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TRANSPORTATION RESEARCH BOARD

Evaluating Tack Coat Materials' Durability in Asphalt Pavements

March 31, 2021

@NASEMTRB
#TRBwebinar

PDH Certification Information:

1.5 Professional Development Hour (PDH) – see follow-up email for instructions
You must attend the entire webinar to be eligible to receive PDH credits
Questions? Contact Reggie
Gillum at <u>RGillum@nas.edu</u>

#TRBwebinar

The Transportation Research Board has met the standards and requirements of the Registered **Continuing Education Providers** Program. Credit earned on completion of this program will be reported to RCEP. A certificate of completion will be issued to participants that have registered and attended the entire session. As such, it does not include content that may be deemed or construed to be an approval or endorsement by RCEP.



REGISTERED CONTINUING EDUCATION PROGRAM

Learning Objectives

1. Discuss appropriate selection of tack coat materials and application rates

2. Develop specifications for the use of tack coat materials

#TRBwebinar

Effect of Tack Coat Materials on Durability of Asphalt Pavement

Louay N. Mohammad, Ph.D., P.E., Fellow ASCE Irma Louise Rush Stewart Distinguished Professor Department of Civil and Environmental Engineering Louisiana Transportation Research Center Louisiana State University

TRB Webinar: Evaluating Tack Coat Materials' Durability in Asphalt Pavements March 31, 2021

Key Topics

- Durability
 - Pavement Performance
 - Bonding
- Tack Coat Research
 NCHRP Project 9-40
 »Report No. 712
 - NCHRP Project 9-40A
 - » Report No. 878
- Summary and Conclusions



Acknowledgement

- Technical Review Panel
- State DOTs

LTRC Asphalt Lab

State DOTs

Missouri; Louisiana; Florida; Tennessee; Nevada; Oklahoma

Material Suppliers and Contractors

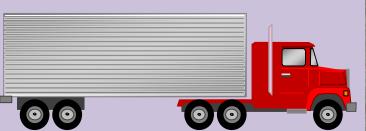
- Asphalt Products Unlimited
- Ergon Asphalts
- Blacklidge
- Coastal Bridge

- . . .

Durable Flexible Pavement

- Permanent deformation
- Fatigue cracking repeated load
- Low temperature cracking
- Moisture induced damage
- Raveling
- etc ...













Durable Flexible Pavements

Mixture Design

- Components Materials
- BMD
- Sustainable Development

Construction

- Tack Coat Practices
- Thermal segregation
- Warm Mix Asphalt
- Increased density

Laboratory Design



Field Construction



Durable Flexible Pavements

• Mixture Design

- Components Materials
- Engineered Performance
- Sustainable Development

Construction

- Tack Coat Practices
- Thermal
- Warm Mi
- Increased

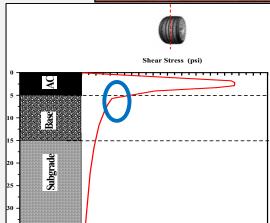




Field Construction



Durable Pavement – Construction Tack Coat



Purpose of tack coat application

- To ensure adequate bond between pavement layers
- To transmit traffic loads down through the whole pavement structure

Not properly bonded, increase tendency for

- Cracking,
- Debonding (delamination/slippage/sliding), and/or
- Fatigue cracking
- ...and thus failure in the new overlay

Tack coat material is relatively inexpensive portion compared to overall pavement construction cost

Bonding failure is extremely \$\$\$!!!





Improper Tack Coat Application



Courtesy of James A. Scherocman

Proper Tack Coat Application Uniform Coverage



| 0.031 gsy | 0.062 gsy | 0.155 gsy |
|-----------|-----------|-----------|
| Low | Medium | High |

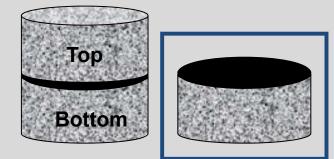
Objectives – NCHRP Project 9-40

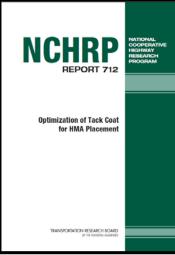
Evaluate factors that affect interlayer bonding

- Tack coat material type and application rate
- Pavement surface type
- Temperature
- Construction condition

Develop AASHTO test methods and practices related to tack coats

- Tack Coat Quality
 - spray application
- Interlayer Bond Strength





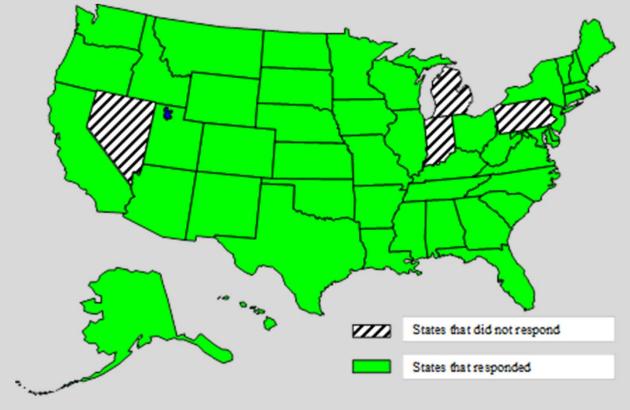
Outcome – NCHRP Project 9-40

Worldwide Survey on Tack Coat Practices

- 92% return
- Canada, Denmark, Finland, South Africa, and the Netherlands.

Best Practices and Training Manual

recommended construction and testing procedures



Tack Coat Application Inspection



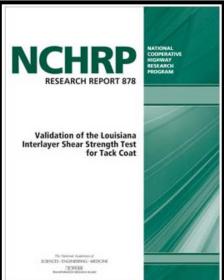
Outcome – NCHRP Project 9-40

- Recommended tack coat residual application rates
- AASHTO TP 114 and AASHTO TP 115 test method was developed to characterize quality and Bond Strength of tack coats
- Recommended threshold Interface Shear Strength criterion
 - Minimum 40 psi from AASHTO TP 114

| | | аазнто ТР 114 | |
|--------------|-----------------------------------|---------------|--|
| Surface Type | Residual Application rate, gsy | - | |
| New HMA | 0.035 | | |
| Existing HMA | 0.055 | | |
| Milled HMA | 0.055 | | |
| PCC | 0.045 | | |

Objective – NCHRP Project 9-40A

- Validate AASHTO TP 114 test method and minimum recommended ISS threshold (40 psi) criterion
- Evaluate factors that affects interface bonding
 - Pavement Surface Type
 - Tack Coat Material Type
 - Residual Application Rate
 - Service Time
- Investigate the effect of bonding on short-term pavement performance



Scope

Six field projects

Missouri; Louisiana; Florida;
 Tennessee; Nevada; Oklahoma

Given Pavement surface types:

New HMA; Existing HMA; Milled HMA; PCC

Tack coat material types:

- Slow setting (SS-1H, CSS-1H, SS-1)
- Non-tracking rapid setting (NTSS-1HM, CBC-1H, CRS-1 HBC)

Tack coat residual application rates:

- specified by state DOTs
- recommended by NCHRP Project 9-40

| Climatic Zones: Wet-Freeze Wet-No Freeze Dry-Freeze Dry-No Freeze | AZ NIN OKA AL GA |
|---|------------------|
| | |

| Surface Type | Residual Application rate, gsy |
|--------------|--------------------------------|
| New HMA | 0.035 |
| Existing HMA | 0.055 |
| Milled HMA | 0.055 |
| PCC | 0.045 |

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Experimental Program

Field Measurements

- Distributor Truck Calibration (ASTM D 2995)
- Pavement Surface Texture Measurement (ASTM E 965)
- Measured Field Application Rate (ASTM D 2995)
- Distress Survey (LTPP Manual)
- FWD (Structural Capacity)
- Laboratory Measurements
 - Interface Shear Strength Test (AASHTO TP 114)
 - Tack Coat Material Characterization (AASHTO M 320)

