

# Skid Number and Speed Gradients on Highway Surfaces

David C. Mahone, Virginia Highway and Transportation Research Council

In the project from which this paper was derived, three major factors that influence the skid number (SN) and speed gradient (G) were studied: tire tread depth, water film, and pavement surface texture (1). However, only the effect of pavement surface is discussed here; the measurement of texture is not considered. The 31 sites that were included in the study are given in Table 1.

In the study, tread depths of 0.87 cm, 0.71 cm, 0.56 cm, 0.40 cm, 0.24 cm, and bald ( $1\frac{1}{32}$  in,  $\frac{9}{32}$  in,  $\frac{7}{32}$  in,  $\frac{5}{32}$  in,  $\frac{3}{32}$  in, and bald) and water film thicknesses of 0.04, 0.05, 0.08, and 0.10 cm (0.015, 0.020, 0.030, and 0.040 in) were tested at speeds of 48.3, 64.4, 80.5, 96.6, and 112.6 km/h (30, 40, 50, 60, and 70 mph). For each combination of test conditions, 5 skid resistance measurements were made at each site for each speed, which totaled more than 13 000 tests. The data reported here have been combined and averaged from all tread depths, excluding bald, and all water film thicknesses for each test speed. Detailed descriptions of the testing method and the procedures used in combining the data can be found elsewhere (1). However, I feel that the data show the same general trends that would be expected with treaded tires and the normal water output required by ASTM E 274-70 (2).

## RESULTS

In the analysis of the test data, the pavements generally fit into three groups: steep gradients—0.50 G or greater, intermediate gradients—0.28 to 0.40 G, and flat gradients—0.20 G or less. The curves for the three groups are shown in Figure 1.

Five of the 31 sites provided G values of 0.50 or greater. They consisted of smooth concrete, a sand asphalt, and a well-worn S-5 bituminous concrete. Table 2 gives the average SNs for the various test speeds, the average G for each of these sites, and the total accumulated traffic.

Twenty of the 31 sites fit in the intermediate speed gradient group. Table 3 gives the summary data for these sites. The sites consisted of various aged S-5 bituminous concrete surfaces; a special urban bituminous mix (3); a surface treatment; and several types of portland cement concrete textures including single burlap-dragged, longitudinally tined, grooved, and bush-hammered textures (4).

Table 4 gives the summary data for the sites in the flat gradient group. These sites consisted of bituminous concrete surfaces, open-graded (popcorn mix) bituminous surfaces, and surface treatments.

Basically, the textures for the pavements represented by the three curves in Figure 1 are

1. Steep gradient, which is for surfaces with smooth macrotexture but gritty or smooth microtexture.
2. Intermediate gradient, which is for all of those surfaces with a good combined microtexture and macrotexture. In addition, some well-worn surfaces that would originally have been found in the steep gradient group fell into this group when they lost their microtexture. Also included are some well-worn surfaces that originally would have been in the flat gradient group. These two exceptions can usually be identified by a lower than expected  $SN_{40}$  value combined with knowledge concerning the accumulated traffic passes and the material from which the surface was fabricated.
3. Flat gradient, which is for surfaces with excellent microtexture and macrotexture.

The estimated slopes for the curves are as follows for various speed ranges (1 km/h = 0.621 mph):

| Group        | 48 to<br>80 km/h | 64 to<br>96 km/h | 80 to<br>112 km/h | 48 to<br>112 km/h |
|--------------|------------------|------------------|-------------------|-------------------|
| Steep        | 0.73             | 0.61             | 0.47              | 0.60              |
| Intermediate | 0.42             | 0.33             | 0.25              | 0.33              |
| Flat         | 0.23             | 0.17             | 0.08              | 0.15              |

It should be noted that the gradient decreased as the test speed increased and that the gradient between 64.4 and 96.6 km/h (40 and 60 mph) was quite similar to the gradient between 48.3 and 112.6 km/h (60 and 70 mph). On

