

TRANSPORTATION RESEARCH BOARD

# TRB Webinar: Innovations in Testing—Modified Binders Cracking Resistance

**May 25, 2022**

**2:30- 4:00 PM Eastern**

**@NASEMTRB**  
**#TRBwebinar**

# PDH Certification Information:

- 1.5 Professional Development Hours (PDH) – see follow-up email for instructions
- You must attend the entire webinar to be eligible to receive PDH credits
- Questions?  
[trbwebinar@nas.edu](mailto:trbwebinar@nas.edu)

**#TRBwebinar**

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**REGISTERED CONTINUING EDUCATION PROGRAM**

# Learning Objectives

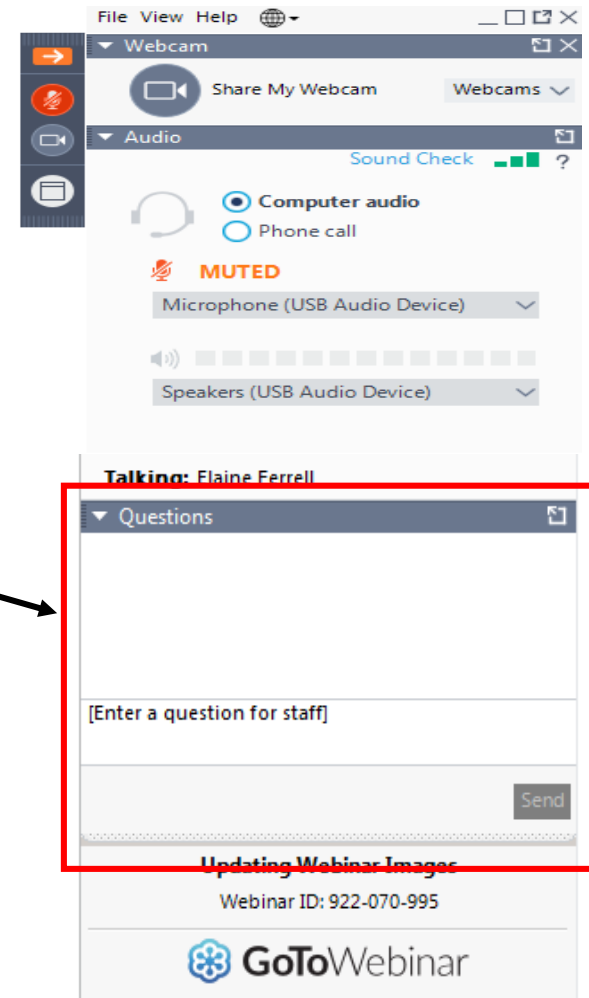
- Use and apply emerging intermediate temperature tests to characterize the benefits of modified binders using existing laboratory equipment

**#TRBwebinar**



# Questions and Answers

- Please type your questions into your webinar control panel
- We will read your questions out loud, and answer as many as time allows



**#TRBwebinar**



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# A new ductility test for asphalt binders considering a realistic triaxial stress state

Ramez Hajj, Ph.D.

Assistant Professor

University of Illinois at Urbana-Champaign

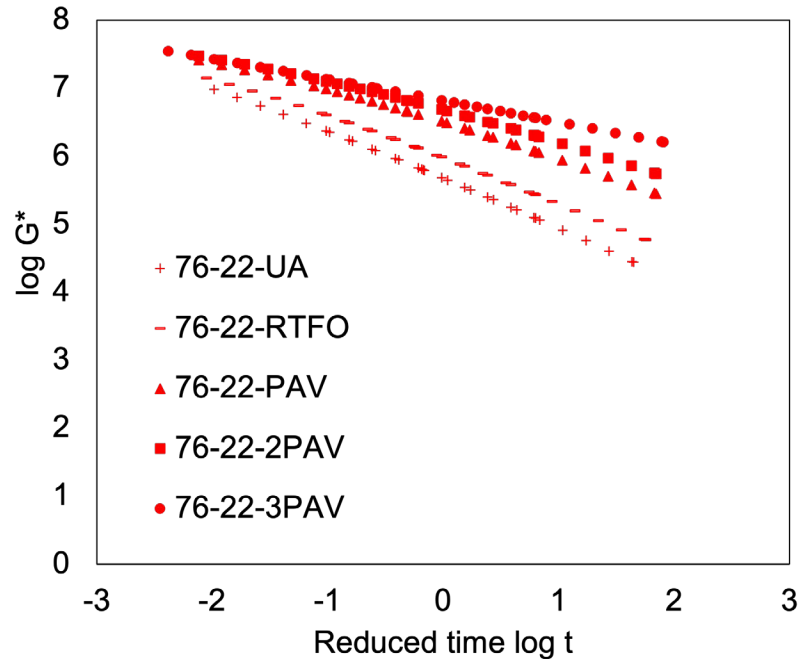
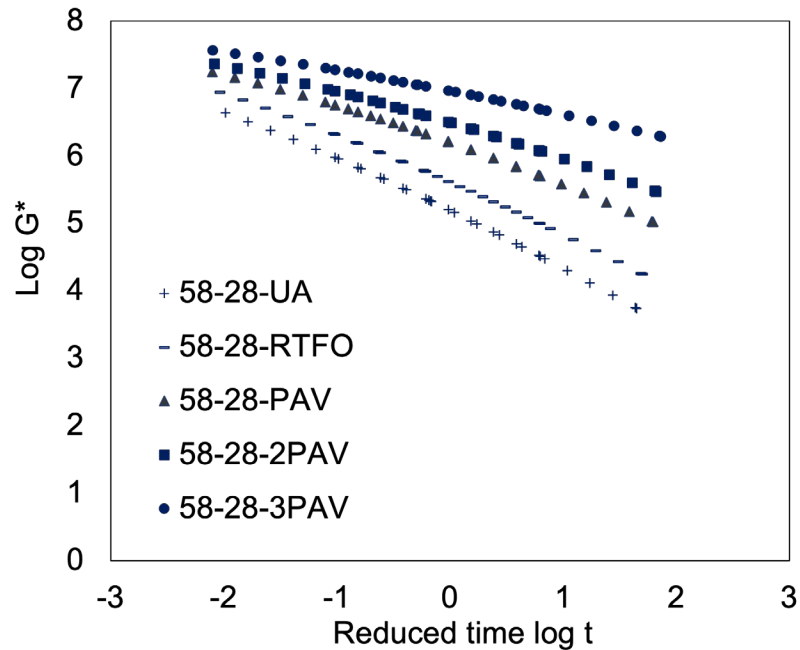
TRB Webinar 05/25/2022

# Disclaimer

- This presentation represents my views only; not the views of any sponsor or agency.

# What we know

- Aging increases stiffness; modification often does too



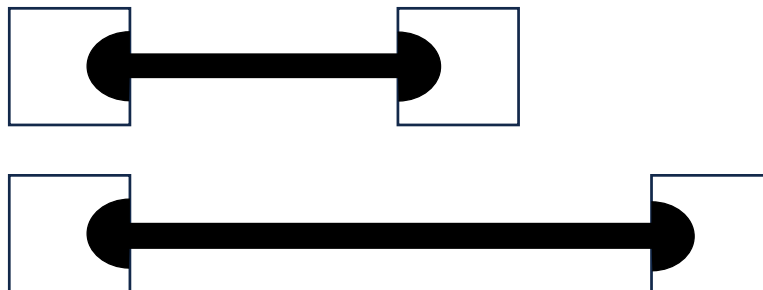


# Polymer-modified asphalt cracking

- **Why do LVE cracking indicators not hold up for polymer modified asphalt?**
  - Block copolymers have a fundamentally different deformation mechanism
  - Polymer generally increases stiffness – can muddle LVE properties
  - Original studies linking binder ductility to asphalt field cracking are from the 1950s! This does not apply to today's binders.
  - We are using only linear viscoelastic behavior to link to nonlinear phenomena. We use MSCR at high temperature to predict plastic deformation for this reason.

# The “old” ductility test

- Issues first noted by Saal (1955)
  - Large temperature rise during stretching and thixotropic effects from structural breakdown cast doubt on test’s significance
- Later, Tabatabaee et al. (2013) observed lack of correlation with cracking and issues capturing ductility of polymer-modified asphalt.

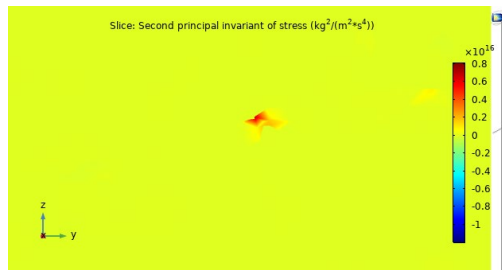
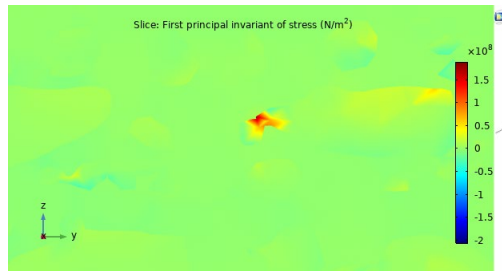


# Importance of triaxiality

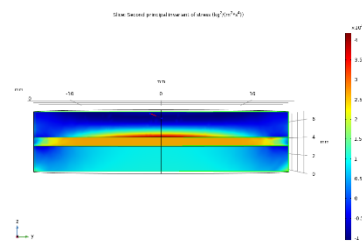
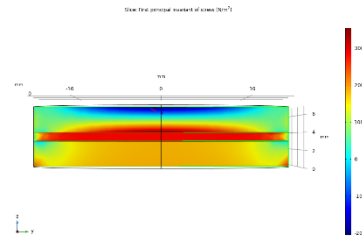
$$\text{Triaxiality} = \frac{\text{Hydrostatic Stress}}{\text{Von Mises Stress}}$$

- Concept explored on and off for asphalt materials over the years
- Higher triaxiality leads to more brittle failure
- Observed in composites, etc. at interfaces between inclusions
- Review of polymer literature indicates that ductility tests cannot be considered accurate without considering stress state

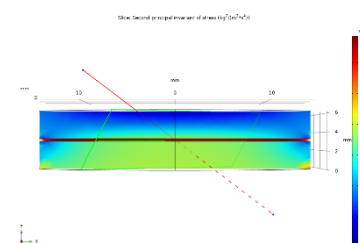
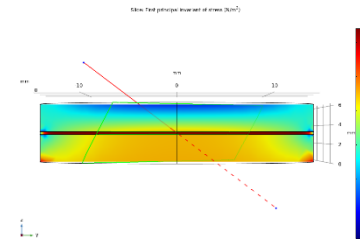
# Stress state observed in asphalt mixes



Aspect Ratio = 15

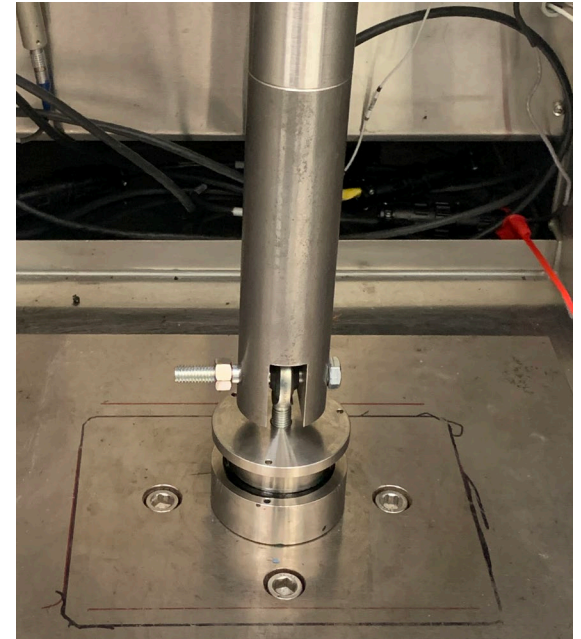
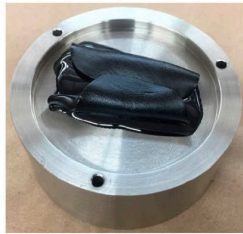


Aspect Ratio = 50

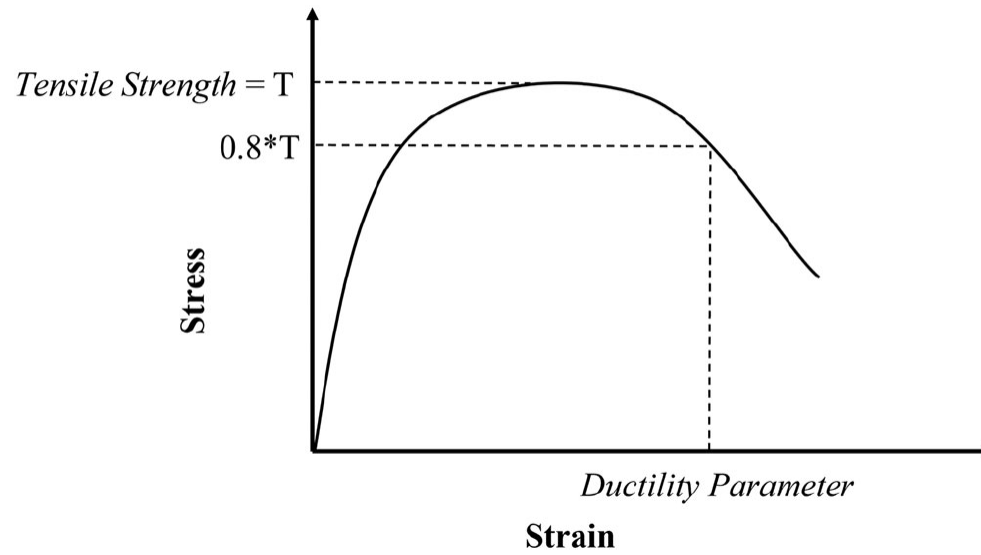


# Alternative for ductility testing

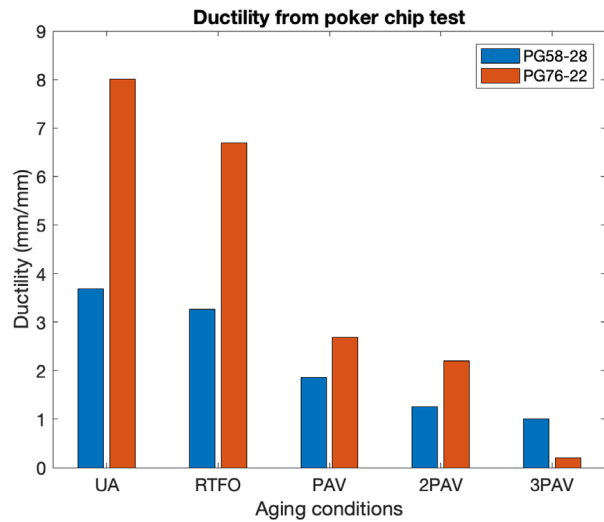
- Poker chip test



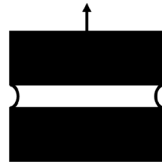
# Typical Test Result



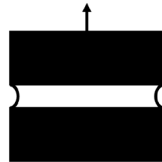
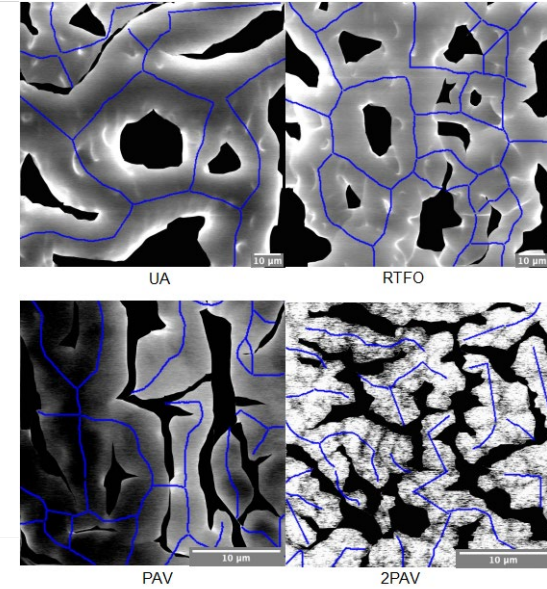
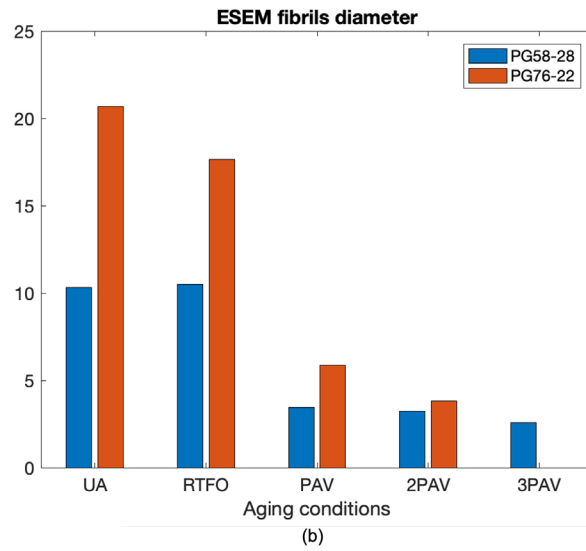
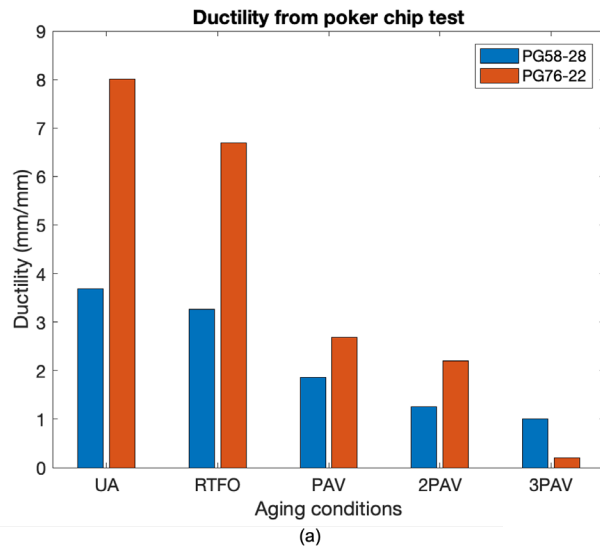
# Modified vs. Unmodified



