^2}2$ $C-1$ **x23 C-2 x26 1 2345G78 9 11112211222 2 2 2 2 2 3 3 x27 45674589012 3 6 7 8 9 0 1 x28 x29 x30 x31**

General Solution of Equations in Symbolic For m

$$
\begin{bmatrix} B_{11} & B_{12} & U & 0 \ B_{21} & B_{22} & 0 & U \end{bmatrix} \begin{bmatrix} x_{B-1} \\ x_{B-2} \\ x_{C-1} \\ x_{C-2} \end{bmatrix} = 0
$$

$$
\begin{bmatrix} B_{11} \\ B_{21} \end{bmatrix} \begin{bmatrix} x_{B-1} \\ x_{B-1} \end{bmatrix} + \begin{bmatrix} B_{12} & U \\ B_{22} & 0 \end{bmatrix} \begin{bmatrix} x_{B-2} \\ x_{C-1} \end{bmatrix} + \begin{bmatrix} 0 \\ U \end{bmatrix} \begin{bmatrix} x_{C-2} \\ x_{C-2} \end{bmatrix} = 0
$$

Substituting $RY = X$ for X_{B-2} and X_{C-1} :

 $\begin{bmatrix} 11 \\ x_{B-1} \end{bmatrix}$ + $\begin{bmatrix} B_{12} & 0 \\ 0 & 0 \end{bmatrix}$ **/2I . . 22 J** \mathbb{R}_{B-2} ⁰ $\left| \int_{B-2}^{Y} \right|$ 0 R_{c-1} $\begin{bmatrix} Y_{c-1} \end{bmatrix}$ $\begin{bmatrix} v \end{bmatrix}$ $\begin{bmatrix} c^{-2} \end{bmatrix}$

One of the key advantages of this type of analysis is the possibility of replacmg certain unknown variables in an equation with a relation of known values. In the next substitution, the unknown Y_{R-2} are replaced by the known values Y_{C-2} (2).

$$
\begin{bmatrix} Y_{2-2} \\ Y_{C-1} \end{bmatrix} = \begin{bmatrix} B_{12} & B_{22} & B_{C-1} \\ 0 & 0 & C_{C-2} \end{bmatrix}
$$

which, when inserted, gives the main equation:

$$
\begin{bmatrix} B_{11} \\ B_{21} \end{bmatrix} \begin{bmatrix} x_{B-1} \\ B_{-1} \end{bmatrix} = \begin{bmatrix} B_{12} & 0 \\ B_{22} & 0 \end{bmatrix} \begin{bmatrix} R_{B-2} & 0 \\ 0 & R_{C-1} \end{bmatrix} \begin{bmatrix} B_{12} & B_{22} \\ 0 & 0 \end{bmatrix} \begin{bmatrix} Y_{C-1} \\ Y_{C-2} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \end{bmatrix} \begin{bmatrix} x_{C-2} \\ x_{C-2} \end{bmatrix} = 0
$$

In this main expression, the bottom line of equations, dealing only with known values, does not contribute to the solution. With the top equation from the preceding, the genera l mesh form or circuit equation can be written:

$$
B_{11} \cdot X_{B-1} + \left[B_{12} \cdot R_{B-2} \cdot B_{12}^T + U \cdot R_{C-1} \right] \left[Y_{C-1} \right] +
$$

$$
\left[B_{12} \cdot R_{B-2} \cdot B_{22}^T \right] \left[Y_{C-2} \right] + 0 \cdot X_{C-2} = 0
$$

The first term is nonexistent in this case, because no X_{n-1} values exist in this **problem. Furthermore , because the last term is multipliea** *by zero,* **it vanishes, The resulting equation for this problem is therefore**

$$
\left[B_{12} \cdot B_{B-2} \cdot B_{12}^T + R_{C-1} \right] \left[Y_{C-1} \right] + \left[B_{12} \cdot R_{B-2} \cdot B_{22}^T \right] \left[Y_{C-2} \right] = 0
$$