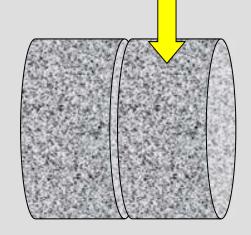






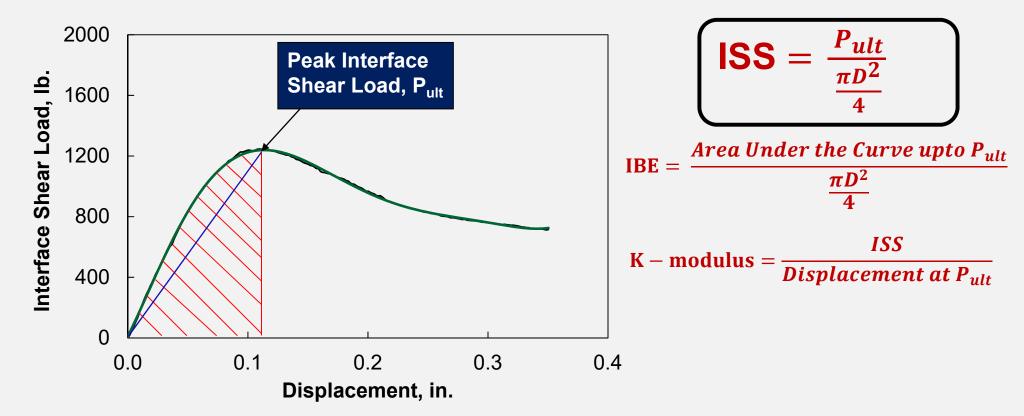






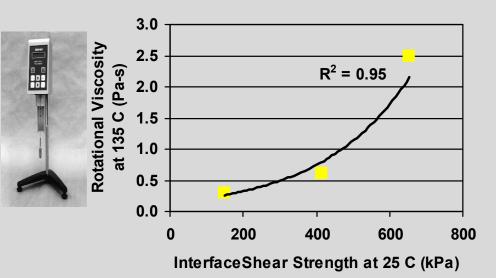


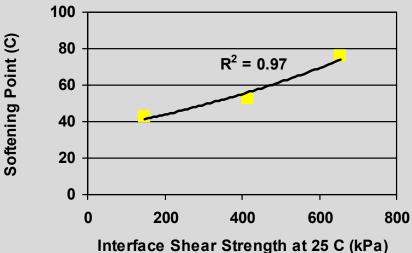
Laboratory Measurement – AASHTO TP 114 Tack Coat Materials Bond Quality

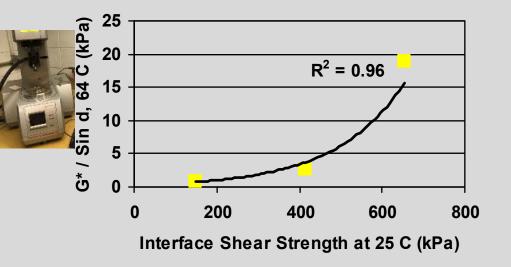


- Interface Shear Strength (ISS, psi) : COV < 15%</p>
- Interface Bond Energy (IBE, Ib.-in/in²)
- Interface Shear Stiffness (k-modulus, psi/in)

Relationship between ISS vs. Rheology Test Results



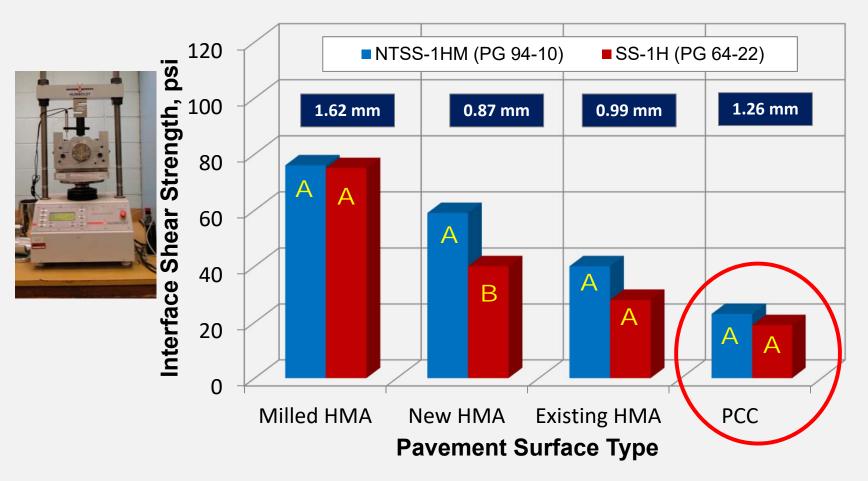






Effect of Pavement Surface Type on ISS

MISSOURI PROJECT



□ All tack coat material were compared at 0.05 gsy residual application rate

Effect of Pavement Surface Type on ISS

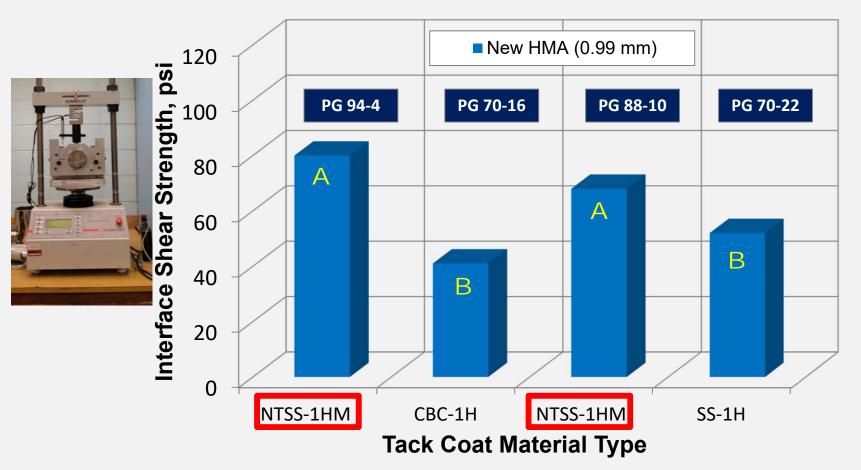
MISSOURI PROJECT



Pavement Surface Type

Effect of Tack Coat Type on ISS

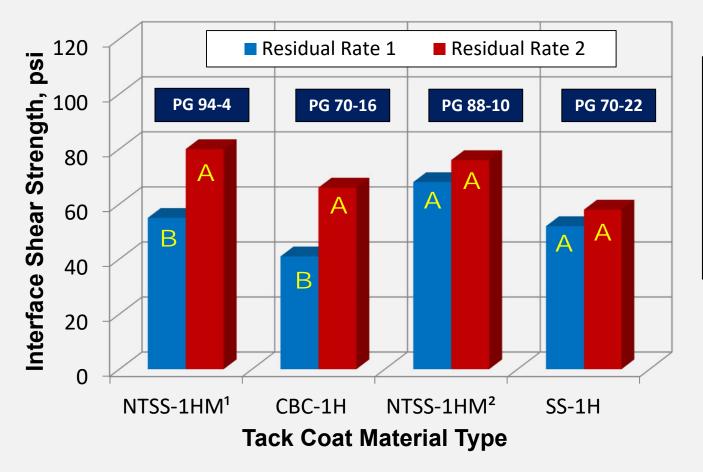
LOUISIANA PROJECT (LA 1053)