(a)



# Modified vs. Unmodified



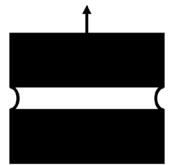
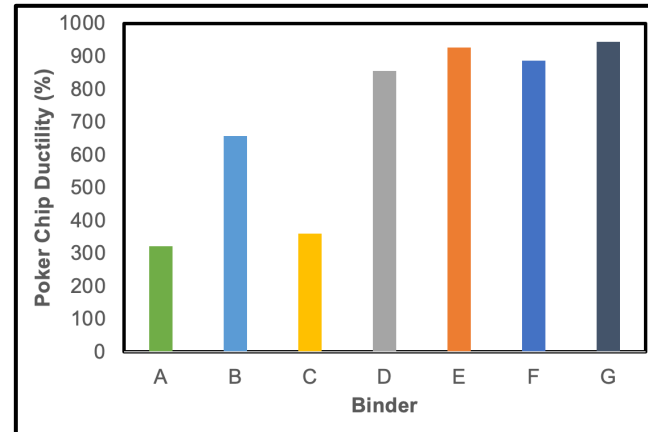
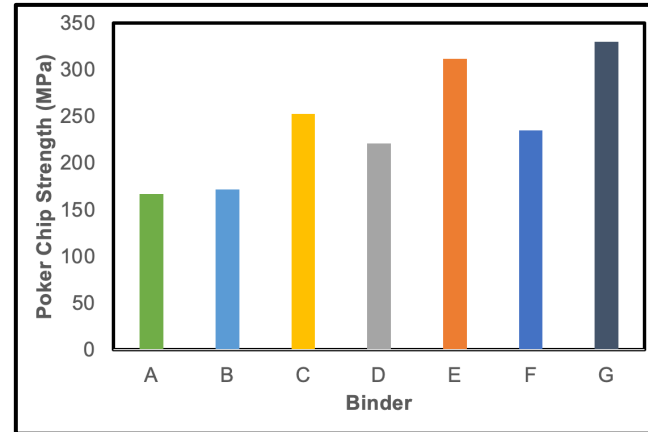


# Another Example

| UTI $\geq$ 92 $\rightarrow$ Modified |          |
|--------------------------------------|----------|
| Symbol                               | Grade    |
| A                                    | PG 58-28 |
| B                                    | PG 64-28 |
| C                                    | PG 64-22 |
| D                                    | PG 70-28 |
| E                                    | PG 70-22 |
| F                                    | PG 76-28 |
| G                                    | PG 76-22 |

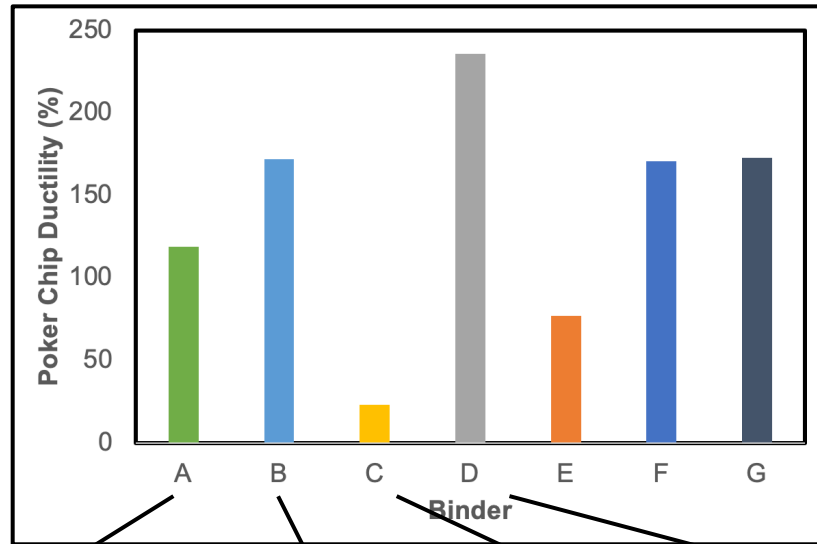
# Another Example

| UTI $\geq$ 92 $\rightarrow$ Modified |          |
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| C                                    | PG 64-22 |
| D                                    | PG 70-28 |
| E                                    | PG 70-22 |
| F                                    | PG 76-28 |
| G                                    | PG 76-22 |



# Low Temperature

| UTI $\geq$ 92 $\rightarrow$ Modified |          |
|--------------------------------------|----------|
| Symbol                               | Grade    |
| A                                    | PG 58-28 |
| B                                    | PG 64-28 |
| C                                    | PG 64-22 |
| D                                    | PG 70-28 |
| E                                    | PG 70-22 |
| F                                    | PG 76-28 |
| G                                    | PG 76-22 |



# However, PG is not always related

- Consider the same base binder, modified with two different polymers, same dosage (intermediate temp):

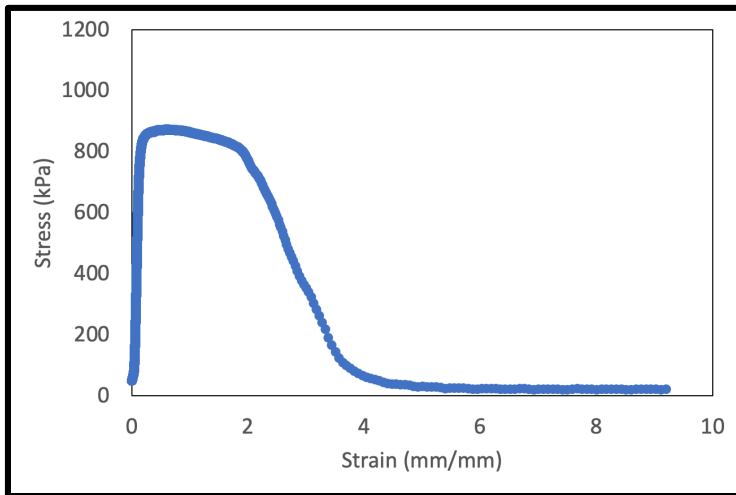
Binder 1 – PG 76-16

Binder 2 – PG 76-22

# However, PG is not always related

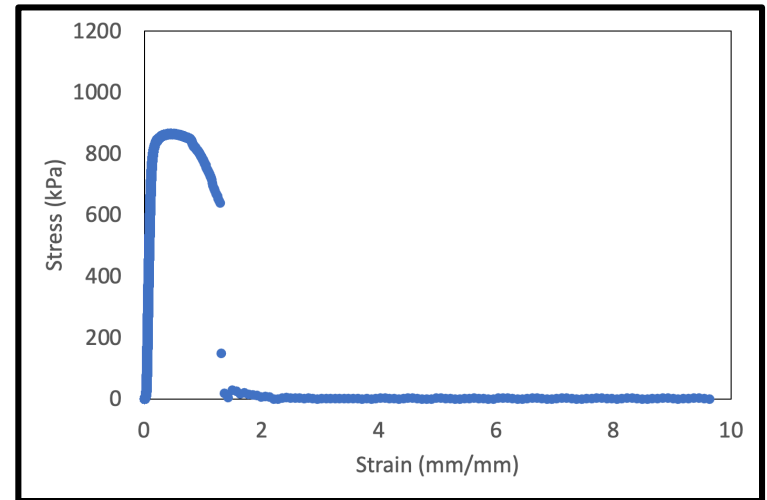
- Consider the same base binder, modified with two different polymers, same dosage (intermediate temp):

Binder 1 – PG 76-16

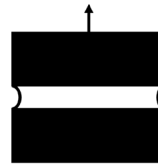


Average poker chip ductility = 297%

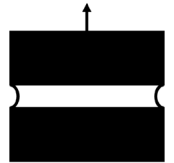
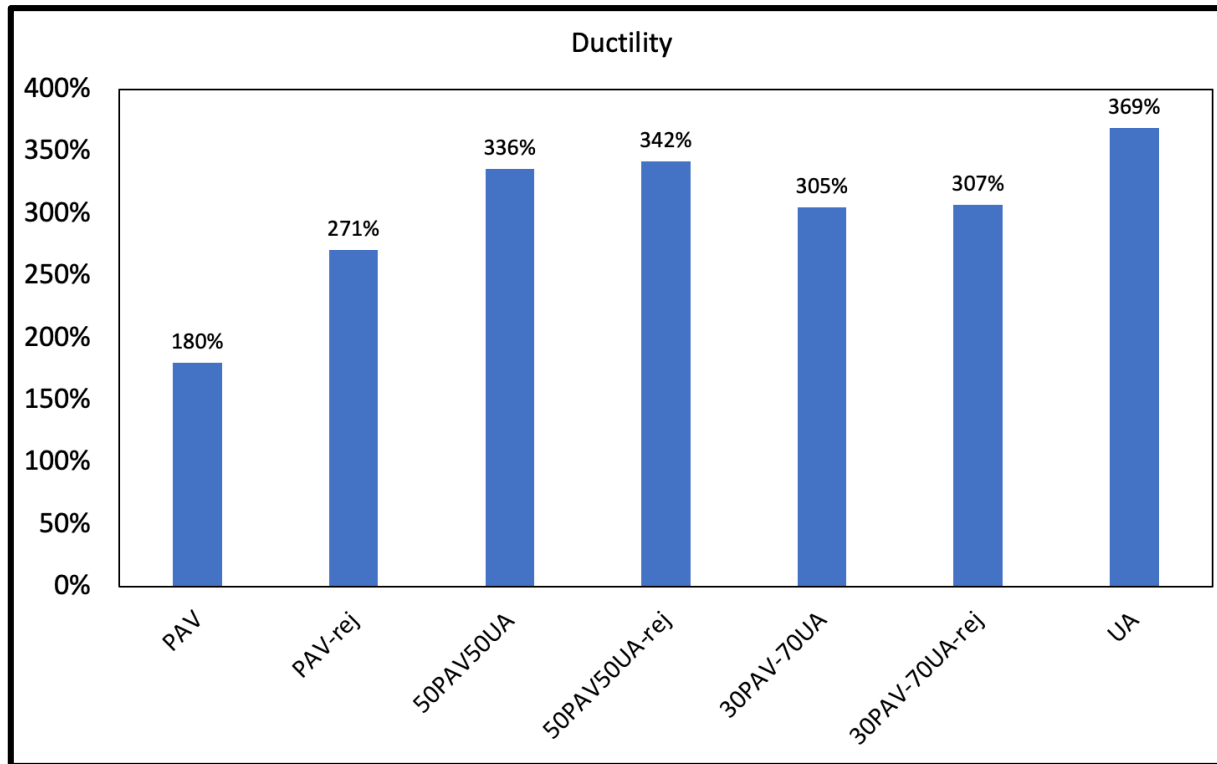
Binder 2 – PG 76-22



Average poker chip ductility = 115%



# Effect of bio-oil rejuvenator



# Conclusions


- Over the years, many LVE indicators have come and gone; aging is often used to justify them but fails to hold up for modified binders
- The traditional ductility test, and any test that does not consider stress state, are insufficient to characterize modified asphalt.
- Poker chip test is sensitive to a range of modifiers and is future proof due to its fundamental nature
- Poker chip test is easy to run, and data is easy to interpret

# Acknowledgements

- Thank you to our sponsors- BASF SE and the Smart Transportation Infrastructure Initiative
- Thank you to my excellent students for their contributions- Yujia Lu, Renan Santos Maia, Babak Asadi, Abhilash Vyas, and Yudi Wang
- Thank you to Amit Bhasin and his research team for their contributions and continued collaboration




Questions?



TRB Webinar: Innovations in  
Testing—Modified Binders  
Cracking Resistance

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N. “Wasi” Wasiuddin  
Professor, Louisiana Tech University



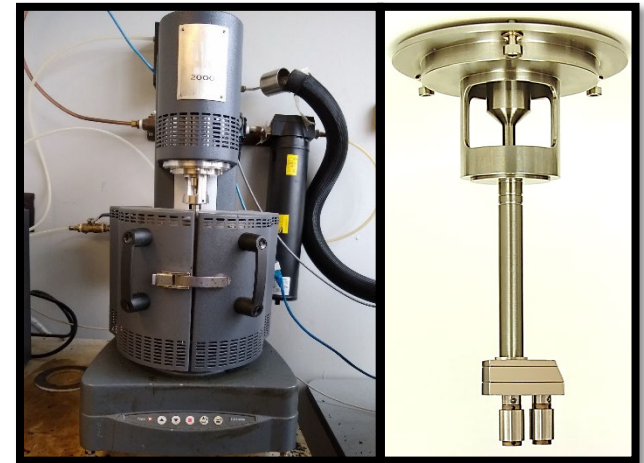
**Subtopic:  
A Novel DSR-Based Force  
Ductility Test Method**

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- Knowledge Gap:
  - Ductility of modified binders
  - Oxidation and corresponding degradation of modifiers

# Advantages of using Sentmanat External Rheometer (SER) Fixture in DSR

- SER can be accommodated in currently used DSR models
- From one DSR mold sample more than 15 SER samples can be prepared
- Results more reflective of the material response
  - Length of the sample remains constant providing true strain
  - Cross sectional area of the sample is assumed not varying throughout the sample length proving true stress
- More precision and wider range in temperature and force



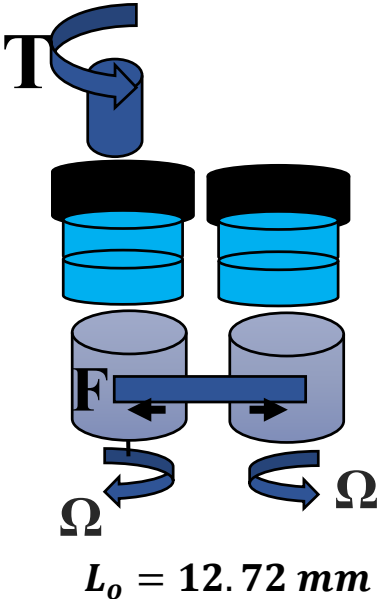
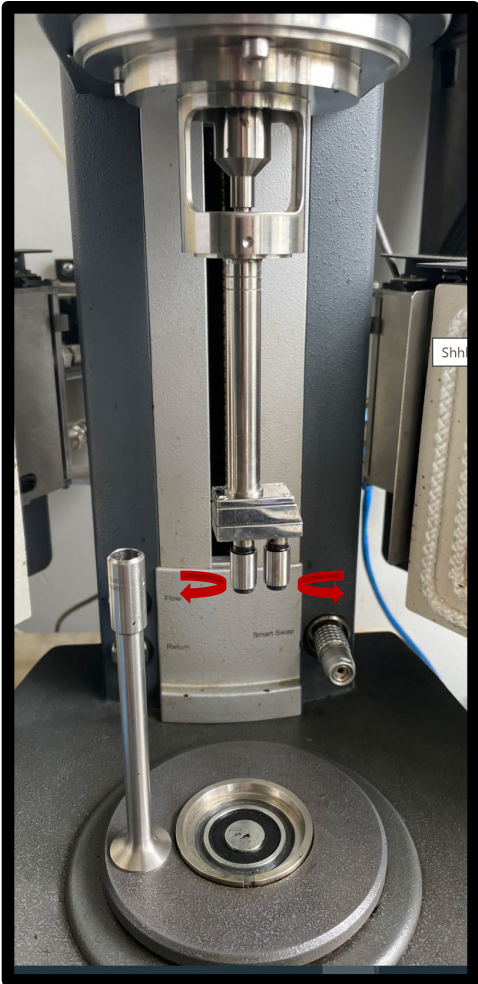
**SER Fixture**