Arithmetic Solution

Numerical computations with the previous equation will give the desired values for YC-1 , the flow on the streets connecting the zones. Replacing the symbols by the actual matrix and solving the triple matrix product gives the resulting matrix equation in terms of R . Insertmg the proper R values and reducing the matrix size where possible, gives the two matrix equations:

Thes e equations can now be solved directly by solving first for Yi4 to Yas and then for Y_{18} to Y_{23} . The solutions are **given in Table 4,**

Discussion of Systems Solution

The matrix mampulations and the arithmetic solution have only been sketched, A more detailed discussion of the steps taken and of the validity of the computation would have been too extensive for this paper, but these matters are ex**plained in detail m the texts on this subject (2).**

It might be argued at this point that a rather cumbersome algebraic procedure was used to solve a relatively trivial problem and that systems analysis for larger **and more complex systems would be im possible to do manually. This is correct, but the extensive algebraic manipulations** are an easy task for an electronic com**puter. The only reason for manually computing such a small example here is to demonstrate how such a problem can be worked. Michigan State University is presently developmg a computer program which will solve these steps and produce the final answers directly from the given terminal and system equations.**

A flow diagram of the solution showing the flow of trips to work only is given in Figure 4.

Comparison with Gravity Model

In this and the following sections the same sample problem is worked using **the iterative processe s called "gravity model" (6) and "electrostatic model" (7), respectively. Only the principal formulas used and the correction factors ar e re peated here.**

The results of the second estimate of the gravity model and of the fourth assignment of the electrostatic model are compared with the results obtained with systems engineermg methods in Table 5. The difference of each flow line computa**tion by the three methods is shown and expressed in percentages, assuming the systems solution as a basis.**

$$
T_{1j} = \frac{T_{i} \times T_{j} / (D_{1j})^{X}}{\sum_{l} T_{j} / (D_{ij})^{X}}
$$

LABLI -	
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WORK TRIPS OR FLOW THROUGH **EAC H ELEMEN T**

Scale 1 inch = 5000 work trips

Figure 4. Flow diagram of work trips from four residential zones to three em**ployment zones.**

in which

- **T j = number of auto drive r work trips made from each residential area (i);**
- **' J size of attractor represented by number of auto driver trips made to each industrial are a (j);**
- **Dij = distance factor expressed in terms of travel time;**
- X **= empirically determined exponent, assumed as 0.5.**

Corrections in the first computation are made as follows:

1. A correction factor is computed for each value of j which equals

$$
\begin{array}{c}\nT_j \\
\hline\n\frac{1}{2} & T_{1j}\n\end{array}
$$

2. The first estimate is multiplied by the appropriate correction factors.

Comparison with Electrostatic Model

$$
V_{P_1 Q_j} = \frac{\frac{Q_j}{R_{1j}} \times P_1}{\sum_{j=1}^{m} \frac{Q_j}{R_{1j}}} \qquad (1 = 1, 2, ..., n)
$$

in which

probability of movement from 1 to *j*; $V_{P_1Q_1}$ $=$

 P_1 $=$ number of workers living in Zone i;

 Q_1 = number of jobs available at Zone **j**;

straight-lme distance from i to j if the field contains R_{11} **no physical barriers. Where such barrier s exist, R would have to be the straight-lme distance from** 1 to the point of passage across the barrier plus **that from the point of passage to j .**