All tack coat material were compared at 0.02 gsy residual application rate

Effect of Residual Application Rate on ISS

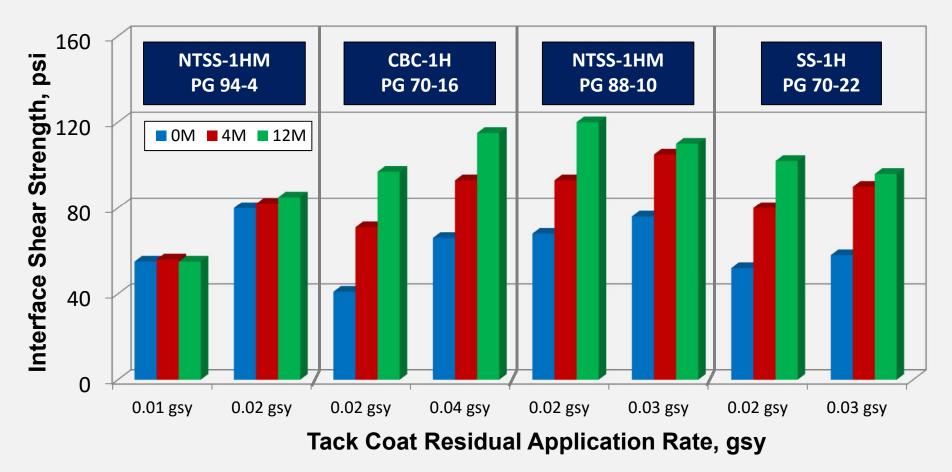
LOUISIANA PROJECT (LA 1053) New HMA



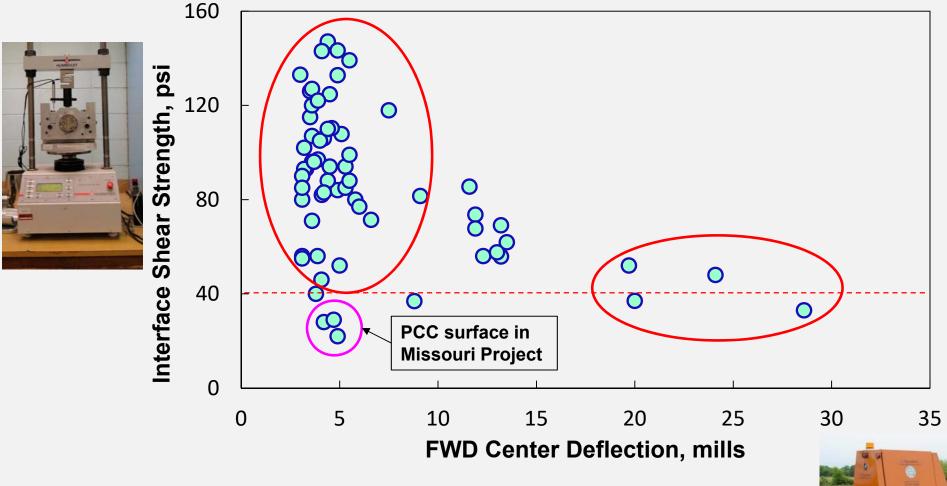
| Tack Coat Material | Residual Rate, gsy | |
|-----------------------|--------------------|------|
| | 1 | 2 |
| NTSS-1HM ¹ | 0.01 | 0.02 |
| CBC-1H | 0.02 | 0.04 |
| NTSS-1HM ² | 0.02 | 0.03 |
| SS-1H | 0.02 | 0.03 |

Effect of Service Time on ISS

LOUISIANA PROJECT (LA 1053) NEW HMA



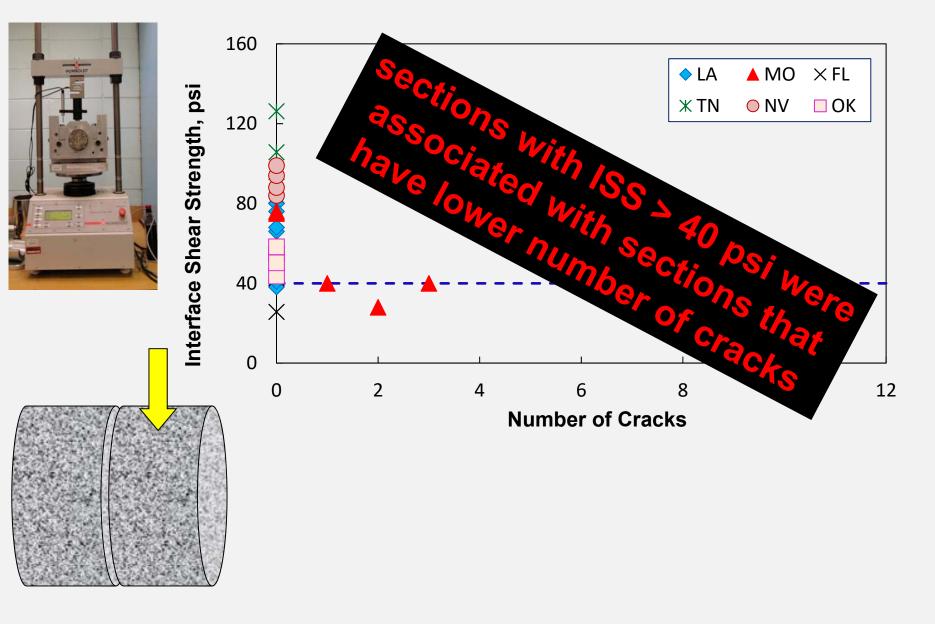
Structural Capacity (FWD) vs ISS



Indicates surface deflection depends on
 the interface bonding between pavement layers



Pavement Cracking vs Bond Strength (ISS)



Key Takeaways

Effect of tack coat type on ISS

Non-tracking rapid setting tack coats with <u>stiff base asphalt</u> (NTSS-1HM) exhibited the highest ISS, and slow setting resulted in the lowest

Effect of pavement surface type on ISS

- ISS was largely dependent on
 - Type of pavement surface (HMA versus PCC)
 - Type of pavement surface texture (milled versus non-milled)
- Milled surface yielded highest ISS, followed by new HMA, existing HMA, and PCC surface types
 - Higher surface roughness provided greater shear resistance

Effect of residual application rate on ISS

 ISS improved with increase in residual application rate for all tack coat types and pavement surface types

Key Takeaways

Effect of service time on ISS

- In geberal, ISS increased with increase in service time
 - tack coat curing

Pavement Structural Capacity (FWD test results)

- Mean center deflection decreased with service time
- Densification of overlays was attributed to
 - in-service trafficking
 - improved ISS

□ Short-term pavement performance

- ISS values correlated well with short-term performance
- test sections with ISS < 40 psi showed low to moderate cracking

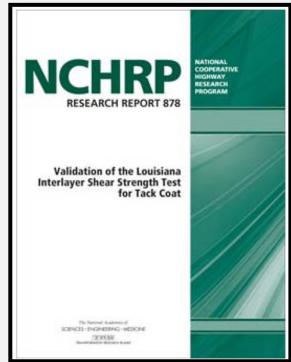
Recommendations

AASHTO TP 114 test

- Quality control and quality assurance testing of tack coat construction
- Evaluation of interface-bonding condition of in-service pavements

Use of minimum ISS threshold criterion (40 psi)

As the specification for satisfactory pavement performance



Thank you Louym@Lsu.Edu

Tack Coat Performance in Cold Regions

LAURA STASIUK M.SC., E.I.T.

UNIVERSITY OF SASKATCHEWAN



TRB WEBINAR: EVALUATING TACK COAT MATERIALS' DURABILITY IN ASPHALT PAVEMENTS

WEDNESDAY, MARCH 31, 2021 - 2PM EST

Outline

- Research Problem & Objectives
- Experimental Program
- Field Study & Findings
- Laboratory Testing Program
- Laboratory Testing Parameters

- Laboratory Study Findings
- Research Significance
- Future Research
- Acknowledgements
- Research Papers & Presentations

Research

Effect of Emulsion Type on Bond Behaviour of Asphalt Concrete Layers in Cold Regions Transportation Research Board (TRB)/Transportation Research Record (TRR), Washington, D.C., January 2019 Conference Presentation & Journal Paper Coauthored by Laura Stasiuk, Haithem Soliman, Ania Anthony

Subsequent research is included in my M.Sc. Thesis: Performance of Tack Coat Materials in Saskatchewan Climate University of Saskatchewan, February, 2020 http://hdl.handle.net/10388/12786

Research Problem

The effectiveness of tack coat products has not been studied extensively in the cold climate of Western Canada.

Tack coat application procedures are not well defined or followed.

Contractors often dilute tack coats heavily which does not allow breaking and setting to occur before paving.

Poor construction practices do not leave enough residue on the road for a good bond to form.

There is a gap in current research about performance and testing of tack coat materials in cold climate.

Research Objectives

• Evaluate the performance of several tack coat materials in Saskatchewan climate.

Monitor the field performance of tack coat materials during construction and in the following year.

Compare the bond quality of tack coat materials using a Louisiana Interlayer Shear Strength Tester (LISST).

Compare field and lab performance of tack coat materials to develop parameters that can be used to establish performance-based specifications for selection of tack coat materials.

Compare the performance of materials subjected to simulated freeze-thaw cycling and real-world exposure.

Experimental Program

5 years in duration – 2 years included in my research

Field Study

- Construction parameter monitoring
- Distress survey performance after construction and each summer
- Core Collection five periods of collection (2 periods included in research)
- Laboratory Testing Program
 - Bond strength testing
 - Lab conditioning to simulate freeze-thaw cycles

Field Study

- In August 2017 the tack coat trial project began
- Location: Highway 12 just south of Blaine
 Lake in Saskatchewan, Canada
- Highway 12: two-way, two-lane rural highway
- Resurfacing involved milling 30mm and laying 2 lifts of 50mm, placing the tack coat between the two lifts



Field Study Cont.