**Table 1. Site information.**

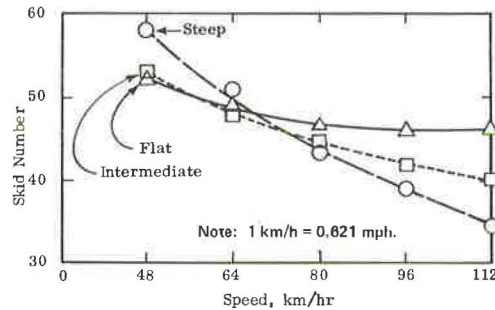
| Site Number | Type of Surface                      | Year Placed | Lane   | Accumulated Traffic (vehicles) |
|-------------|--------------------------------------|-------------|--------|--------------------------------|
| 1           | Portland cement concrete             | 1970        | EBTL   | 4 028 870                      |
| 2           | Portland cement concrete             | 1970        | WBPL   | 1 007 218                      |
| 3           | S-5 bituminous concrete <sup>a</sup> | 1970        | EBTL   | 4 028 870                      |
| 4           | S-5 bituminous concrete <sup>a</sup> | 1970        | WBPL   | 1 007 218                      |
| 5           | S-1 sand asphalt <sup>a</sup>        | 1968        | N&SBTL | 3 149 950                      |
| 6           | Portland cement concrete             | 1959        | SBTL   | 17 212 962                     |
| 7           | Portland cement concrete             | 1959        | SBPL   | 4 303 240                      |
| 8           | Mechanically chipped concrete        | 1974        | SETL   | 0                              |
| 9           | Mechanically chipped concrete        | 1974        | SBPL   | 0                              |
| 10          | S-5 bituminous concrete <sup>a</sup> | 1969        | EBTL   | 4 411 755                      |
| 11          | S-5 bituminous concrete <sup>a</sup> | 1969        | WBTL   | 4 411 755                      |
| 12          | S-5 bituminous concrete <sup>a</sup> | 1969        | EBPL   | 1 102 939                      |
| 13          | S-5 bituminous concrete <sup>a</sup> | 1969        | WBPL   | 1 102 939                      |
| 14          | Bituminous urban mix <sup>a</sup>    | 1971        | SBTL   | 3 255 800                      |
| 15          | Bituminous urban mix <sup>a</sup>    | 1971        | SBPL   | 3 255 800                      |
| 16          | Popcorn bituminous mix               | 1973        | NBTL   | 2 285 630                      |
| 17          | Popcorn bituminous mix               | 1973        | SBPL   | 571 408                        |
| 18          | S-5 bituminous concrete <sup>a</sup> | 1968        | NBTL   | 9 187 050                      |
| 19          | S-5 bituminous concrete <sup>a</sup> | 1968        | SBPL   | 2 296 762                      |
| 20          | Portland cement concrete             | 1973        | EBTL   | 2 106 780                      |
| 21          | Portland cement concrete             | 1973        | EBTL   | 526 695                        |
| 22          | Portland cement concrete             | 1968        | EBTL   | 13 430 175                     |
| 23          | Portland cement concrete             | 1968        | EBPL   | 7 815 106                      |
| 24          | Grooved portland cement concrete     | 1968        | EBTL   | 13 430 175                     |
| 25          | Grooved portland cement concrete     | 1968        | EBPL   | 7 815 106                      |
| 26          | Surface treatment                    | 1969        | NBPL   | 534 542                        |
| 27          | Surface treatment                    | 1969        | SBTL   | 2 138 170                      |
| 28          | Surface treatment                    | 1970        | NBPL   | 449 680                        |
| 29          | Surface treatment                    | 1970        | SBTL   | 1 798 720                      |
| 30          | S-5 bituminous concrete <sup>a</sup> | 1965        | WBPL   | 2 342 388                      |
| 31          | S-5 bituminous concrete <sup>a</sup> | 1965        | EBTL   | 3 360 550                      |

Note: EB = eastbound; WB = westbound; NB = northbound; SB = southbound; TL = through lane; and PL = passing lane.  
<sup>a</sup>Specifications can be found in Road and Bridge Specifications (5).

the other hand, the gradient between 48.3 and 80.5 km/h (30 and 50 mph) bears little resemblance to that between 80.5 and 112.6 km/h (50 and 70 mph). Therefore, great care should be taken in selecting test speeds to establish gradients.

There is no question that the average G value decreased with increased macrotexture. Exceptions to this were the grooved concrete pavements on which the grooves or macrotexture provided ample water escape routes but no microharshness; therefore, the gradient was rather steep. This finding indicates that, in addition to a provision for the escape of water, a pronounced

**Figure 1. Speed gradients for three groups of pavements.**



**Table 2. Summary data for steep gradient group.**

| Site Number | Skid Number |         |         |         |          | Slope (SN/km/h) | Accumulated Traffic (millions of vehicle passes) |
|-------------|-------------|---------|---------|---------|----------|-----------------|--|
|             | 48 km/h     | 64 km/h | 80 km/h | 96 km/h | 112 km/h |                 |  |
| 1           | 58          | 50      | 43      | 39      | 35       | 0.58            | 4.0  |
| 2           | 67          | 60      | 52      | 47      | 41       | 0.65            | 1.0  |
| 5           | 62          | 54      | 46      | 39      | 33       | 0.73            | 3.1  |
| 23          | 57          | 52      | 45      | 42      | 37       | 0.50            | 7.8  |
| 31          | 47          | 40      | 32      | 28      | 25       | 0.55            | 9.4  |
| Average     | 58          | 51      | 43      | 39      | 34       | 0.60            |  |

Note: 1 km/h = 0.621 mph.