To Zone	Model ^a	From Zone 26			From Zone 27			From Zone 30		From Zone 31		Total to	
		Flow	Δ	%	Δ Flow	%	Flow	Δ	%.	Flow	Δ	ą,	Zones
	s	1.1991			7789		536 1			4859			3,000,0
	G	1.1615	$-376 - 31$		$6950 - 839$	-108	623 ₅	$+ 874 + 163$			$5199 + 34.0$		$+702.9999$
	E	1.2176	$+185 + 15$		583 7 - 195.2	-250	7078	$+171$ 7	$+320$		$490.9 + 5.0$		$+1, 0$ 3,000 0 3,000.0
28	s	1.2154			825 1		490 3			469.2			
	G	1.2319	$+165 + 1.4$		$8121 - 130$	-16	507 2	$+16.9 + 3.5$					$461.4 - 78 - 163.0126$
	E	1.359.8	$+144.4$ $+11.9$		$7916 - 33.5$	-41	464.9	-254	-52				383 7 -85 5 -18 2 3,000 0
29	s	1.585.5			1.3961		973 5			1.044.9			5.000.0
	G	1.6205			$+ 350 + 221.494.1 + 980 + 70$		869 5	-104.0					-10 7 1, 014, 7 -30 2 - 2 9 4, 998 8
	E	1.423.5			-162 0 -10 2 1, 624, 2 + 228 1 + 16 3		827.4	-146 1		-150 1, 124, 8 +79 9 + 7, 6 4, 999 9			
Total	s	4.0000			3,000,1		1.9999			2,0000			11,000,0
	G	4.0139			3,001 2		2.000.2			1,996 0			11,011 3
	E	4.000.9			2,999 5		2,000,1			1,9997			11,000 1

TABL E 5 COMPARISO N O F FLO W COMPUTATION S

aS = systems engineering, G = gravity model, E = electrostatic model

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Corrections in this computation are based on the following equation:

1. First assignment is multiplied by the appropriate correction factor C_1 for $j =$ $1, 2, \ldots, m$

$$
C_j = \frac{Q_j}{\sum_{i=1}^n V_{P_i Q_j}}
$$

2. The second assignment is multiplied by the appropriate correction factor C i for $1 = 1, 2, \ldots, n$

$$
C_1 = \frac{P_1}{\sum_{j=1}^{m} V_{P_1 Q_j}}
$$

3. The first and second steps are repeated for each successive assignment.

COMMENTS

The example problem, although extremely small, should have served to demonstrate the great potential of systems analysis by linear graph techniques for theoretical traffic flow problems. Many simplifying assumptions have been made. Further research is required to establish the technique to the point where it can be used to its full potential. The next step in the research will be a test of the theory against actual origin and destination surveys.

Future work on establishing other system components must be tried to evolve finally the best possible components or component systems, with proper x and y measurements and terminal representation. It is possible that a heterogeneous zone might be separated into distinct parts, each of which may be defined by a component and described mathe-

matically.
The components used to date require a more complete study. For example, the **The components used to date require a more complete study. Fo r example, the curves used to predict the resistance factor on the street components must be studied**

more completely.
Although only a hypothetical case has been presented here, the results, when com-Although our any *a hypothetical case has been presented as how promise for eventual* part with the gravity model or the electrostatic model of the model of the model of $\frac{1}{2}$

acceptance of this method.
It must be recognized, too, that changes in parameters in the given system can be made easily without disturbing the principles of the technique. Thus, any refinements in component definition can be entered as they become available without need for dein component definition can be entered as the entered in the entered as the entered as the component of dependence of \mathbb{R} reputable this technique will permit research into the **velopment of a new technique. Eventually this technique will permit research into the parameters.**

Appendix

DETAILS OF LINEAR GRAPH

Measurements

In the mathematical analysis of any given type of physical system (electrical, mechanical, thermal, etc.) the tie between the mathematics and the system is generally accomplished through the use of two basic measurements; the across (or x) and the through (or y) measurements. The x and y measurements used to date are

- **1. Electrical . —x is voltage and y is current flow.**
- **2. Mechanical translation. —x is displacement and y is force .**
- **3. Therma l systems. —x is temperature and y is heat flow.**
- **4. Hydraulics. —x is pressur e and y is flow.**

Definitions

Termina l Graph. —The terminal graph of an n-terminal component is defined as a collection of (n - 1) oriented line segments which forms a connected graph with no circuits and includes exactly one vertex for each terminal of the component.