•A 1.1km section of the highway was designated for the project

■10 test sections were set up – 5 in each lane

Each section was approximately 225m long for a total of 1.1km

Tack Coat Products: SS-1 (3 sections, different dilution ratios), SS-1H (2 sections), CSS-1H, MS-1, three non-tracking/quick setting proprietary products

Target residual application rate of ~0.16 L/m² with triple overlap

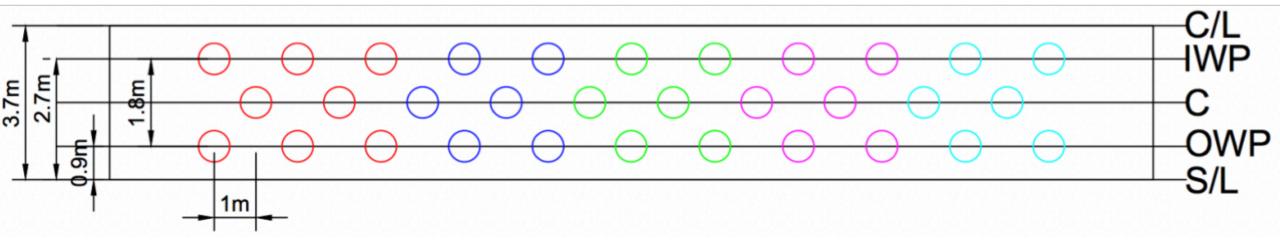
| 264 | 000 | | | | | 24+9 | -900 |
|-----|----------------------------|--------------------|---|-----|---------------------|--------------------|----------|
| | 6 SS-1 (50-50W) | 7 🗙 | | c * | 9 SS-1h (50-50W) | ¹⁰ B | |
| | 1 SS-1 (50-50W) | 2 SS-1h(50-50W) | 3 | A | 4 MS-1 (70-30W) | 5 SS-1 (30-70W) | |
| | 🛧 Indicates a cationic emu | Ision | | | - | | |

Coring

 Cores were collected in the wheel paths and centre of the lane, with 4-6 replicates per location and per product



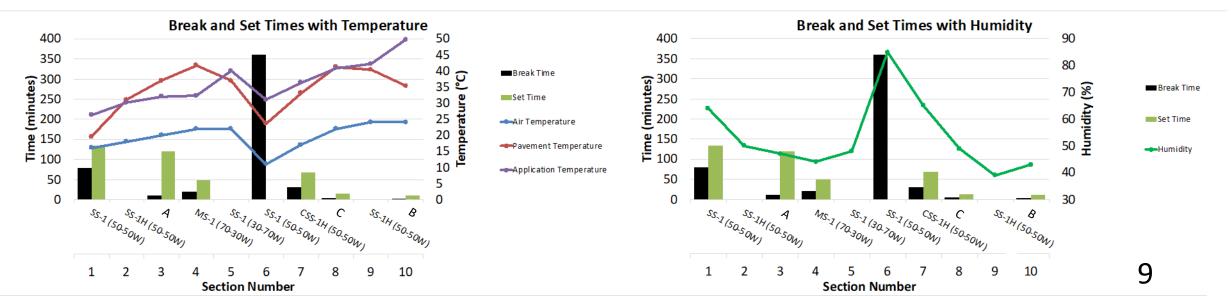
Collected 3 weeks post-construction, after 1 year, will continue each summer



Field Study Findings

Proprietary non-tracking products cure quickly which allows for less pickup and stronger bond.

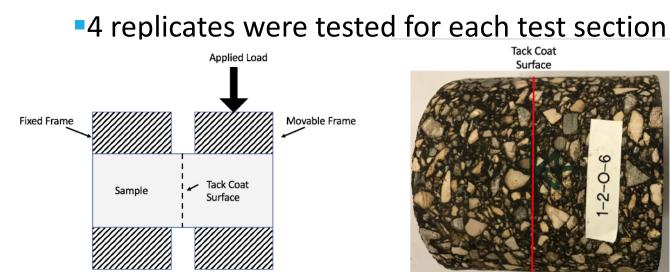
- All other products perform better, in terms of breaking and setting, than the basic SS-1 emulsion.
- •Weather conditions including temperature and humidity affect the speed of breaking and setting of tack coat materials. Hot dry weather will result in the fastest breaking and setting.
- The first two distress surveys, shortly after construction and one year post-construction, did not show any distresses due to the poor bond between pavement layers.

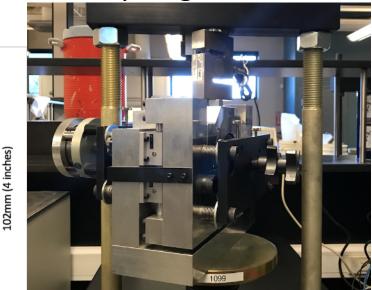


Laboratory Testing

Interlayer Shear Strength Testing Cores (AASHTO TP 114)

- Shear stress is applied to see how strong the bond is between the two pavement layers
- Louisiana Interlayer Shear Strength Tester (LISST)
- Three groups of cores- post construction cores (baseline), year one cores, cores lab conditioned cores subjected to accelerated freeze-thaw cycling

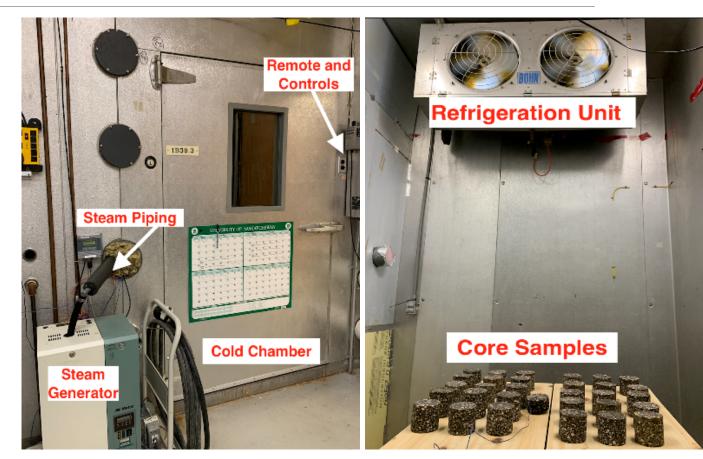




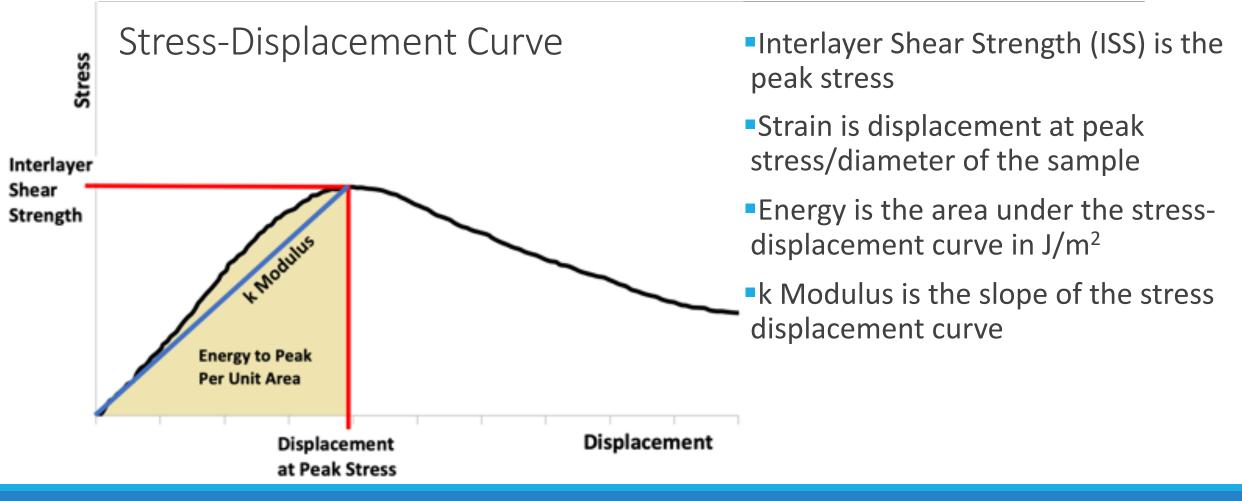
Environmental Conditioning

 A portion of the cores collected post construction were environmentally conditioned in a freeze thaw chamber prior to shear strength testing.