## **With This Test Method We Will:**

- Compare the effectiveness of different types of modifications
- Investigate the  $F_2$  value of stiffer binder due to aging
- Determine the degradation of modifiers due to aging
- Investigate the effect of UV aging on degradation of SBS

# How It Works:

A Sentmanat  
Extensional  
Rheometer  
(SER) fixture  
was introduced  
for modified  
asphalt binder  
characterization



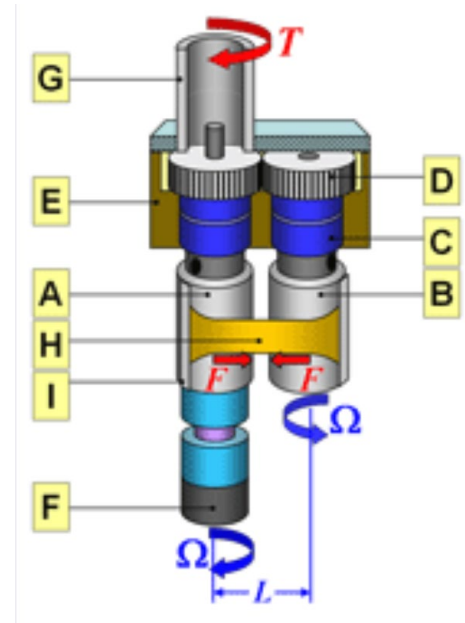
# How It Works:

Hencky Strain Rate:

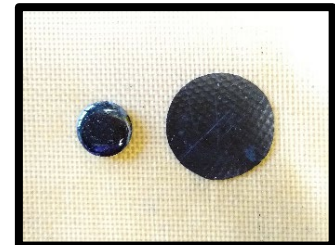
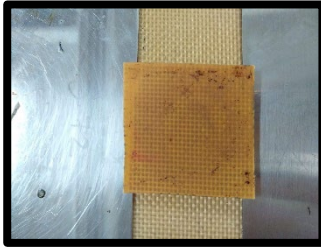
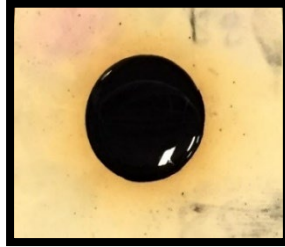
$$d\epsilon_H/dt = 2 \Omega R/L_0$$

Instantaneous X-Sectional Area:

$$A(t) = A_0 \exp[- (d\epsilon_H/dt) t]$$

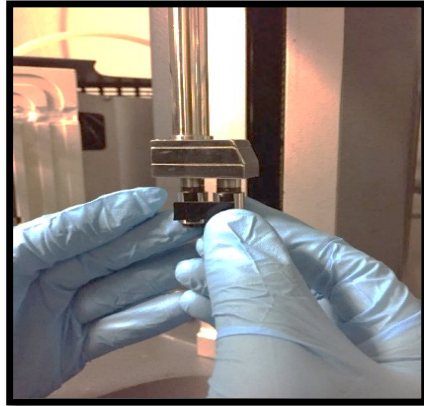


# Sample Preparation:





## Sample Preparation:





**SBS Polymer**

Binder is in a quarter-gallon container and polymer is being mixed with it.

Precise Temperature Controller

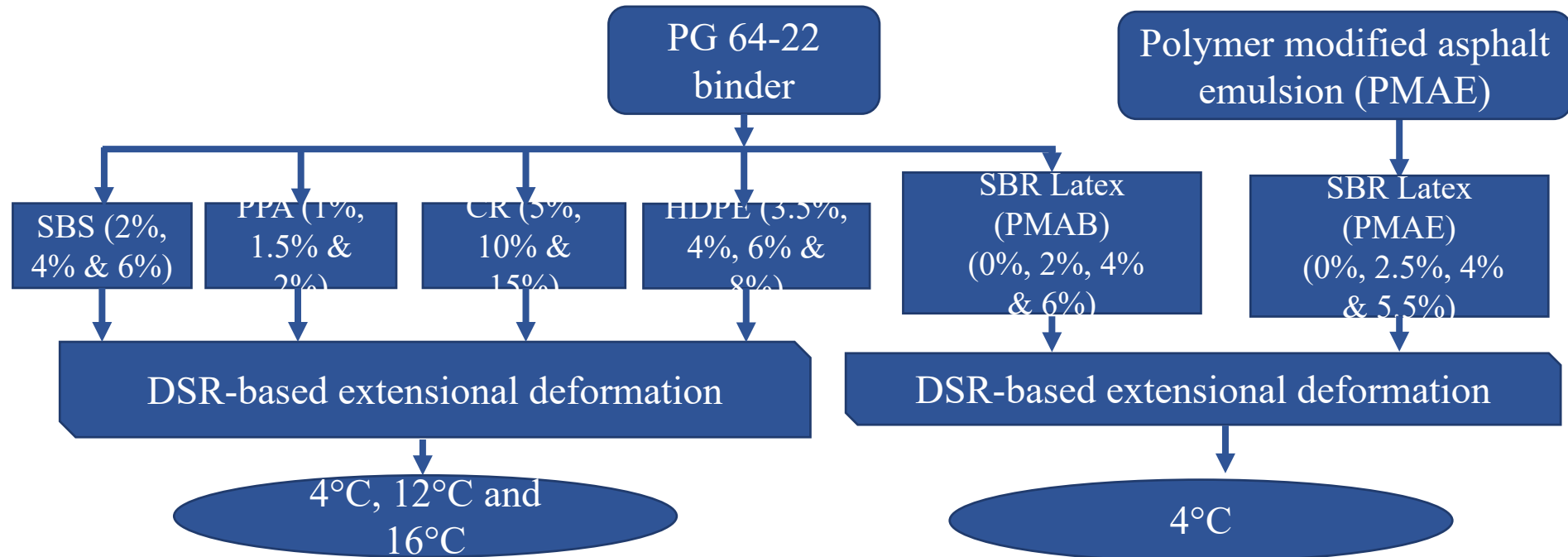
Glas-Col Heating Mantel capable of heating up to 450°C.



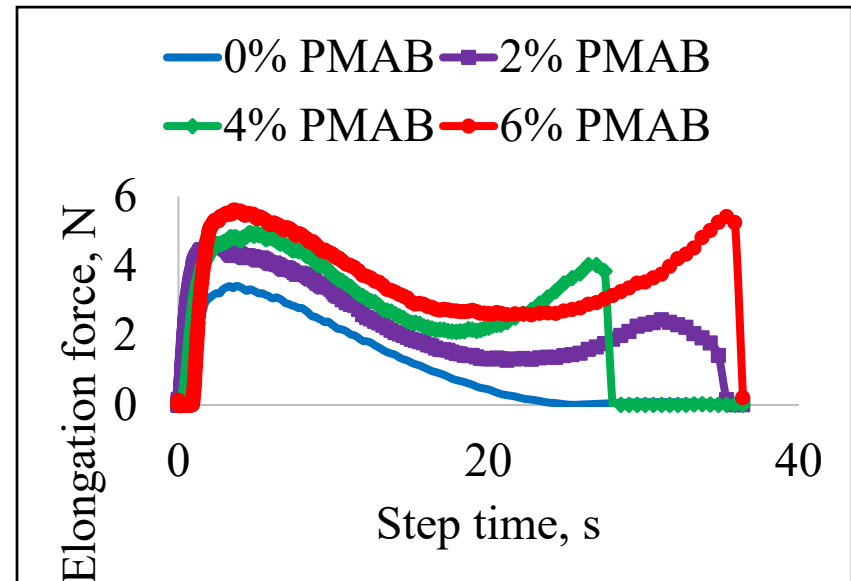
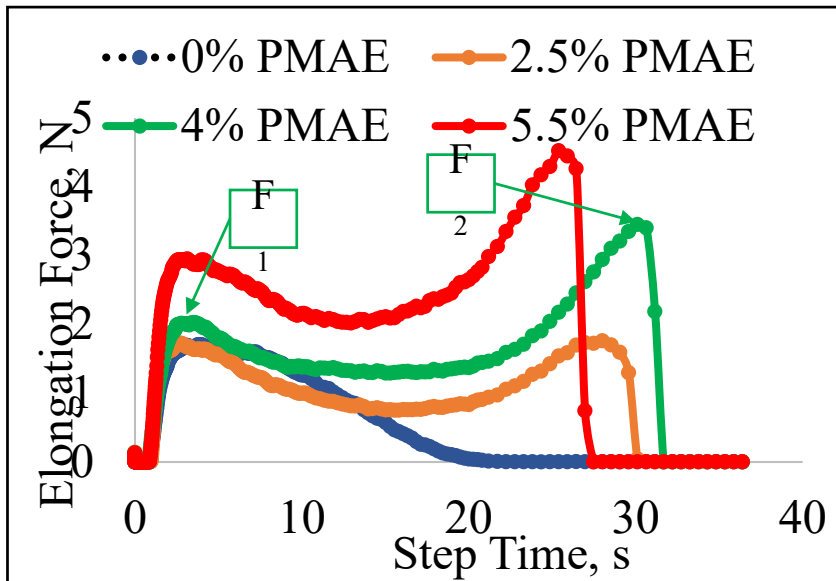
**Mixing of SBS with asphalt binder by a hand drill**

## Mixing of Polymer with Binder by A High Shear Mixer

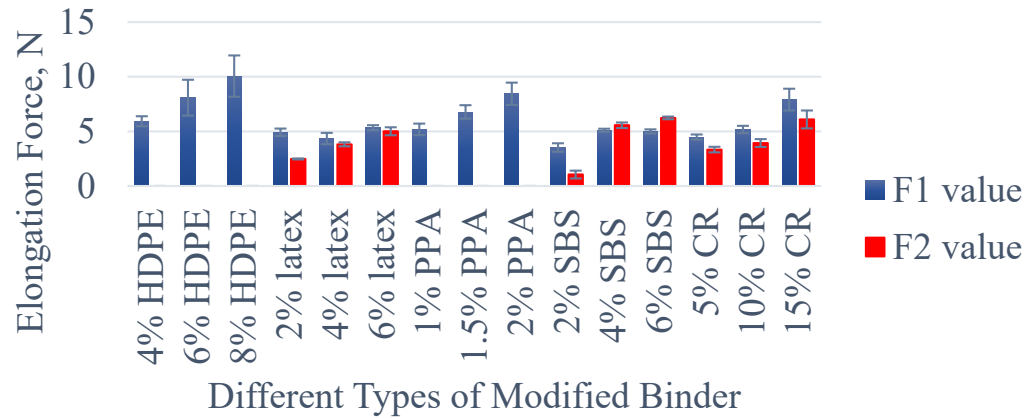
## Test Factorial: Identification and Determination of Elastomeric Polymer Content



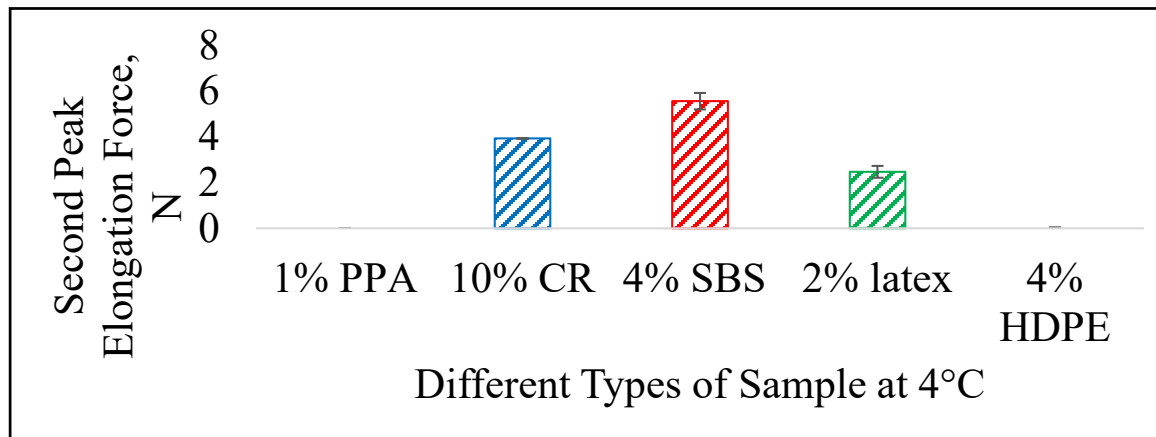
## Elongation Force vs Step Time Curve Characterization



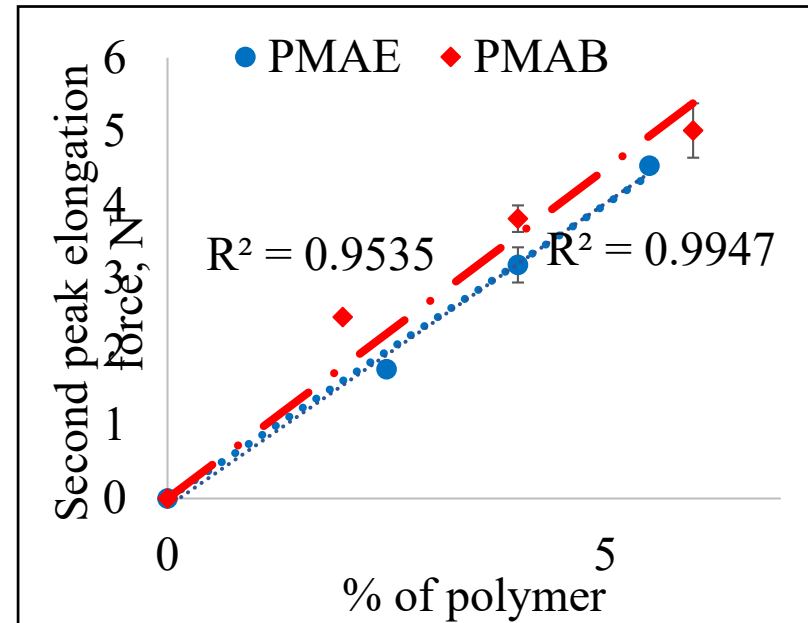
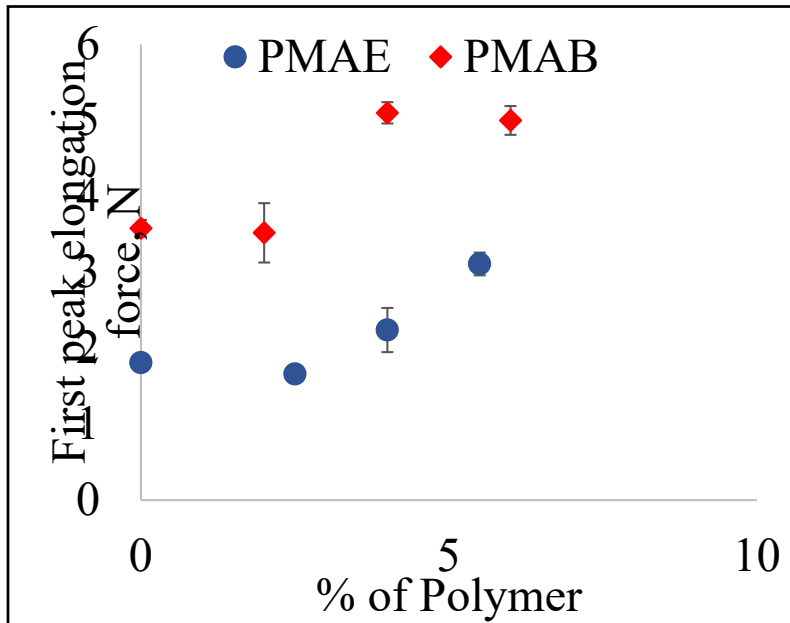
## F<sub>2</sub> at Similar Stiffness