**Table 3. Summary data for intermediate gradient group.**

| Site Number     | Skid Number |         |         |         |         |          | Slope (SN/km/h) | Accumulated Traffic (millions of vehicle passes) |
|-----------------|-------------|---------|---------|---------|---------|----------|-----------------|--|
|                 | 32 km/h     | 48 km/h | 64 km/h | 80 km/h | 96 km/h | 112 km/h |                 |  |
| 3               | —           | 54      | 45      | 45      | 51      | 39       | 0.38            | 4  |
| 4               | —           | 56      | 53      | 49      | 47      | 44       | 0.28            | 1  |
| 6               | —           | 37      | 32      | 29      | 25      | 23       | 0.35            | 17   |
| 7               | —           | 47      | 42      | 37      | 33      | 31       | 0.40            | 4  |
| 8               | —           | 42      | 37      | 33      | 31      | 30       | 0.30            | 0  |
| 9               | —           | 50      | 45      | 41      | 37      | 36       | 0.35            | 0  |
| 10              | —           | 53      | 49      | 45      | 42      | 40       | 0.33            | 4.3  |
| 11              | —           | 52      | 49      | 45      | 44      | 42       | 0.25            | 4.3  |
| 14 <sup>a</sup> | 61          | 56      | 46      | 50      | 48      | —        | 0.33            | 3.25   |
| 15 <sup>a</sup> | 65          | 59      | 55      | 51      | 49      | —        | 0.40            | 3.25   |
| 18              | —           | 53      | 50      | 46      | 42      | 39       | 0.35            | 9  |
| 19              | —           | 56      | 53      | 50      | 46      | 44       | 0.30            | 2.5  |
| 20              | —           | 60      | 58      | 56      | 53      | 48       | 0.30            | 2  |
| 21              | —           | 72      | 66      | 63      | 59      | 57       | 0.38            | 2.5  |
| 22              | —           | 50      | 44      | 39      | 36      | 38       | 0.30            | 13.5   |
| 24              | —           | 49      | 48      | 43      | 41      | 39       | 0.25            | 13.5   |
| 25              | —           | 56      | 52      | 49      | 45      | 40       | 0.40            | 7.7  |
| 27              | —           | 42      | 38      | 35      | 33      | 31       | 0.28            | 2  |
| 29              | —           | 45      | 41      | 37      | 36      | 34       | 0.28            | 1.75   |
| 30              | —           | 55      | 48      | 47      | 41      | 41       | 0.35            | 2.3  |
| Average         | —           | 53      | 48      | 44      | 42      | 40       | 0.33            |  |

Note: 1 km/h = 0.621 mph.

<sup>a</sup>Only 0.05 cm (0.020-in) film of water tested with speeds 32.2 to 96.6 km/h (20 to 60 mph).

**Table 4. Summary data for flat gradient group.**

| Site Number | Skid Number |         |         |         |          | Slope (SN/km/h) | Accumulated Traffic (millions of vehicle passes) |
|-------------|-------------|---------|---------|---------|----------|-----------------|--|
|             | 48 km/h     | 64 km/h | 80 km/h | 96 km/h | 112 km/h |                 |  |
| 12          | 53          | 50      | 48      | 46      | 46       | 0.18            | 1  |
| 13          | 53          | 50      | 47      | 46      | 48       | 0.18            | 1  |
| 16          | 50          | 50      | 48      | 47      | 45       | 0.13            | 2.3  |
| 17          | 50          | 47      | 46      | 46      | 46       | 0.10            | 0.5  |
| 26          | 51          | 48      | 46      | 42      | 43       | 0.23            | 0.5  |
| 28          | 53          | 49      | 48      | 47      | 46       | 0.18            | 0.5  |
| Average     | 52          | 49      | 47      | 46      | 46       | 0.15            |  |

Note: 1 km/h = 0.621 mph.

microtexture is needed to provide a flat gradient. By the same token, if an open-graded bituminous mix is manufactured with aggregate that is highly polish susceptible, it probably will develop a rather steep gradient in addition to becoming slippery.

The data, then, point to the following: High G values are common to pavements that do not have a relatively high degree of macrotexture. Although this fact merely substantiates previous research on the subject, if the surface has a sharp microtexture, as is the case for all locations except site 31 in the steep gradient group, its skid resistance can be excellent at all legal speeds with legal tread tires.

The highest skid numbers recorded in the study were at low speeds in the steep gradient group, which means that a low macrotexture and a high microtexture provide the best skid-resistance surface at low speeds [64.4 km/h (40 mph) and lower]. Cities and counties should take this into account when they are paving streets with low speed limits. On the other hand, the open-graded mixes, which provide flat gradients, provide a very desirable surface for high-speed traffic. Grooving does not improve the skid resistance or the G value for treaded tires. Thus, because grooving does not decrease the G value, I suggest that the mere provision for water escape does not guarantee that the pavement surface will have a flat gradient.

#### REFERENCES

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