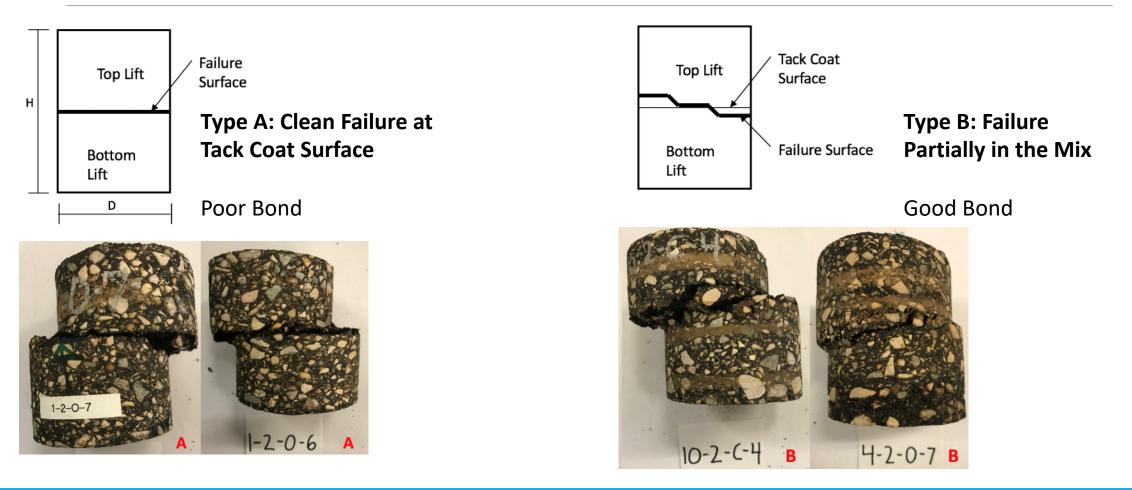
- Up to 15 Freeze-Thaw cycles, 12 hours at -25°C and 12 hours 15°C and 50-60% relative humidity
- 4 thermocouples measured the temperature of the chamber, one inside a core sample



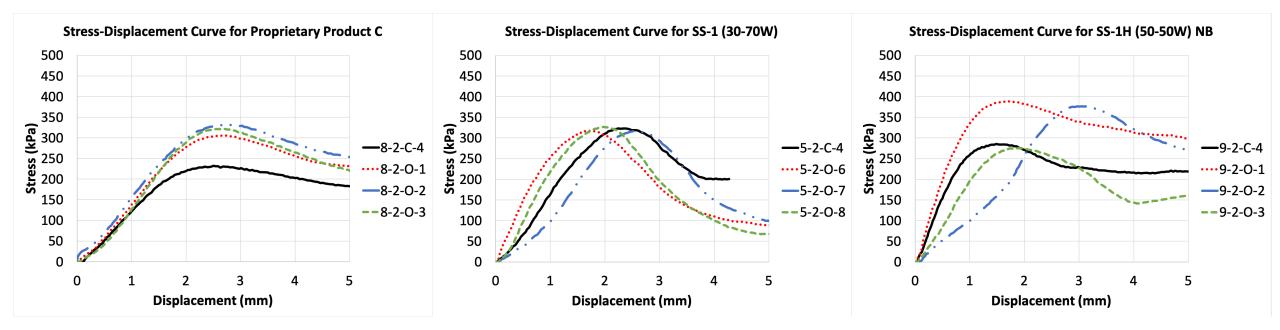
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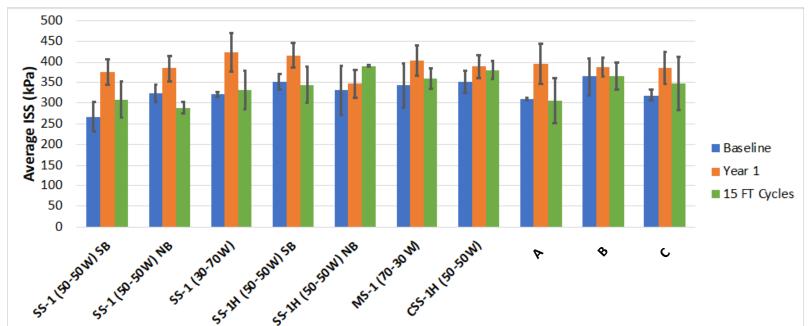
Stress-Displacement Curves



Lab Testing Program Findings – ISS

One year cores had the highest ISS, followed by lab conditioned cores, and then baseline cores. The increase in ISS can be attributed to the continuous curing of tack coat materials.

SS-1 products with 50-50W dilution consistently ranked low in terms of ISS among the three core groups.

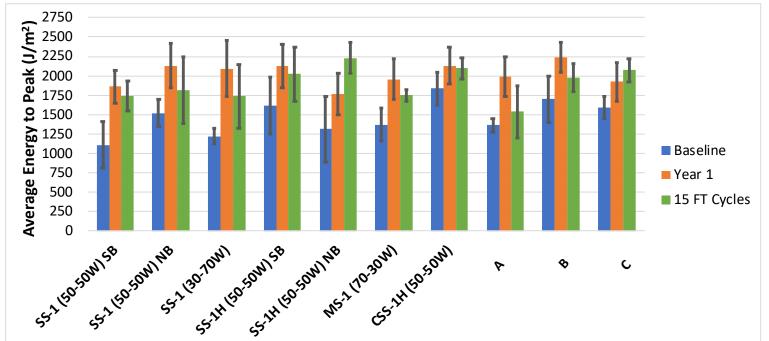


Lab Testing Program Findings – Failure Type

| Section | Material | Baseline | Year 1 | 15 FT Cycles |
|---------|-------------------|----------|--------|--------------|
| 1 | SS-1 (50-50W) SB | A | A | А |
| 6 | SS-1 (50-50W) NB | A | A | В |
| 5 | SS-1 (30-70W) | A | A | А |
| 2 | SS-1H (50-50W) SB | В | В | В |
| 9 | SS-1H (50-50W) NB | В | A/B | В |
| 4 | MS-1 (70-30W) | В | A/B | В |
| 7 | CSS-1H (50-50W) | В | В | В |
| 3 | A | В | A/B | В |
| 10 | В | В | В | В |
| 8 | С | В | A/B | В |

Lab Testing Program Findings – Energy

The energy required to reach the peak shear stress accounts for both the applied stress and the amount of deformation that the sample undergoes before reaching bond failure. For the FT conditioned and one year cores, there is an increase in energy required to reach peak shear stress. SS-1 SB had a consistently low energy rank for all 3 core groups and CSS-1H had a consistently high energy rank for all 3 core groups.



Parameter Comparison – Baseline Cores

| Material | Dilution | ISS Rank | Strain Rank | Failure Type | k Modulus Rank | Energy Rank |
|----------|-------------|----------|-------------|--------------|----------------|-------------|
| SS-1 SB | 50-50W | 10 | 6 | А | 9 | 10 |
| SS-1 NB | 50-50W | 6 | 3 | A | 8 | 5 |
| SS-1 | 30-70W | 7 | 8 | A | 4 | 9 |
| SS-1H SB | 50-50W | 2 | 5 | В | 5 | 3 |
| SS-1H NB | 50-50W | 5 | 10 | В | 1 | 8 |
| MS-1 | 70-30W | 4 | 9 | В | 2 | 6 |
| CSS-1H | 50-50W | 3 | 1 | В | 7 | 1 |
| A | No dilution | 9 | 7 | В | 3 | 7 |
| В | No dilution | 1 | 4 | В | 6 | 2 |
| С | No dilution | 8 | 2 | В | 10 | 4 |

Lab Testing Program Findings

The lab conditioned cores did not show significant degradation in bond behaviour due to FT cycling.

The ISS and energy values are affected by the placement of the core in the inner wheel path (highest), centre of the lane, or outer wheel path (lowest).

•Five parameters including the ISS, strain at bond failure, failure type, k modulus, and energy to bond failure were studied and showed merit in quantifying the quality of bond between two AC layers.

Overall, SS-1H, MS-1, CSS-1H, and the 3 proprietary products showed better performance than SS-1 emulsion according to the test results of the baseline and year one cores.

Research Significance

This research can help Saskatchewan Ministry of Highways & Infrastructure develop and implement performance based specifications for tack coat materials according to bond strength in terms of ISS value, failure type, k modulus, energy, and strain.

With the completion of the study, the change in bond strength between AC layers will be fully characterized and acceptance limits can be established for bond strength of tack coat materials in cold regions.

Future Research

Delayed by Covid-19, will be continued by someone else.

Monitoring of the test sections should continue for at least three more years and should include collection of cores for bond strength testing and field distress surveys.

The FT cycling completed in this study did not cause significant change in bond strength. More research should be completed to investigate the impact of higher number of FT cycling and different methods for sample conditioning.

Further testing of non-tracking proprietary emulsions and products besides SS-1 should be considered as these products appear to have better performance based on year 1 results.

Testing data should include monitoring the placement of core samples in the wheel paths and centre of the lane should be continued because the placement of the cores may yield different results in future testing.