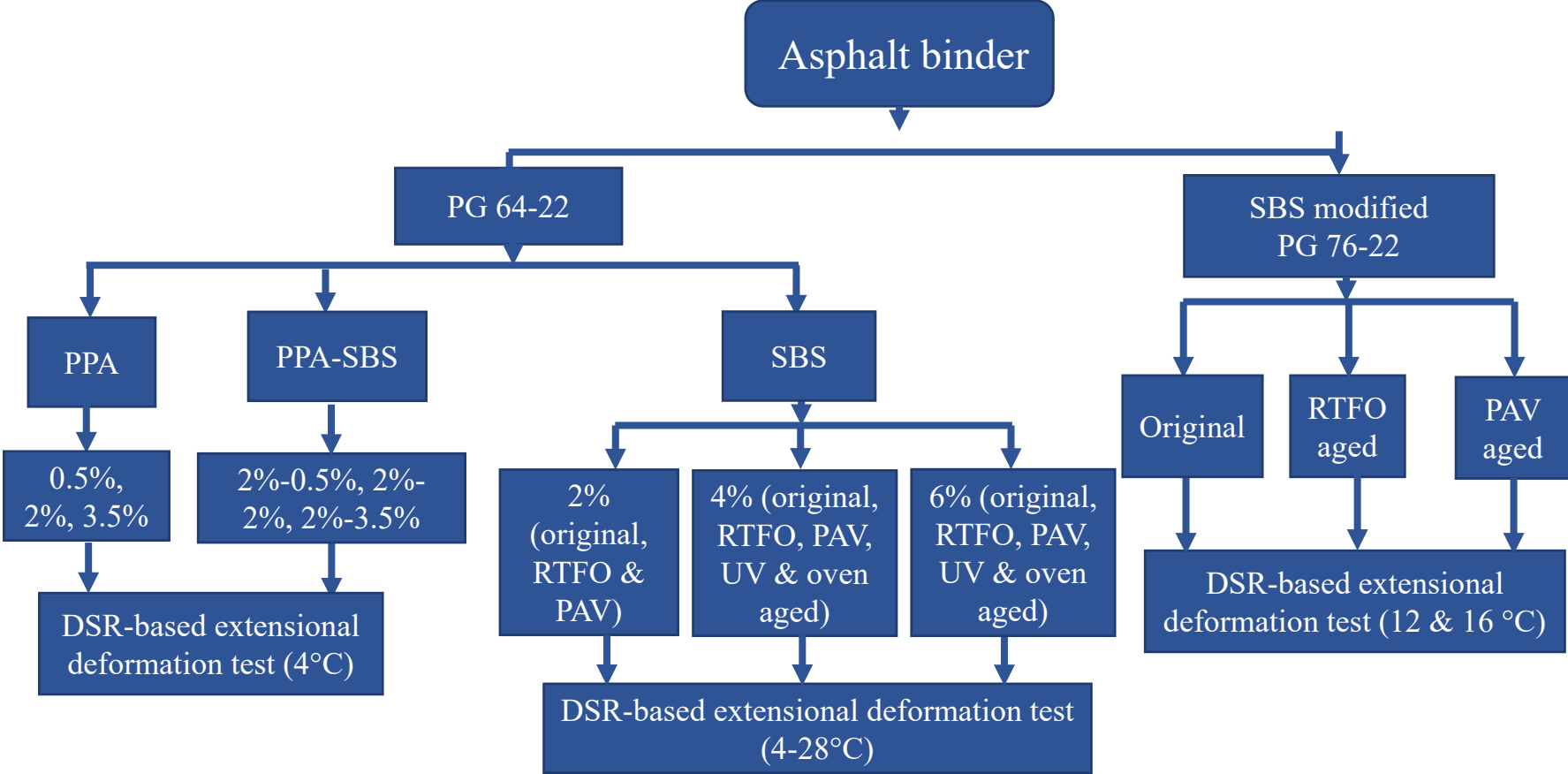
| Modified Binder | F <sub>1</sub> value at 4°C |
|-----------------|-----------------------------|
| 1% PPA          | 5.18                        |
| 10% CR          | 5.17                        |
| 4% SBS          | 5.1                         |
| 2% latex        | 4.92                        |
| 4% HDPE         | 4.93                        |



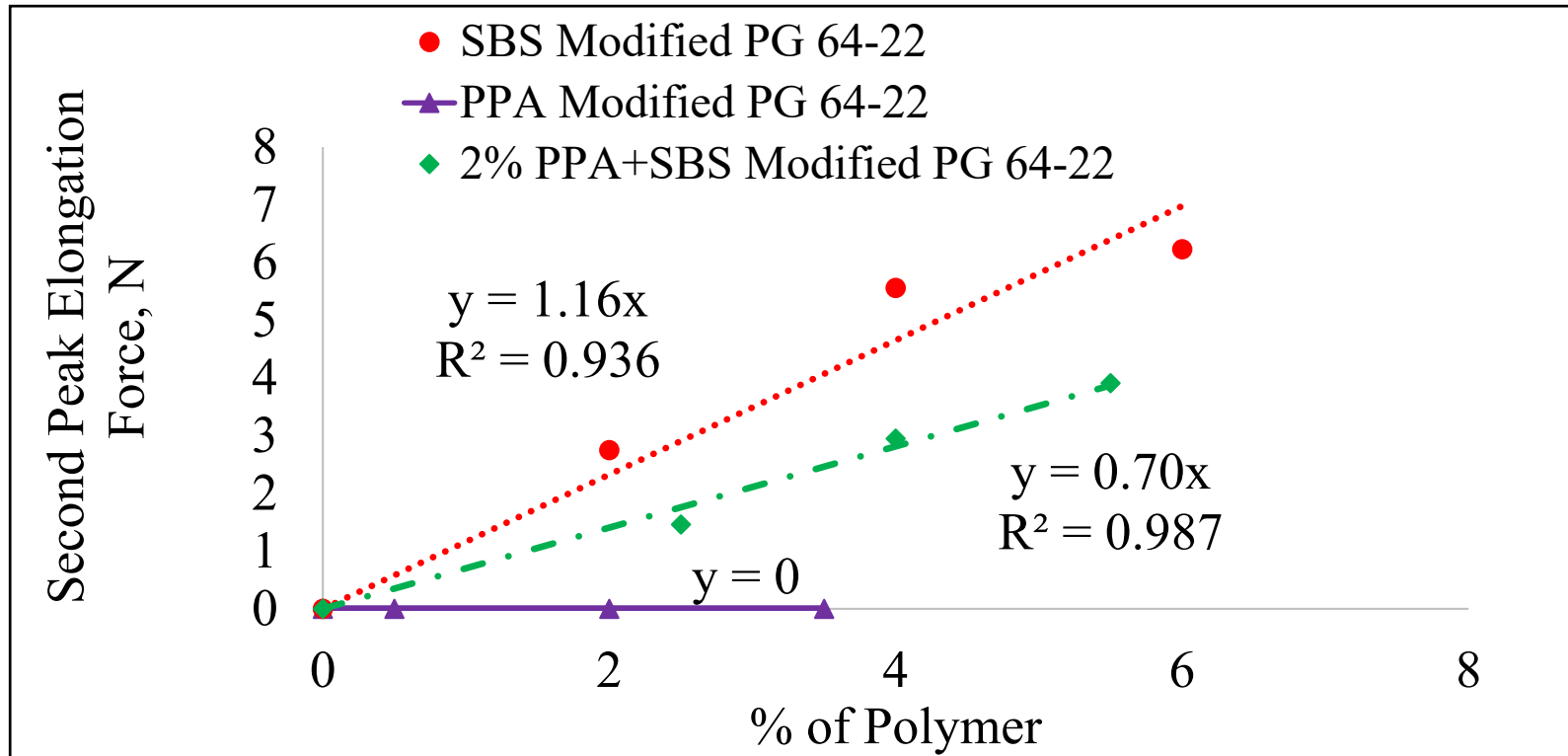
## Elongation Force and Percent of Polymer



# Test Factorial: Evaluating SBS Degradation due to Aging of Binder



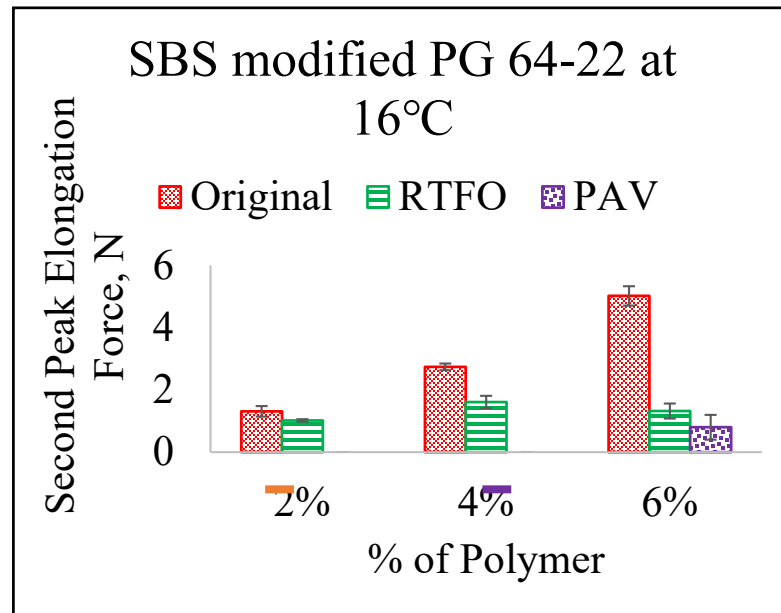
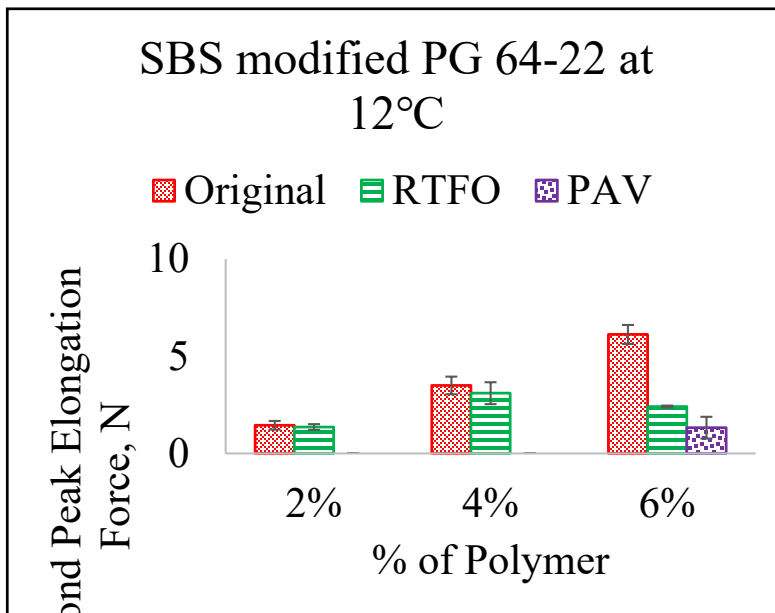
## Second Peak Elongation Force vs. Percent of Polymer





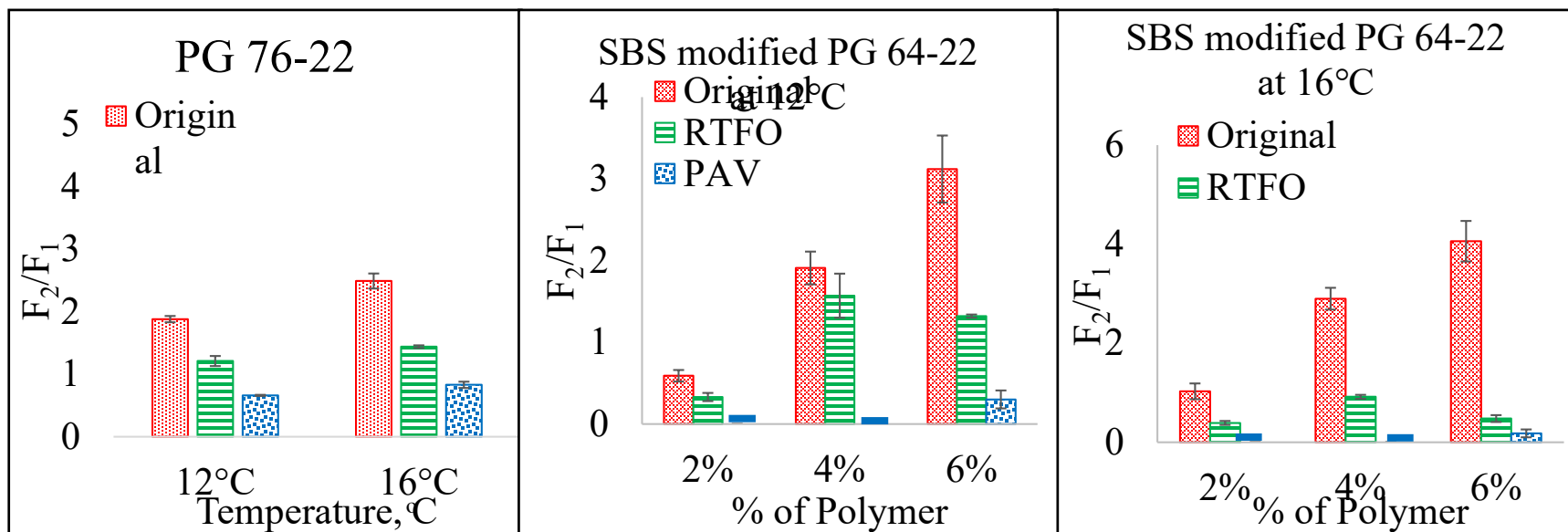
## Second Peak Elongation Force of Different Percent of Polymer

- High stiffness- sample breaks – no  $F_2$
- Increasing of test temperature (up to 28°C).
- 7-60% reduction after RTFO aging
- 79-100% reduction after PAV aging