In general, the terminal graph serves to identify the variables in the terminal equa**tions with a unique set of measurements and establishes a vital link between the physical component and its mathematical description. The graph or terminal equation are each incomplete m themselves.**

Termina l Equations. —The mathematical equations relatmg the measurements represented by the through and across variables of the terminal graph are called the **termmal equations of the component.**

Termina l Representation. —The terminal graph plus the terminal equations are called the terminal representation of a system component.

System Graph. —A system graph is a collection of component terminal graphs obtained by uniting the vertices of the terminal graphs in a one-to-one correspondence **with the union of the physical components. When the fundamental operational concept of the linear graph is adopted, the system graph follows directly from the prescribed** manner in which the components of the system are connected. If the characteristics **of the system components can be determined—and they must be if the system is to be analyzed—there is never any question as to the form of the system graph.**

System Equations. —The graph equations along with the terminal equations of the system components are defined as the system equations. The fundamental cut-set **equations, stating that the sum of all through measurements at the vertices equal zero, and fundamental circuit equations, hereafter referred to as the graph equations, serve to establish a set of independent equations among the through and among the across** variables used in presenting the characteristics of the system components.

The system equations represent a complete mathematical description of the system. When the terminal equations of the system components are linear, a partial solution to **these simultaneous equations can be effected without the necessity of calculating an inverse . The partial solutions obtainable depend on the given forms of component terminal equations.**

Tree . —If a connected graph G contains v vertices, connected subgraph of G containing all V **vertices and no circuits is defined as a tree.**

Branches. —The elements in the tree are appropriately called branches. Although there may be many different trees in any graph, a tree is easily identified by simply **allowing one and only one element to join any pair of the v vertices. The tree which has all elements incident at one vertex is called a Lagrangian tree.**

Chords. —The elements of a connected graph G which form the complement of a tree are defined as chords.

Specified Values. - The tree will then be further subdivided into those elements for **which one has specified x or across variables, symbolically referred to as (B-1), and those for which no variable is known (B-2). The chords are also subdivided into (C-1) which are the unknowns and (C-2) for which the y or through variable has been specified.**

Postulates

The graph equations can be established when the vertex and circuit equations are **satisfied. The system must be such that the x or across variables will sum to zero around the circuits of the systems graph and further that the y or through variables** sum to zero at the vertices of the linear graph. The fundamental across and through variables used to represent measurements in the various types of physical systems **all have these important and fundamental properties. The mathematical formulation of these properties (the vertex and circuit equations, together with the component terminal equations) forms the basis for the analysis of physical systems. If the through and across variables of the system graph are defined so that they sum to zero at the vertices and around the circuits, then these techniques of formulation will apply** to that physical system. These criteria can be formally stated as postulates.

Vertex Postulate. —If the system graph of a physical system contains e-oriented elements and if y_j represents the fundamental through variable of the jth element, then **at the kth vertex of the grs^h**

$$
\sum_{j=1}^{e} a_j y_j = 0
$$

in which

 $a_1 = 0$ if the jth element is not incident at the kth vertex; $\mathbf{a}_1 = 1$ if the jth element is oriented away from the kth vertex; $a_1 = -1$ if the jth element is oriented toward the kth vertex.

Circuit Postulate. -I f the linear graph of a physical system contains e-oriented elements and if x_1 represents the fundamental across variable of the jth element, then **for the kth circuit**

$$
\sum_{j=1}^{e} b_j x_j = 0
$$

in which

 $b_1 = 0$ if the jth element is not included in the kth circuit;

 $b_1 = 1$ if the orientation of the $j^{\mu\nu}$ element is the same as the **orientation chosen for the k^h circuit;**

b, = -1 if the orientation of the jth element is opposite to that of the kth circuit.

When the circuits used in writing the independent equations ar e chosen so as to include the branches first and chords last, a general and convenient form can be obtained. This is also applicable when writing the vertex or segregate equations except that one and only one branch is included when summing around the vertices.

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