Acknowledgements

Saskatchewan Ministry of Highways & Infrastructure

McAsphalt

Pounder Emulsions (Husky Energy)

Colasphalt

The City of Saskatoon

Research Papers and Presentations Evaluating the Performance of Tack Coat Materials in Saskatchewan Climate Transportation Association of Canada (TAC), Saskatoon, SK, October 2018 Conference Paper & Presentation

Coauthored by Laura Stasiuk, Haithem Soliman, Ania Anthony, Chris Dechkoff, Jen Penner

Characterizing Bond Strength Behaviour of Tack Coat Materials in Saskatchewan Climate

Canadian Technical Asphalt Association (CTAA), Regina, SK, November 2018

Conference Paper

Coauthored by Ania Anthony, Christ Dechkoff, Laura Stasiuk, Haithem Soliman, Nathan Prosko

Effect of Emulsion Type on Bond Behaviour of Asphalt Concrete Layers in Cold Regions

Transportation Research Board (TRB)/Transportation Research Record (TRR), Washington, D.C., January 2019

Conference Presentation & Journal Paper

Coauthored by Laura Stasiuk, Haithem Soliman, Ania Anthony

Tack Coats For Micro-Surfacing Applications

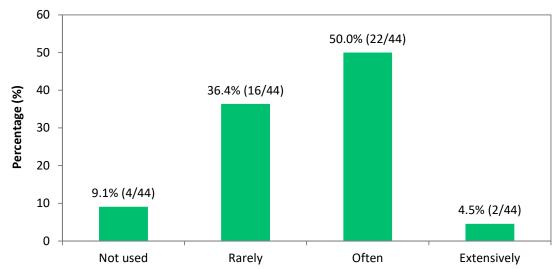


Munir D. Nazzal, Ph.D., P.E. Department of Civil and Architectural Engineering & Construction Management University of Cincinnati

Background

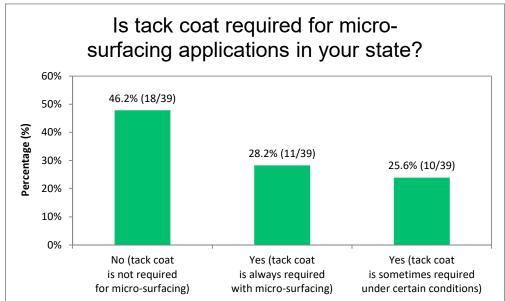


How often is micro-surfacing used by your agency?



Background

- Some DOTs including ODOT currently requires placing a tack coat on the existing pavement.
- Some industry professionals argue that tack coat is not necessary in micro-surfacing applications.



However, there will a risk of premature failure due to poor bonding between the micro-surfacing mix and the existing pavement surface.

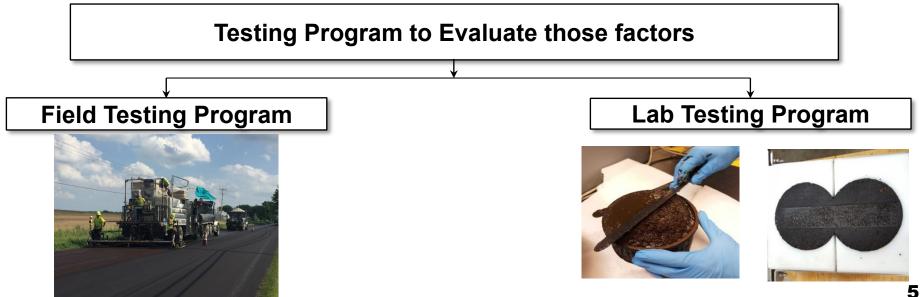


Objectives

- Determine if it is needed to apply tack coat in micro-surfacing applications.
- Identify the factors that affect the interlayer bond strength in micro-surfacing applications.
- Develop a standard test procedure and sample preparation technique for measuring the interface bond strength for micro-surfacing applications after construction.

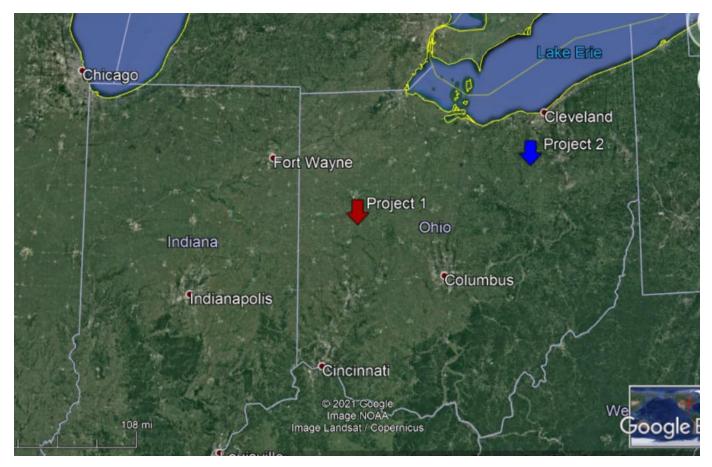
Testing Program

- Different factors can affect the bonding strength between micro-surfacing mix and existing surface:
 - Tack coat application rate
 - Tack coat material type
 - Micro-surfacing mix emulsion content
 - Existing surface conditions



Testing Program

To evaluate the different factors the field testing program included constructing a total of 23 test sections were constructed in two different project in Ohio.



Field Testing Program

Project 1-Single Micro-surfacing layer

| Section | Tack Coat Material Type | Tack Coat Application Rate (g/sy) ^[1] | Residual Asphalt Binder Content of Mix | Road Condition | |
|---------|----------------------------|--|--|----------------|--|
| 1-A | SS-1h | 0.03 | 0.75% Lower | | |
| 1-B | CSS-1hM | 0.03 | Than Typical | Typical Aging | |
| 2 | C33-111M | 0.06 | Design | | |
| 3 | | 0.06 | | | |
| 4 | | 0.1 | | Highly aged | |
| 5 | CSS-1hM | 0.03 | Typical | | |
| 6 | | 0.03 | Design | | |
| 7 | | 0.1 | | Typical Aging | |
| 8 | SS-1H | 0.1 | | | |

Field Testing Program

Project 2-Single Micro-surfacing layer

| Section | Tack Coat | Tack Coat Diluted | Residual Asphalt Binder | | | | |
|---------|---------------|-------------------------|---------------------------------------|--|--|--|--|
| Section | Material Type | Application Rate (g/sy) | Content of Micro-Surfacing Mix | | | | |
| 1 | CSS-1hM | 0.03 | 0.75% lower than typical design | | | | |
| 2 | None | None | | | | | |
| 3 | | 0.03 | | | | | |
| 4 | CSS-1hM | 0.06 | Typical Decign | | | | |
| 5 | | 0.10 | Typical Design | | | | |
| 6 | 66 1h | 0.10 | | | | | |
| 7 | SS-1h | 0.03 | | | | | |

Project 2-Double Micro-surfacing layer

| | Sect | ions on Existing Pavem | Sections on New Leveling Course | | |
|---------|-----------------------|--|-----------------------------------|-----------------------|--|
| Section | Tack Coat Material | Tack Coat Diluted Application Rate (g/sy) | Residual Binder Content of Mix | Tack Coat Material | Tack Coat Diluted Application Rate (g/sy) |
| 8 | CSS-1hM | 0.03 | 0.75% lower than typical design | CSS-1hM | 0.03 |
| 9 | None | None Typical Design | | None | None |
| 10 | | 0.06 | | None | None |
| 11 | CSS-1hM | 0.06 | | | 0.03 |
| 12 | | 0.06 | Typical Design | CSS-1hM | 0.06 |
| 13 | SS1h | 0.06 | | | 0.03 |
| 14 | | 0.06 | | SS1h | 0.06 |

Field Testing Program



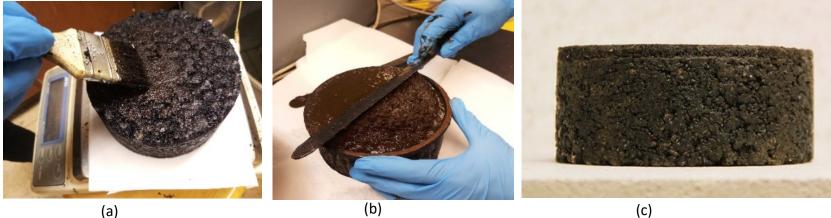
Monitor construction& measure tack coat application rate during construction

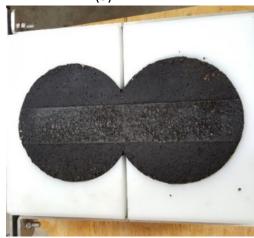
Obtain cores after one week, 3 months & 12 months

Evaluate the different sections after 1 and 2 years

Lab Testing Program

> Micro-surfacing samples were prepared in the lab using the aggregates and emsulsion samples obtained from the field according to field testing matirx.