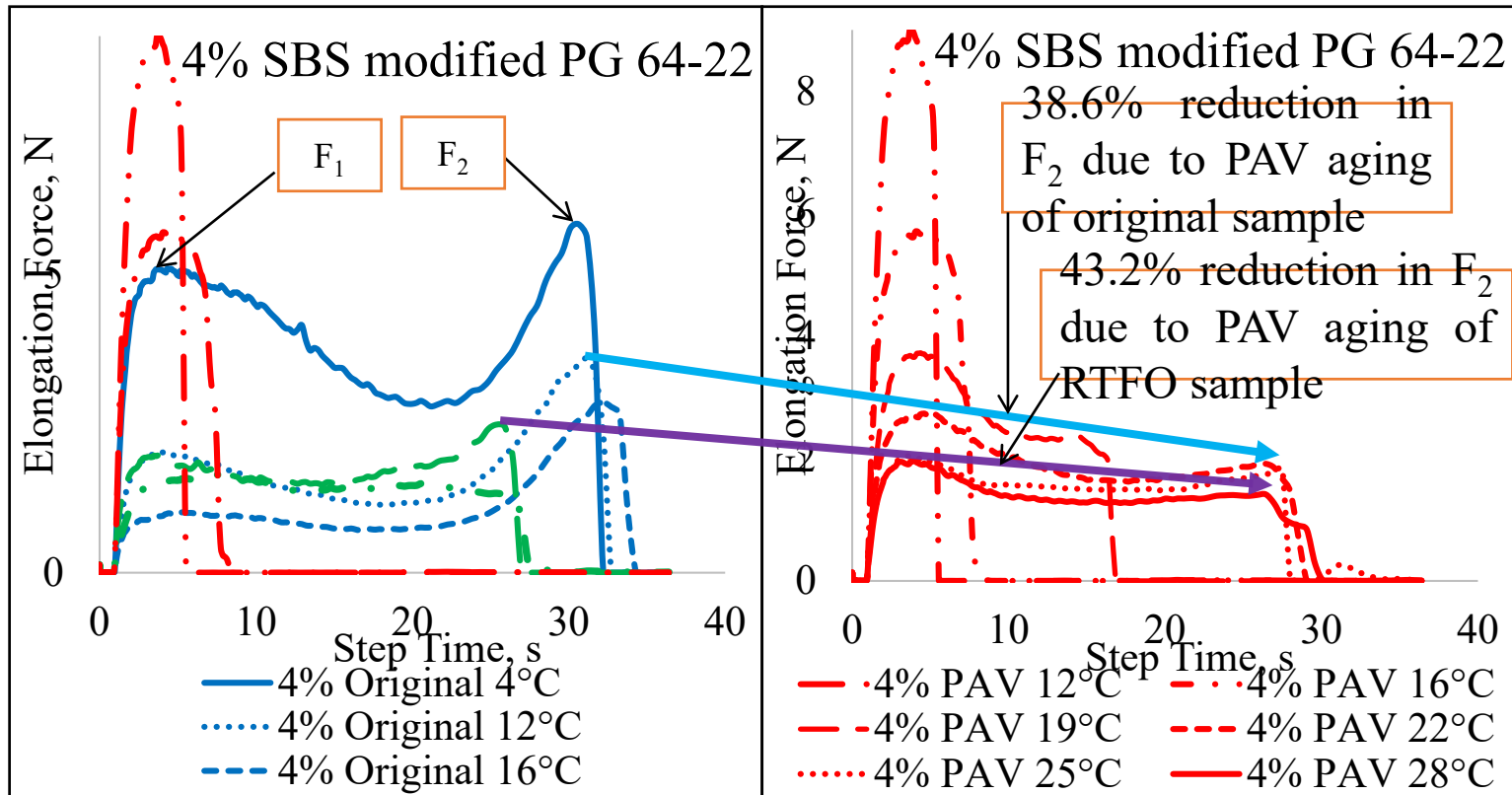


## Second Peak Elongation Force over First Peak Elongation Force

- 18-44% reduction after RTFO aging
- 65-100% reduction after PAV aging

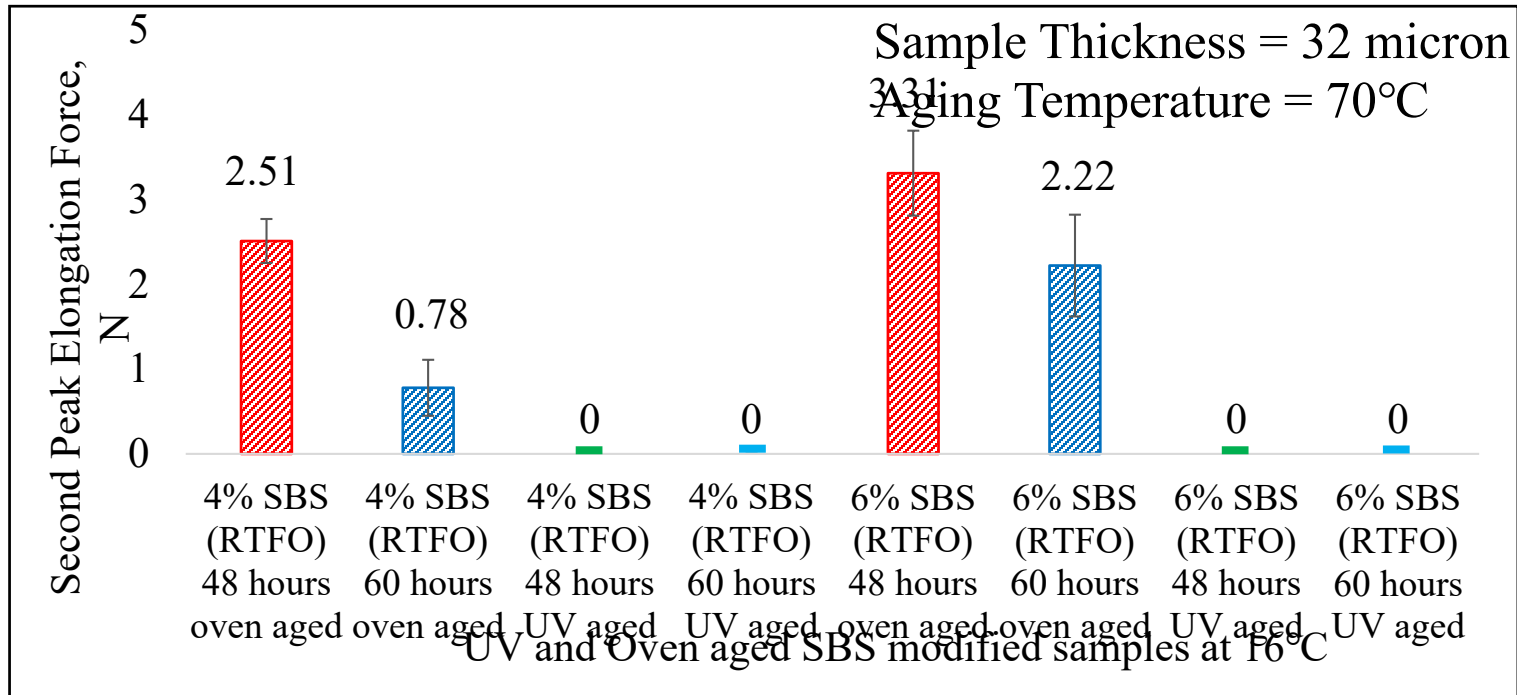


# Understanding $F_2$ Value of Stiffer Binder



## Second Peak Elongation Force of UV and Oven Aged Binder

- Oven aging: 40-78%
- UV aging: 100%
- UV A: 72mW/cm<sup>2</sup>
- 32 μm film thickness



## Test Factorial: SBS Degradation due to Aging of Asphalt Mixture

| Type                            | Specified Sample                                | Duration of Aging | Test Temperature   | No. of Sample                                |
|---------------------------------|---|-------------------|--|--|
| 4% SBS Modified PG 64-22 binder | Original  | -                 | 4°C, 12°C & 16°C   | 3 replicates for a specific test temperature |
|                                 |   |                   |  |  |
| Laboratory aged mixture         | Aging at 85°C temperature in forced draft oven  | 0 hour            | 4°C to 16°C at 4°C interval & 19°C to 28°C at 3°C interval | 3 replicates for a specific test temperature |
|                                 |   | 4 hours           |  |  |
|                                 |   | 1 day             |  |  |
|                                 |   | 3 days            |  |  |
|                                 |   | 5 days            |  |  |
|                                 | Aging at 135°C temperature in forced draft oven | 0 hour            | 4°C to 16°C at 4°C interval & 19°C to 31°C at 3°C interval | 3 replicates for a specific test temperature |
|                                 |   | 4 hours           |  |  |
|                                 |   | 8 hours           |  |  |
|                                 |   | 12 hours          |  |  |
|                                 |   | 1 day             |  |  |

## Laboratory Aged Asphalt Mixture



**Collection of mixture in a bowl before aging started**



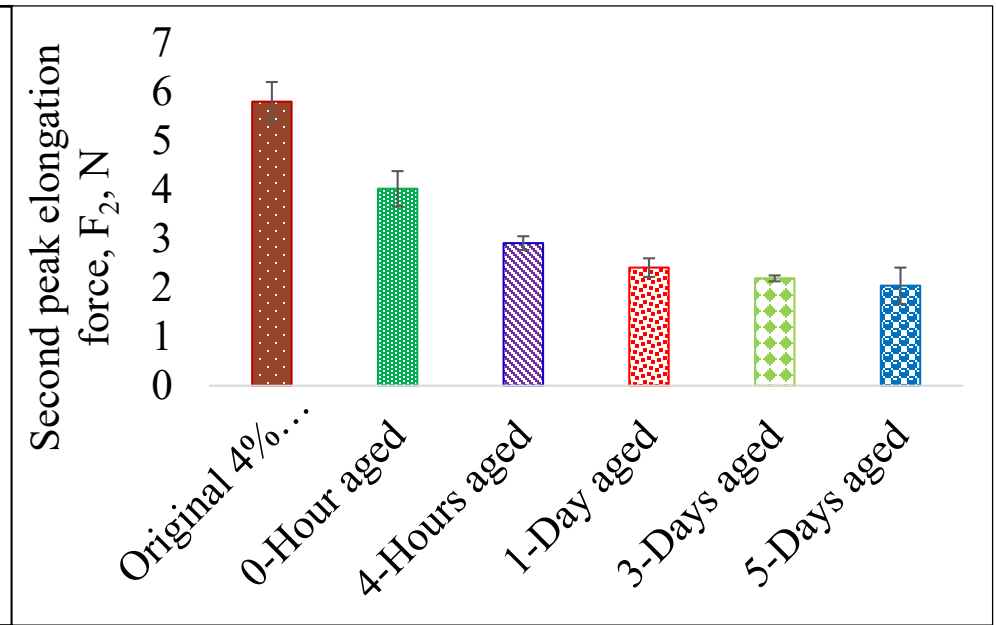
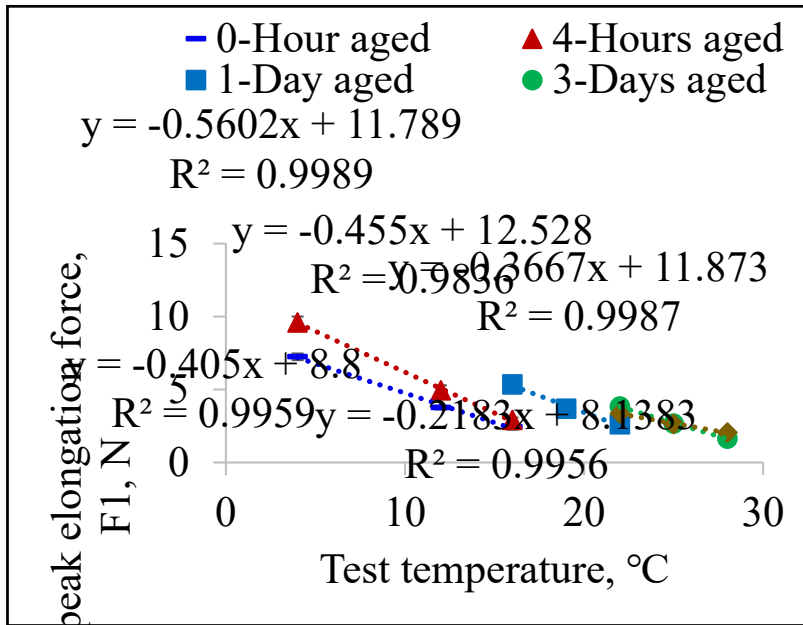
**Laboratory mixture aging at 85°C and 135°C**



**Asphalt binder extraction from loose mixture**

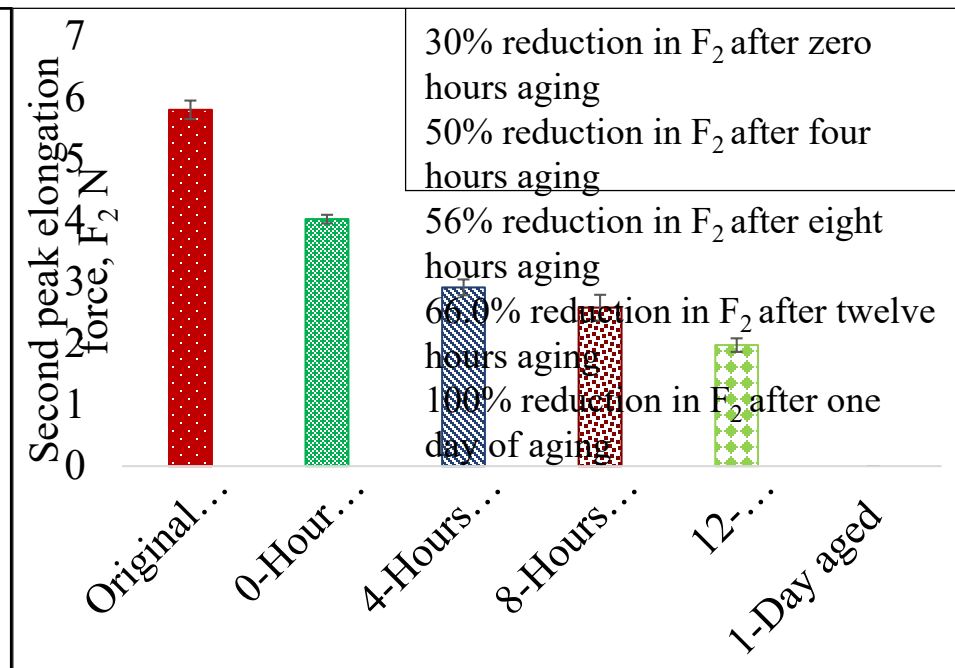
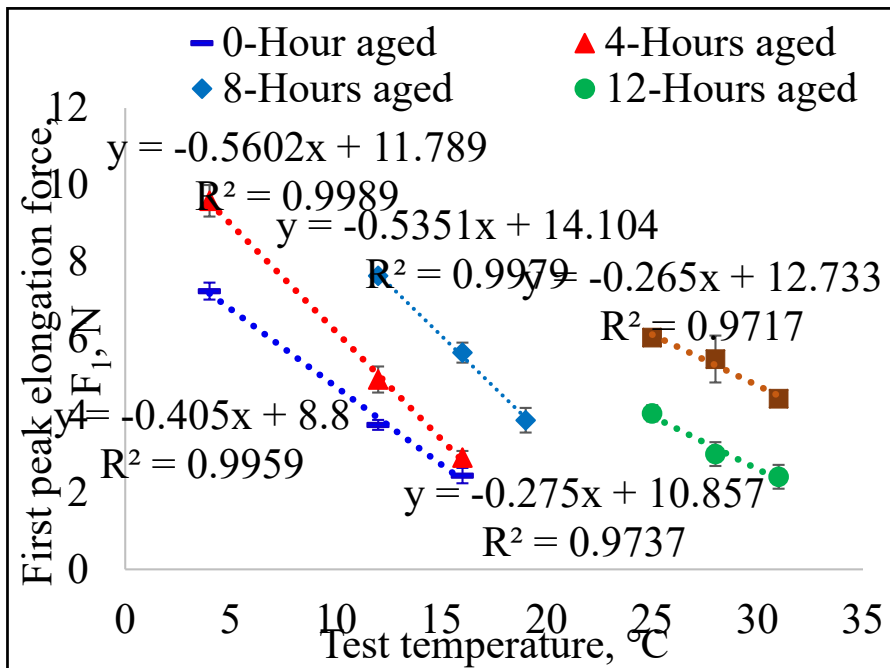


# Laboratory Aged Mixture Extracted Binder at Equal Stiffness (Aged at 85°C)





# Laboratory Aged Mixture Extracted Binder at Equal Stiffness (Aged at 135°C)



## Remarks

- SBS modified binder is the most effective in force ductility
- $F_1$  has no linear correlation with percent of elastomeric polymer
- $F_2$  has linear correlation with percent of elastomeric polymer with  $R^2= 0.99$
- All the test temperatures used in this study exhibit reduction in  $F_2/F_1$  due to RTFO aging, and further reduction is observed due to PAV aging
- UV aging degrades the SBS polymer completely
- 85°C mixture aging showed a 65% reduction; 135°C mixture aging showed a 100% reduction in  $F_2$  value
- Mixture aging temperature has more influence than aging duration in SBS degradation
- $F_2/F_1$  is recommended as a polymer degradation parameter due to aging

# Innovations in Testing—Modified Binders Cracking Resistance

## State Perspective on Cracking Resistance of Modified Binders

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MAY 25, 2022

ENAD MAHMOUD

DEPUTY DIRECTOR, MATERIALS AND TESTS DIVISION

TEXAS DEPARTMENT OF TRANSPORTATION

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# Outline

- Historical use of modified asphalt binders in Texas
- Research and specifications related to cracking resistance
  - Past
  - Present
  - Future

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- Historical use of modified asphalt binders in Texas
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# Historical Use of Modified Asphalt Binders

1960s 1970s 1980s 1990s 2000s 2010s 2020s

- HMA overlays on bridge decks needed more “flexible” mixes
  - Experimented with SBR
  - Success prompted the use of SBR modified binders
-

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# Historical Use of Modified Asphalt Binders

1960s 1970s 1980s 1990s 2000s 2010s 2020s

- AC-3 and AC-5 + 2% SBR for seal coats
- AC-5 and AC-10 + 2 to 3% SBR for HMA
- Developed FTIR based method to detect polymer content

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# Historical Use of Modified Asphalt Binders

1960s 1970s 1980s 1990s 2000s 2010s 2020s

- SBR use was very common
  - Other modifiers were introduced including SBS, EVA, Polyethylene
  - SBS showed better performance
  - Specs for AC-15P -30P for seal coats and -15P -30P -45P for HMA were added
  - 1997 adopted PG + retained polymer specific tests
-



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# Historical Use of Modified Asphalt Binders

1960s 1970s 1980s 1990s 2000s 2010s 2020s

- AC-xx- P or SBR or TR designations were used for chip seal binders
  - Polymer designations for PG binders were removed BUT Elastic Recovery using ductilitometer was retained as a requirement to detect elastomers
  - Research project on simple cracking test for binders → (more later)
    - Charles Glover @Texas A&M
    - Developed surrogate DSR parameter for ductility
    - Worked very well for unmodified binders
-

---

# Historical Use of Modified Asphalt Binders

1960s 1970s 1980s 1990s 2000s 2010s 2020s

- Additional specs for softer xx-TR binders
- Multiple projects and specs looking beyond PG:
  - Ductilometer elastic recovery spec → MSCR elastic recovery spec
  - XRF → Screen and limit use of PPA and REOB
  - Investigated cracking tests → Tc, GR, Poker Chip

---

# Outline

- Historical use of modified asphalt binders in Texas
- Research and specifications related to cracking resistance
  - Past
  - Present
  - Future

---

# Cracking of Asphalt Binders –

Past

“Indirect cracking” requirement via Elastic Recovery using Ductilometer



30% ER for UTI = 92  
(e.g. PG64-28, 70-22)

50% ER for UTI = 98  
(e.g. PG70-28, 76-22)

60% ER for UTI = 104  
(e.g. PG76-28, 82-22)

# Cracking of Asphalt Binders –

Past

Research on surrogate for ductility

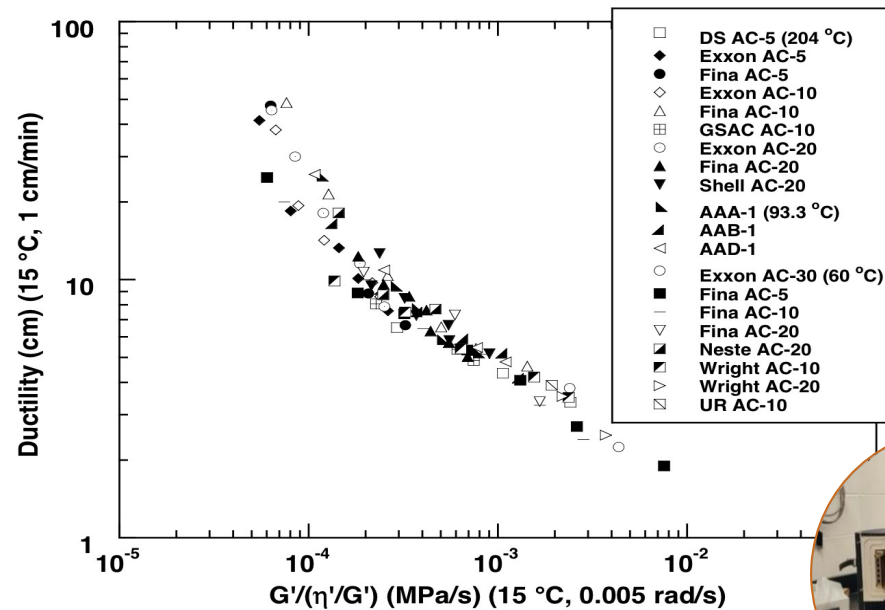
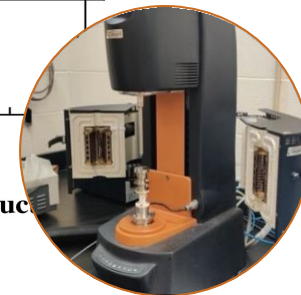