(e)



(f)

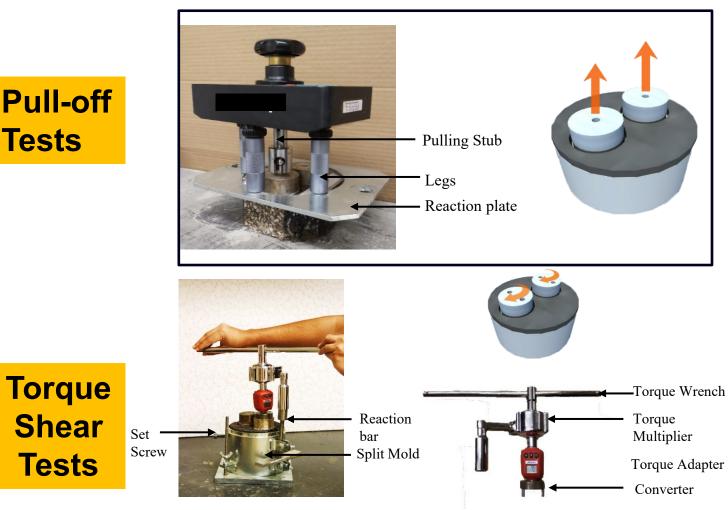
Core and Lab Samples Testing

Two different bond strength tests were performed on the field core samples and the lab prepared samples.

Pull-off Tests

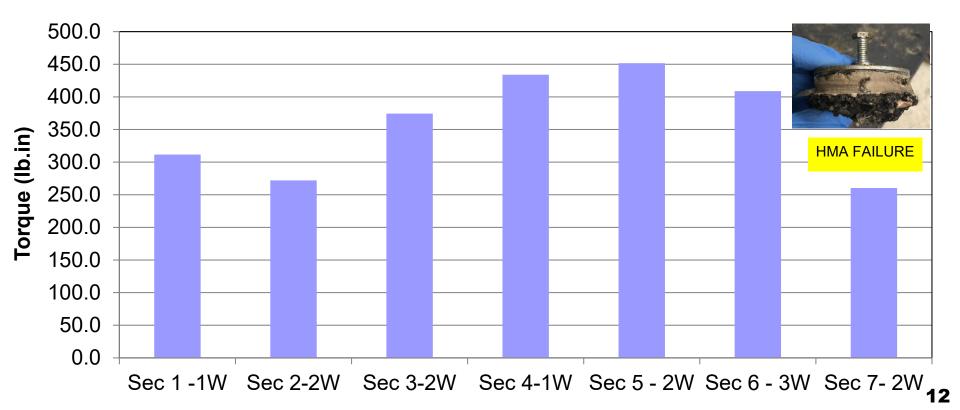
Shear

Tests



Torque Test Results – Cores Obtained after 12 Months

| Sample ID | Sec 1 | Sec 2 | Sec 3 | Sec 4 | Sec 5 | Sec 6 | Sec 7 |
|------------------|---------|-------|---------|---------|---------|-------|-------|
| Em. Cont | 7.05% | 7.8% | 7.8 | 7.8% | 7.8% | 7.8% | 7.8% |
| TC type | CSS-1hM | None | CSS-1hM | CSS-1hM | CSS-1hM | SS-1h | SS-1h |
| TC rate (gsy) | 0.019 | 0 | 0.022 | 0.054 | 0.111 | 0.105 | 0.022 |



Torque Test Results-Cores Obtained after 12 Months

| Sample ID | Sec 1 | Sec 2 | Sec 3 | Sec 4 | Sec 5 | Sec 6 | Sec 7 |
|------------------|---------|-------|---------|---------|---------|-------|-------|
| Em. Cont | 7.05% | 7.8% | 7.8 | 7.8% | 7.8% | 7.8% | 7.8% |
| TC type | CSS-1hM | None | CSS-1hM | CSS-1hM | CSS-1hM | SS-1h | SS-1h |
| TC rate (gsy) | 0.019 | 0 | 0.022 | 0.054 | 0.111 | 0.105 | 0.022 |

| Type 3 Tests of Fixed Effects | | | | | | |
|-------------------------------|-----|-----|---------|--------|--|--|
| | Num | Den | | | | |
| Effect | DF | DF | F Value | Pr > F | | |
| Section | 5 | 11 | 15.61 | 0.0001 | | |

| Section | Estimate | Letter Group |
|---------|----------|--------------|
| 5 | 451.60 | A |
| 4 | 434.00 | A |
| 6 | 408.80 | AB |
| 3 | 374.40 | В |
| 1 | 362.40 | В |
| 2 | 272.00 | С |

Torque Test Results – Overall Comparison

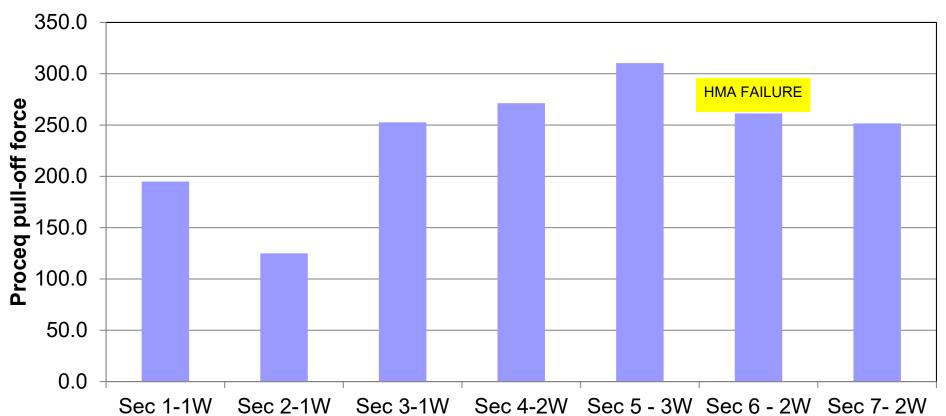
| Effect | Num DF | Den DF | F Value | Pr > F |
|--------------|--------|--------|---------|--------|
| Section | 5 | 33 | 33.87 | <.0001 |
| Time | 2 | 33 | 223.06 | <.0001 |
| Section*Time | 10 | 33 | 9.59 | <.0001 |

| | | Letter |
|---------|----------|--------|
| Section | Estimate | Group |
| 5 | 366.13 | A |
| 6 | 349.20 | AB |
| 4 | 336.80 | В |
| 3 | 300.13 | С |
| 1 | 274.40 | D |
| 2 | 242.31 | E |

| Time | Estimate | Letter Group |
|-----------|----------|-----------------|
| 12 Months | 383.87 | A |
| 4 Months | 334.62 | В |
| One Week | 216.00 | С |

Proceq Test Results – Cores Obtained after 12 Months

| Sample ID | Sec 1 | Sec 2 | Sec 3 | Sec 4 | Sec 5 | Sec 6 | Sec 7 |
|------------------|---------|-------|---------|---------|---------|-------|-------|
| Em. Cont | 7.05% | 7.8% | 7.8 | 7.8% | 7.8% | 7.8% | 7.8% |
| TC type | CSS-1hM | None | CSS-1hM | CSS-1hM | CSS-1hM | SS-1h | SS-1h |
| TC rate (gsy) | 0.019 | 0 | 0.022 | 0.054 | 0.111 | 0.105 | 0.022 |



Proceq Test Results – Cores Obtained after 12 Months

| Sample ID | Sec 1 | Sec 2 | Sec 3 | Sec 4 | Sec 5 | Sec 6 | Sec 7 |
|-----------------------|---------|-------|---------|---------|---------|-------|-------|
| Em. Cont | 7.05% | 7.8% | 7.8 | 7.8% | 7.8% | 7.8% | 7.8% |
| TC type | CSS-1hM | None | CSS-1hM | CSS-1hM | CSS-1hM | SS-1h | SS-1h |
| Res. TC rate (gsy) | 0.019 | 0 | 0.022 | 0.054 | 0.111 | 0.105 | 0.022 |

| Type 3 Tests of Fixed Effects | | | | | | | |
|-------------------------------|----|----|---------|--------|--|--|--|
| Num Den | | | | | | | |
| Effect | DF | DF | F Value | Pr > F | | | |
| Section | 5 | 12 | 18.64 | <.0001 | | | |

| Section | Estimate | Letter Group |
|---------|----------|--------------|
| 5 | 310.33 | A |
| 4 | 271.33 | AB |
| 3 | 252.67 | В |
| 7 | 251.67 | В |
| 1 | 195.00 | С |
| 2 | 125.00 | D |