Figure 4-11. Ductility versus DSR Parameter  $G''/(\eta'G')$ , All Duct



Source: Glover et al. (2005); research was done between 1998 -2002

# Cracking of Asphalt Binders –

Past  
Research on surrogate for ductility

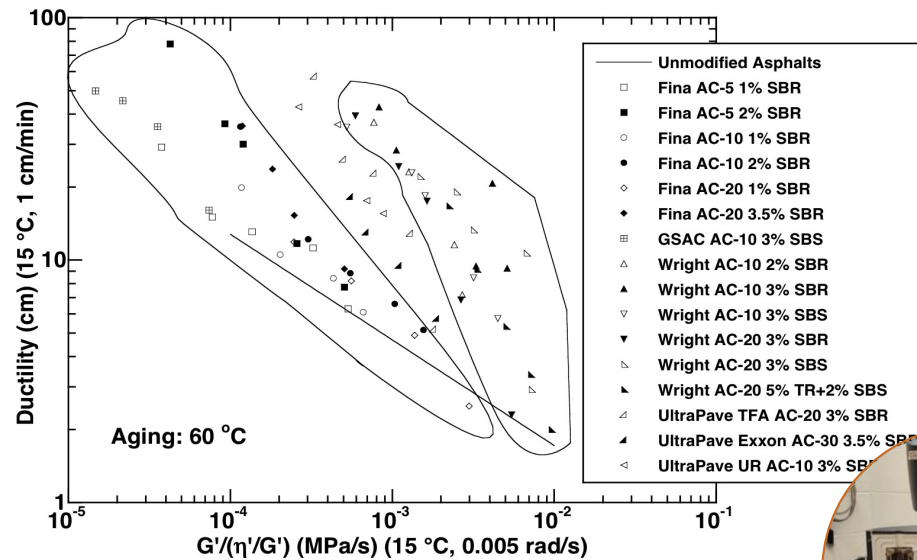
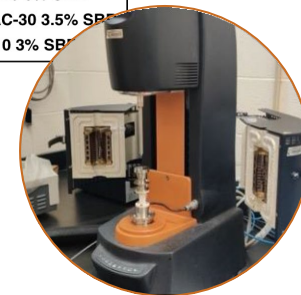


Figure 5-11. Ductility versus  $G'/(η'/G')$  for Modified Asphalts.

Source: Glover et al. (2005); research was done between 1998 -2002



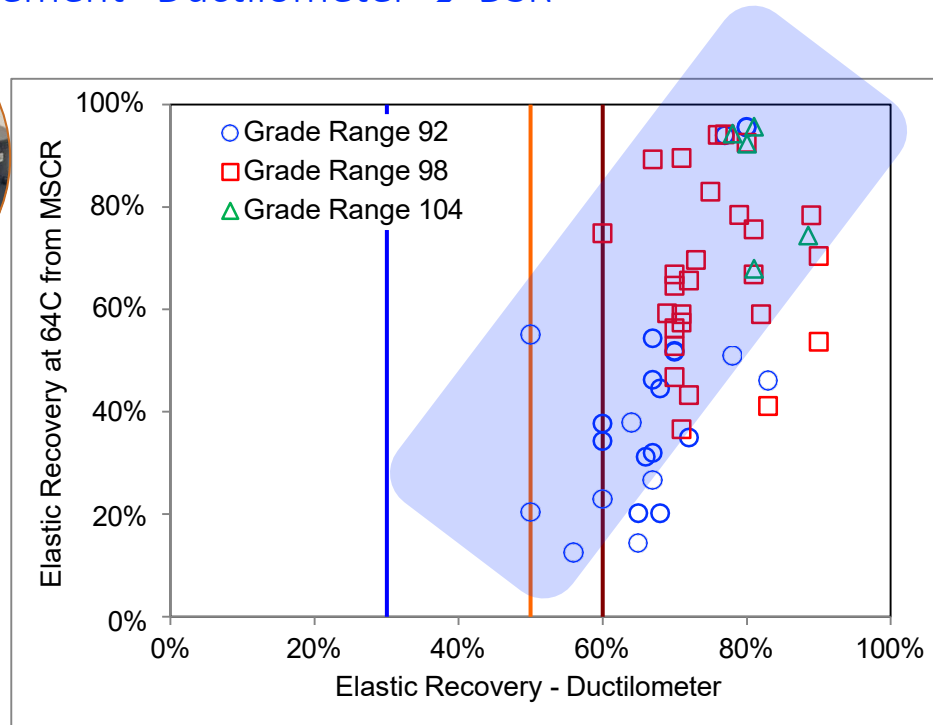
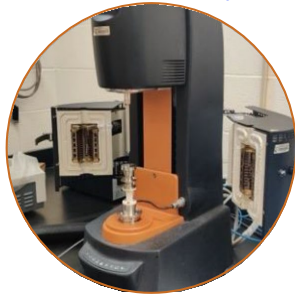
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# Outline

- Historical use of modified asphalt binders in Texas
- Research and specifications related to cracking resistance
  - Past
  - Present
  - Future

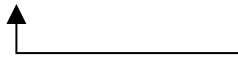
# Cracking of Asphalt Binders – Present

“Indirect requirement” Ductilometer → DSR

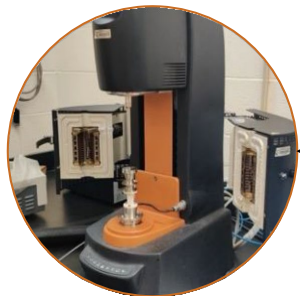




# Cracking of Asphalt Binders – Present



| Property and Test Method  | PG 58 |     |     | PG 64 |     |     | PG 70 |     |     | PG 76 |     |     | PG 82 |     |     |    |    |    |    |
|---|-------|-----|-----|-------|-----|-----|-------|-----|-----|-------|-----|-----|-------|-----|-----|----|----|----|----|
|   | -22   | -28 | -34 | -16   | -22 | -28 | -34   | -16 | -22 | -28   | -34 | -16 | -22   | -28 | -34 |    |    |    |    |
| Average 7-day max pavement design temperature, °C <sup>1</sup>      | 58    |     |     | 64    |     |     | 70    |     |     | 76    |     |     | 82    |     |     |    |    |    |    |
| Min pavement design temperature, °C <sup>1</sup>                    | -22   | -28 | -34 | -16   | -22 | -28 | -34   | -16 | -22 | -28   | -34 | -16 | -22   | -28 | -34 |    |    |    |    |
| <b>Original Binder</b>  |       |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| Flash point, T 48, Min, °C  | 230   |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| Viscosity, T 316 <sup>2,3</sup> :                                   | 135   |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| Max, 3.0 Pa·s, test temperature, °C                                 |       |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| Dynamic shear, T 315 <sup>4</sup> :                                 |       |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| G*/sin(δ), Min, 1.00 kPa, Max, 2.00 kPa <sup>7</sup> ,              | 58    |     |     | 64    |     |     | 70    |     |     | 76    |     |     | 82    |     |     |    |    |    |    |
| Test temperature @ 10 rad/sec., °C                                  |       |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| Elastic recovery, D6084, 50°F, % Min <sup>8</sup>                   | -     | -   | 30  | -     | -   | 30  | 50    | -   | 30  | 50    | 60  | 30  | 50    | 60  | 70  | 50 | 60 | 70 |    |
| <b>Rolling Thin-Film Oven (Tex-541-C)</b>                           |       |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| Mass loss, Tex-541-C, Max, %  | 1.0   |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| Dynamic shear, T 315:   |       |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| G*/sin(δ), Min, 2.20 kPa, Max, 5.00 kPa <sup>7</sup> ,              | 58    |     |     | 64    |     |     | 70    |     |     | 76    |     |     | 82    |     |     |    |    |    |    |
| Test temperature @ 10 rad/sec., °C                                  |       |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| MSCR, T350, Recovery, 0.1 kPa, High Temperature, % Min <sup>8</sup> | -     | -   | 20  | -     | -   | 20  | 30    | -   | 20  | 30    | 40  | 20  | 30    | 40  | 50  | 30 | 40 | 50 |    |
| <b>Pressure Aging Vessel (PAV) Residue (R 28)</b>                   |       |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| PAV aging temperature, °C   | 100   |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| Dynamic shear, T 315:   |       |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |
| G*/sin(δ), Max, 5000 kPa  | 25    | 22  | 19  | 28    | 25  | 22  | 19    | 28  | 25  | 22    | 19  | 28  | 25    | 22  | 19  | 28 | 25 | 22 | 19 |
| Test temperature @ 10 rad/sec., °C                                  |       |     |     |       |     |     |       |     |     |       |     |     |       |     |     |    |    |    |    |



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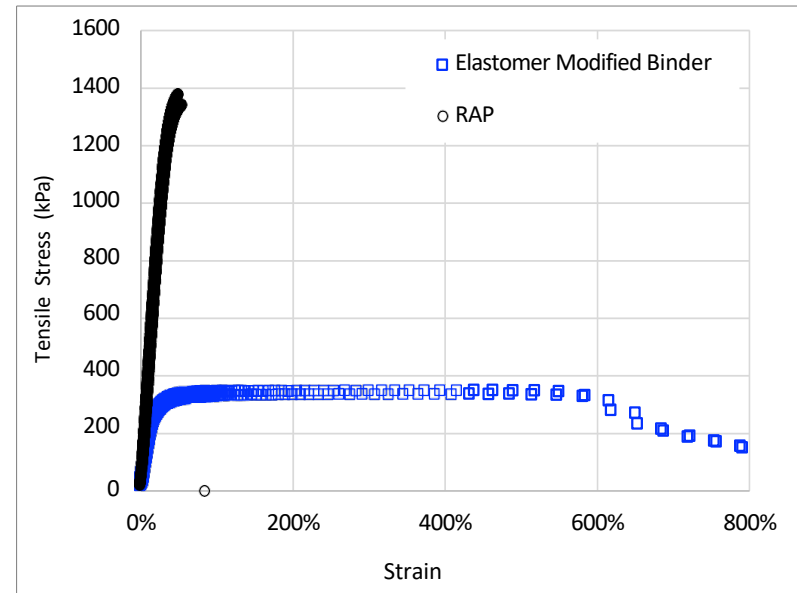
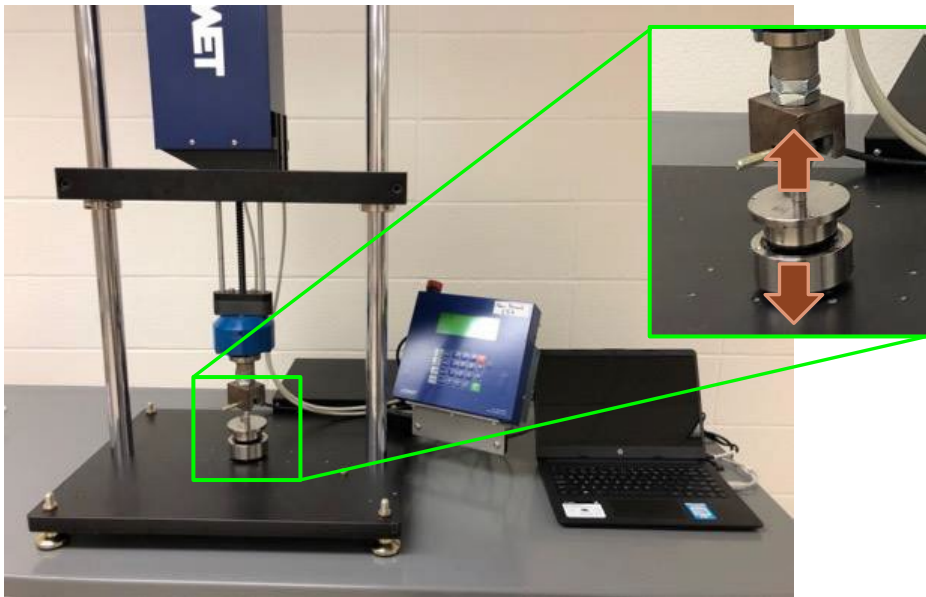
# Outline

- Historical use of modified asphalt binders in Texas
  - Research and specifications related to cracking resistance
    - Past
    - Present
    - Future
-

# Cracking of Asphalt Binders – Future

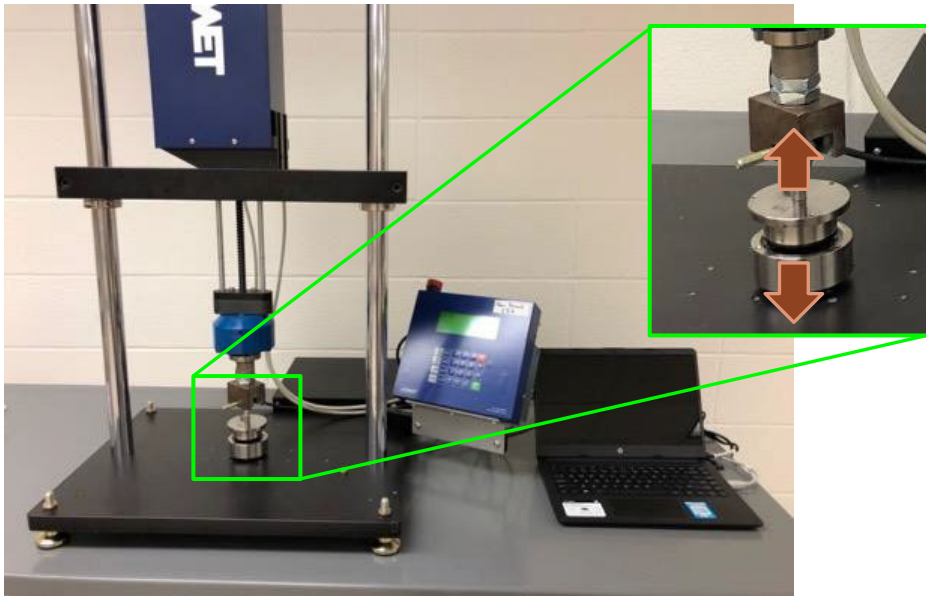
Poker chip test →

Combine fundamental mechanics  
with simple test



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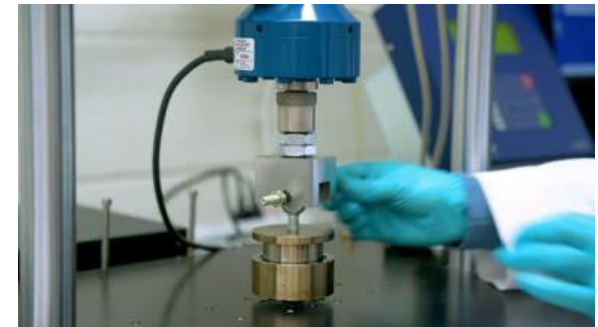
## Cracking of Asphalt Binders – Future



- Equipment
  - ✓ Low capital cost
  - ✓ Small footprint
  - ✓ Plug and play
- Sample
  - ✓ Easy to prepare and run
- Results
  - ✓ Easy to interpret
  - ✓ No special software
- Other
  - ✓ Induces failure
  - ✓ Repeatable

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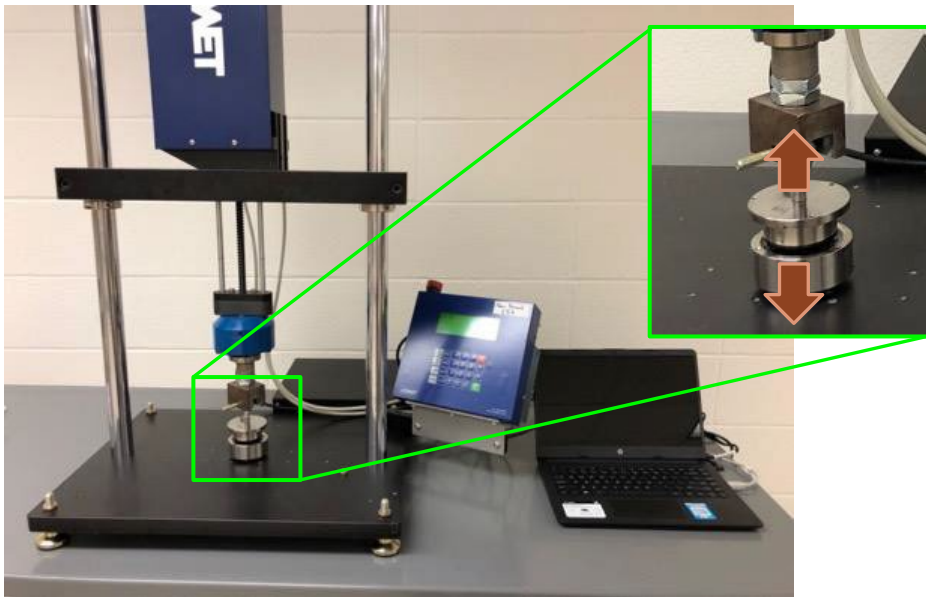
# Cracking of Asphalt Binders – Future