Proceq Test Results – Cores Obtained after 12 Months

| Type 3 Tests of Fixed Effects | | | | | | | | |
|-------------------------------|--------|--------|---------|--------|--|--|--|--|
| Effect | Num DF | Den DF | F Value | Pr > F | | | | |
| Section | 5 | 36 | 31.05 | <.0001 | | | | |
| Time | 2 | 36 | 199.05 | <.0001 | | | | |
| Section*Time | 10 | 36 | 8.26 | <.0001 | | | | |

| | | Letter |
|---------|----------|--------|
| Section | Estimate | Group |
| 5 | 241.11 | А |
| 4 | 224.33 | AB |
| 7 | 209.33 | BC |
| 3 | 196.78 | С |
| 1 | 178.78 | D |
| 2 | 147.44 | E |

| | | Letter |
|-----------|----------|--------|
| Time | Estimate | Group |
| 12 Months | 234.33 | A |
| 4 Months | 234.06 | A |
| One Week | 130.50 | В |

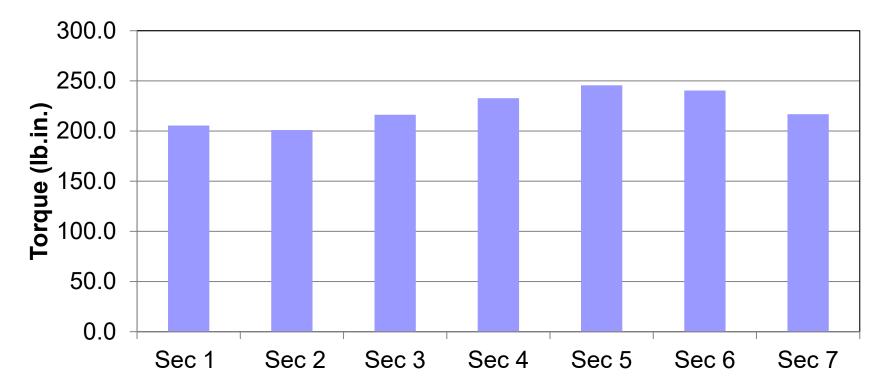
Proceq Test Results – Effect of Tack Coat Type& Rate

| | Num | Den | | |
|----------------|-----|-----|---------|------------------|
| Effect | DF | DF | F Value | Pr > F |
| Tack coat type | 1 | 6 | 0.00 | 0.9518 |
| Tack coat rate | 1 | 6 | 13.21 | 0.0109 |

| | | | Standard | Letter |
|--------|-----|----------|----------|--------|
| ТСТ | TCR | Estimate | Error | Group |
| CSS1hm | Н | 310.33 | 11.2200 | А |
| CSS1hm | L | 252.67 | 11.2200 | В |
| SS1h | L | 251.67 | 11.2200 | В |

Torque Test Results – Lab Prepared Samples

| Sample ID | Sec 1 | Sec 2 | Sec 3 | Sec 4 | Sec 5 | Sec 6 | Sec 7 |
|------------------|-------------|-------|---------|---------|---------|-------|-------|
| Em. Cont | 7.05% | 7.8% | 7.8 | 7.8% | 7.8% | 7.8% | 7.8% |
| TC type | CSS- 1hm | None | CSS-1hm | CSS-1hm | CSS-1hm | SS-1h | SS-1h |
| TC rate (gsy) | 0.025 | 0 | 0.025 | 0.06 | 0.108 | 0.108 | 0.025 |



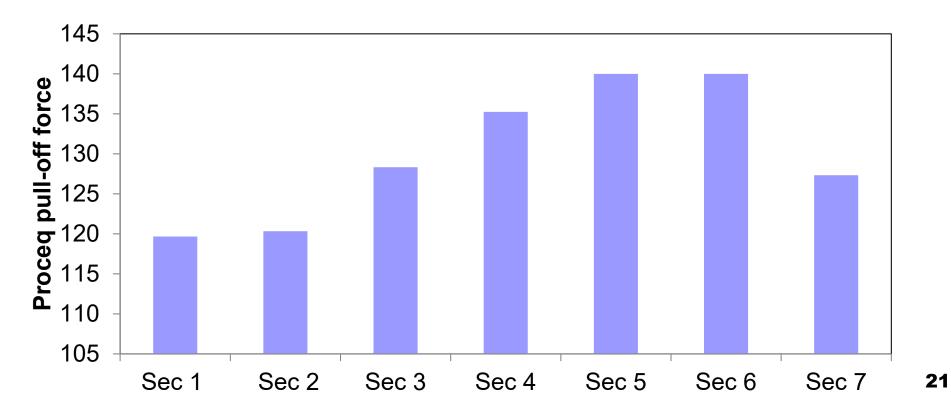
Torque Test Results – Lab Prepared Samples

| Sample ID | Sec 1 | Sec 2 | Sec 3 | Sec 4 | Sec 5 | Sec 6 | Sec 7 |
|------------------|-------------|-------|---------|---------|---------|-------|-------|
| Em. Cont | 7.05% | 7.8% | 7.8 | 7.8% | 7.8% | 7.8% | 7.8% |
| TC type | CSS- 1hm | None | CSS-1hm | CSS-1hm | CSS-1hm | SS-1h | SS-1h |
| TC rate (gsy) | 0.025 | 0 | 0.025 | 0.06 | 0.108 | 0.108 | 0.025 |

| Section | Estimate | Letter Group |
|---------|----------|--------------|
| Sec 5 | 245.60 | А |
| Sec 6 | 240.40 | А |
| Sec 4 | 232.80 | В |
| Sec 7 | 216.80 | BC |
| Sec 3 | 216.30 | BC |
| Sec 1 | 205.50 | С |
| Sec 2 | 201.00 | С |

Proceq Test Results – Lab Prepared Samples

| Sample ID | Sec 1 | Sec 2 | Sec 3 | Sec 4 | Sec 5 | Sec 6 | Sec 7 |
|------------------|-------------|-------|---------|---------|---------|-------|-------|
| Em. Cont | 7.05% | 7.8% | 7.8 | 7.8% | 7.8% | 7.8% | 7.8% |
| TC type | CSS- 1hm | None | CSS-1hm | CSS-1hm | CSS-1hm | SS-1h | SS-1h |
| TC rate (gsy) | 0.025 | 0 | 0.025 | 0.06 | 0.108 | 0.108 | 0.025 |



Proceq Test Results – Lab Prepared Samples

| Sample ID | Sec 1 | Sec 2 | Sec 3 | Sec 4 | Sec 5 | Sec 6 | Sec 7 |
|------------------|-------------|-------|---------|---------|---------|-------|-------|
| Em. Cont | 7.05% | 7.8% | 7.8 | 7.8% | 7.8% | 7.8% | 7.8% |
| TC type | CSS- 1hm | None | CSS-1hm | CSS-1hm | CSS-1hm | SS-1h | SS-1h |
| TC rate (gsy) | 0.025 | 0 | 0.025 | 0.06 | 0.108 | 0.108 | 0.025 |

| Section | Estimate | Letter Group |
|---------|----------|--------------|
| Sec 5 | 140.00 | А |
| Sec 6 | 140.00 | A |
| Sec 4 | 135.25 | A |
| Sec 3 | 128.33 | AB |
| Sec 7 | 127.33 | AB |
| Sec 2 | 120.33 | В |
| Sec 1 | 119.67 | В |

Findings

- The results of bond strength tests conducted on the samples obtained from the field test section indicated that, at 95% confidence level, the sections with no tack coat had significantly lower bond strength than those with tack coat with least 0.06 gsy application rate (0.01 gsy residual application rate).
- The results indicated that, at 95% confidence level, the use of 0.75% lower residual asphalt binder content in micro-surfacing mix resulted in significantly lower bond strength between the micro-surfacing and existing pavement.

Findings

➤ The results indicated that increasing the tack coat application rate resulted in improving the bond strength. However, the improvement was not significant when the total application was higher than 0.06 gsy (0.01 gsy residual application rate).

Questions?





Today's Panelists #TRBWebinar

Moderator: Danny Gierhart, Asphalt Institute



Louay Mohammad, Louisiana State University



Laura Stasiuk, University of Saskatchewan



Munir Nazzal, University of Cincinnati

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