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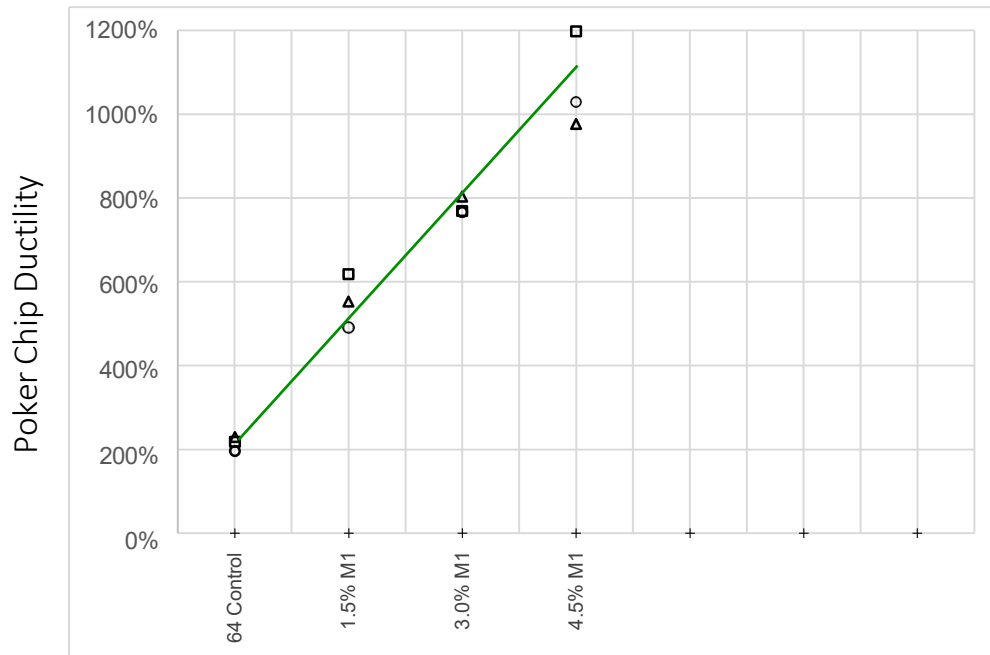
## Cracking of Asphalt Binders – Future

- Lab modified binders
- PG binders
- Field validation with cracking

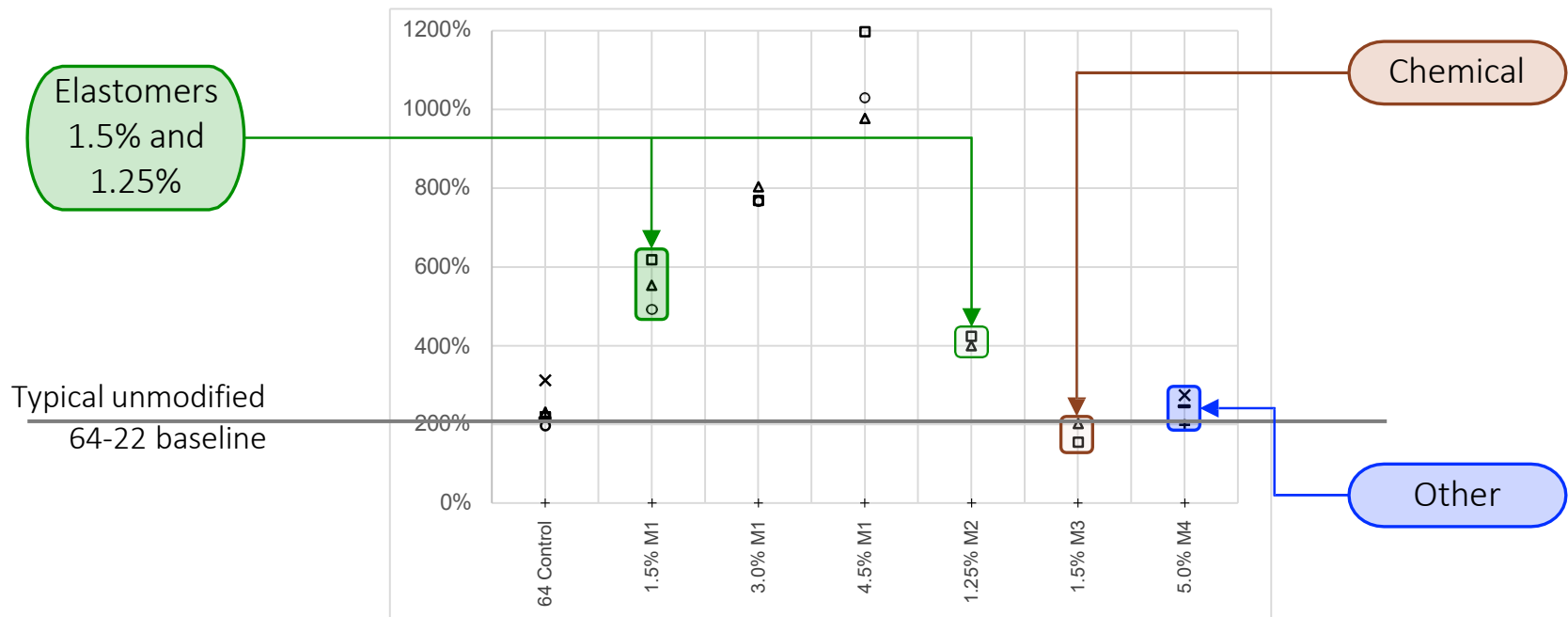


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# Cracking of Asphalt Binders – Future



# Cracking of Asphalt Binders – Future

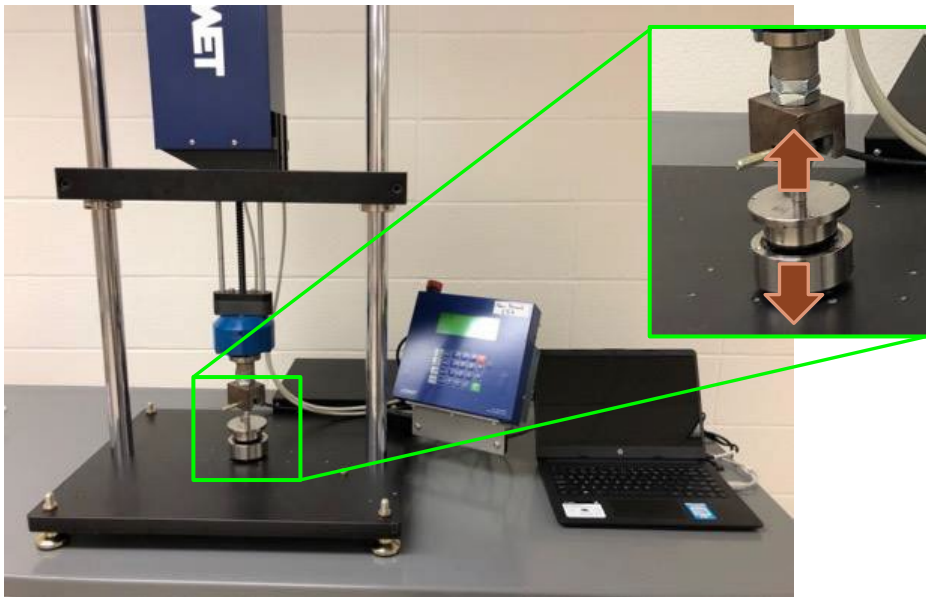




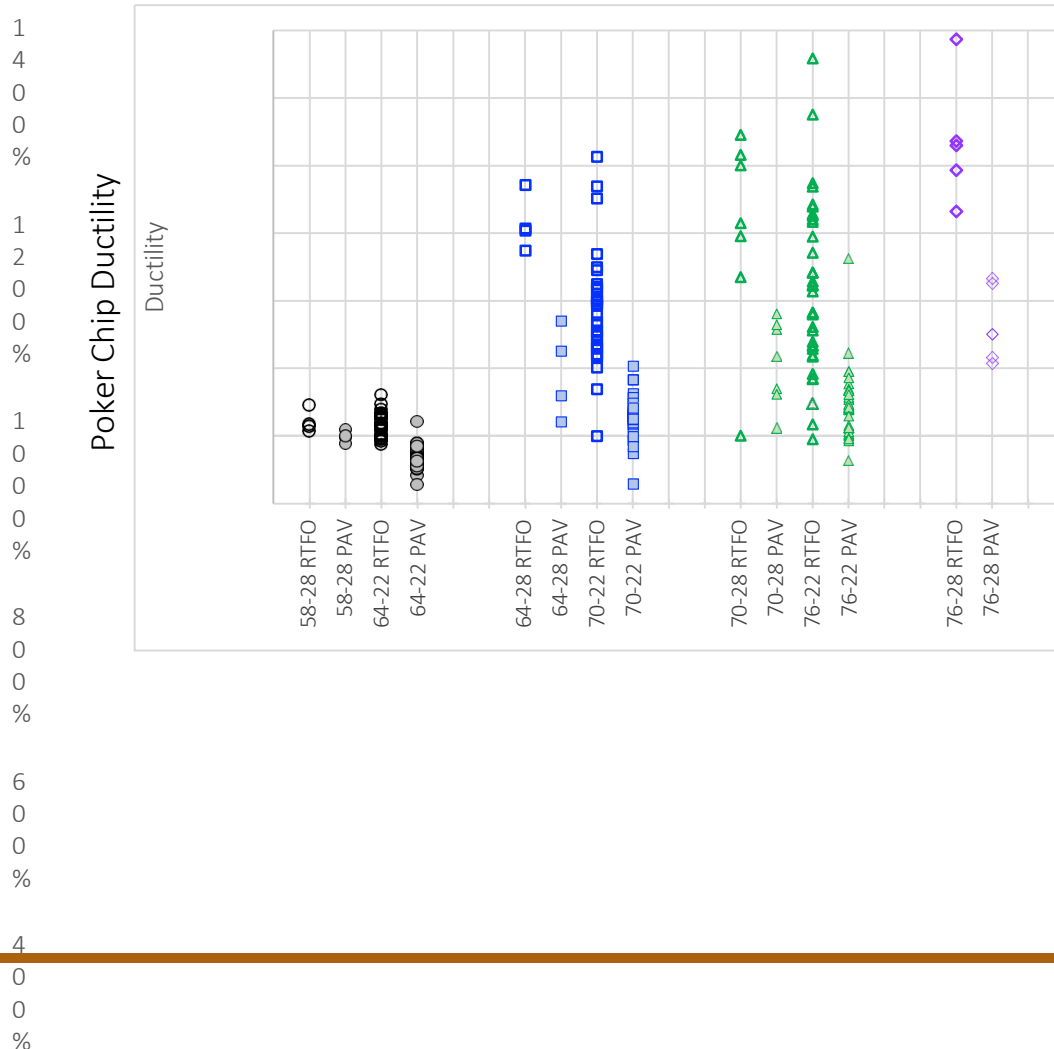
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## Cracking of Asphalt Binders – Future

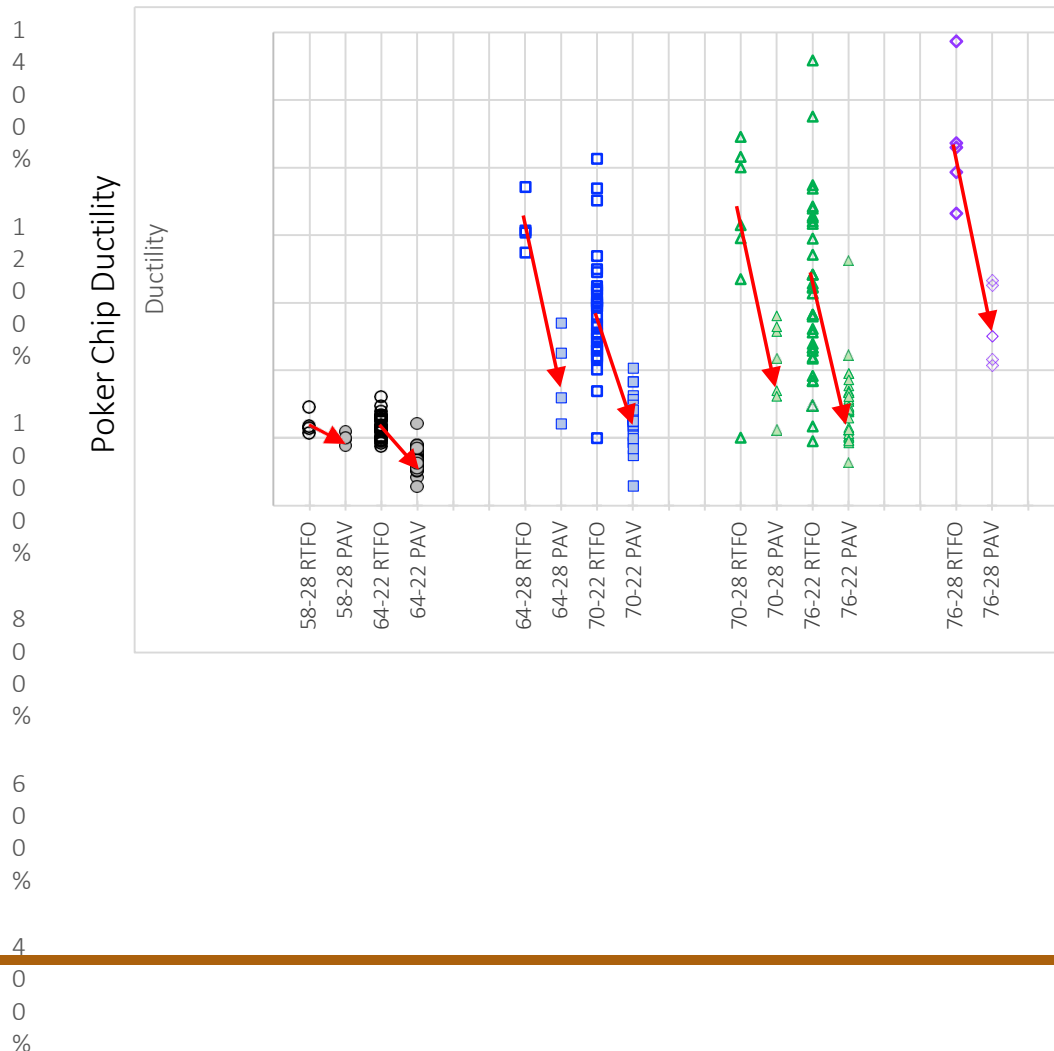
- Lab modified binders
- PG binders
- Field validation with cracking



# Cracking of Asphalt Binders – Future

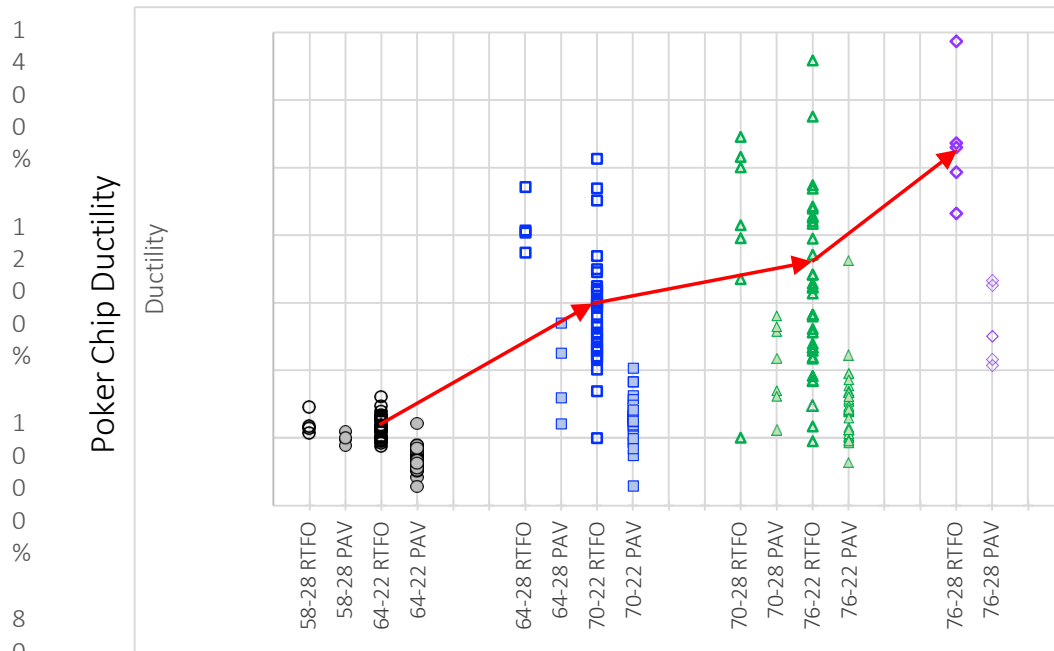


# Cracking of Asphalt Binders – Future



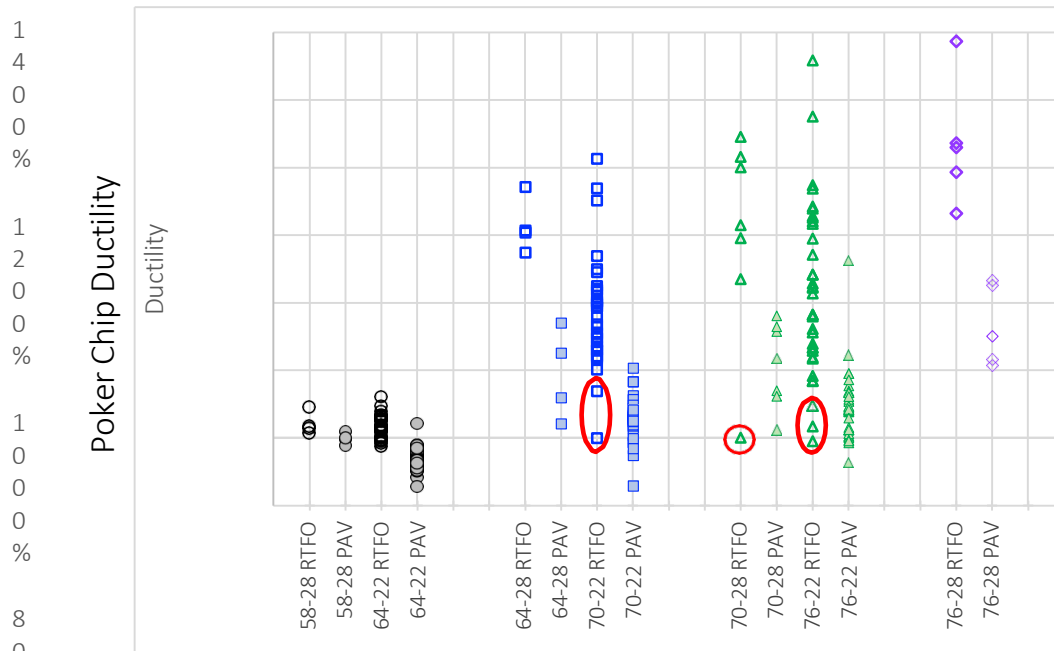
- Effect of 20PAV aging

# Cracking of Asphalt Binders – Future



- Effect of 20PAV aging
- Effect of polymer (RTFO)
  - 64-22 →
  - 70-22 →
  - 76-22 →
  - 76-28

# Cracking of Asphalt Binders – Future

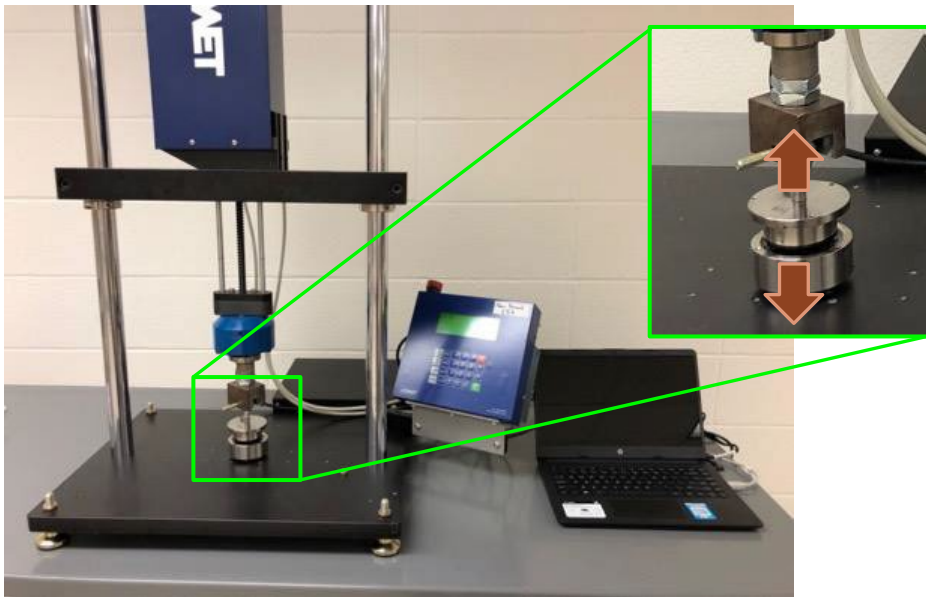


- Effect of 20PAV aging
- Effect of polymer (RTFO)
  - 64-22 →
  - 70-22 →
  - 76-22 →
  - 76-28
- Anomalous Binders with elastic recovery but low ductility

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## Cracking of Asphalt Binders – Future

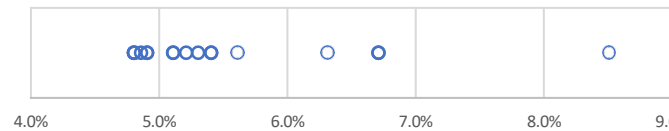
- Lab modified binders
- PG binders
- Field validation with cracking



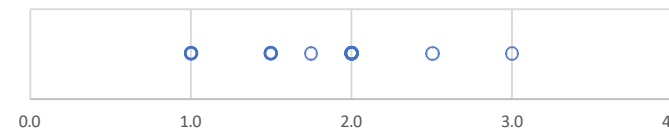
# Cracking of Asphalt Binders – Future

- Diverse locations / weather conditions

- Binder contents (%)



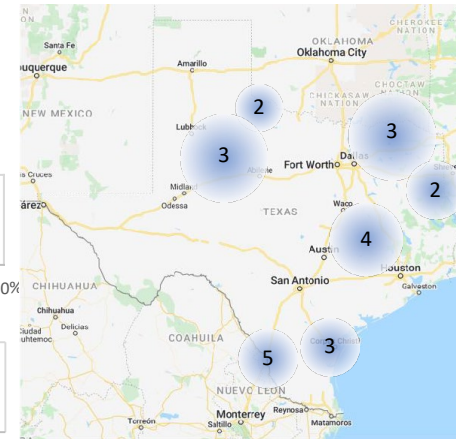
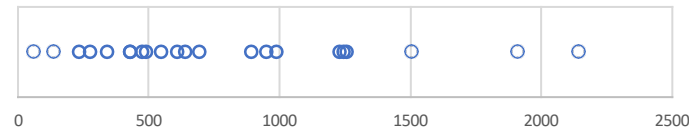
- Layer thickness (in)



- Total HMA thickness (in)



- Truck traffic



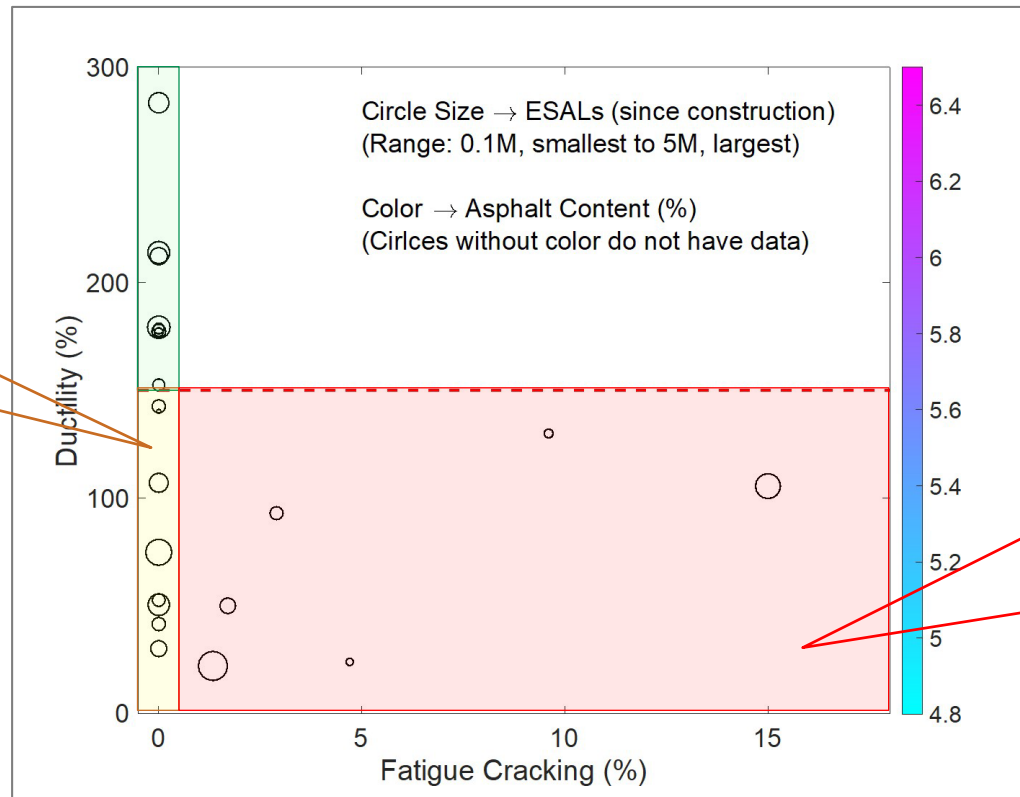
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# Cracking of Asphalt Binders – Future





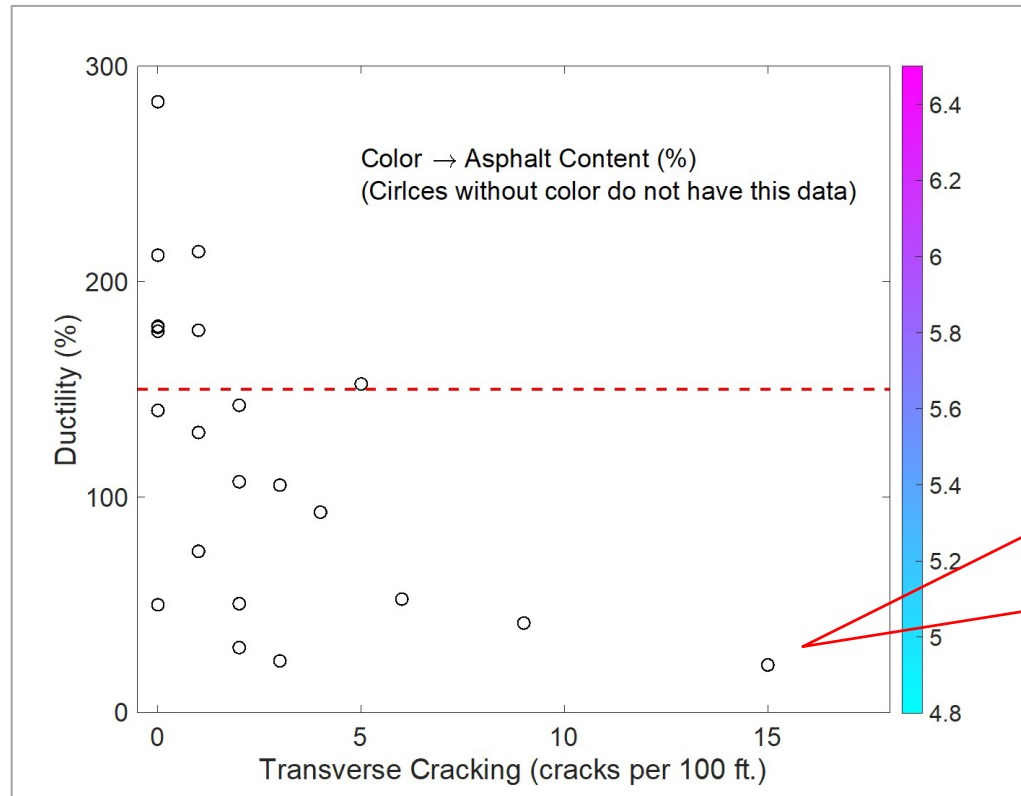
# Cracking of Asphalt Binders – Future



These sections have low ductility but no surface cracking at the time of inspection

43% of sections with ductility < 150% showed signs of fatigue cracking on surface regardless of traffic volume, thickness, and binder content.

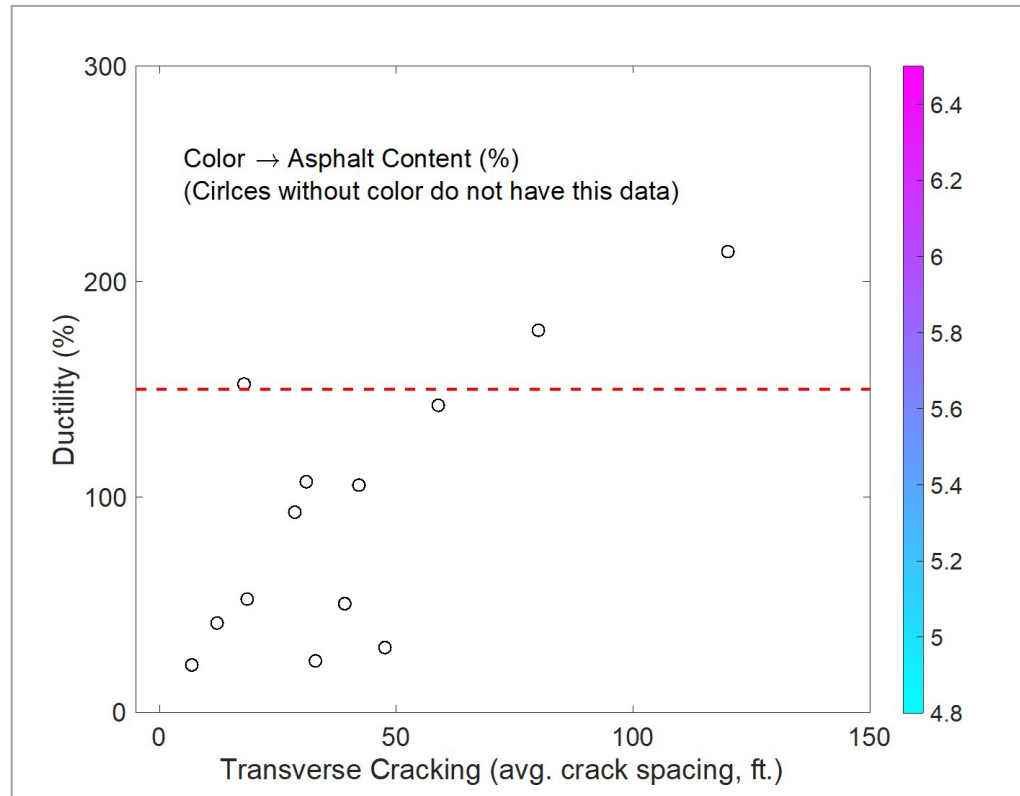
# Cracking of Asphalt Binders – Future



86% of sections that showed ductility < 150% showed some degree of transverse cracking.

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# Cracking of Asphalt Binders – Future

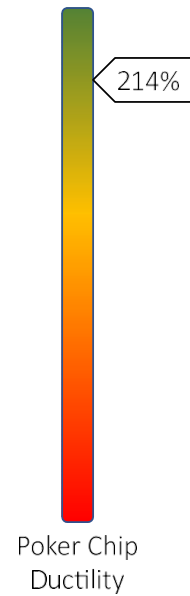


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# Cracking of Asphalt Binders – Future

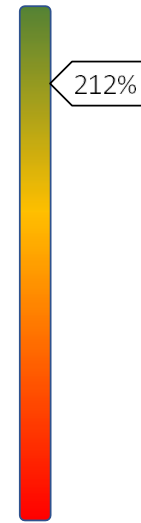
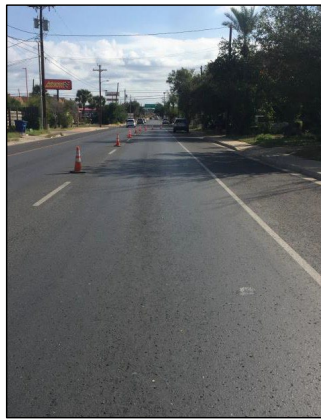


#1: 7 years  
Photo and coring from Oct. 2019



---

# Cracking of Asphalt Binders – Future



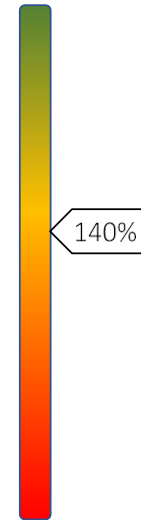
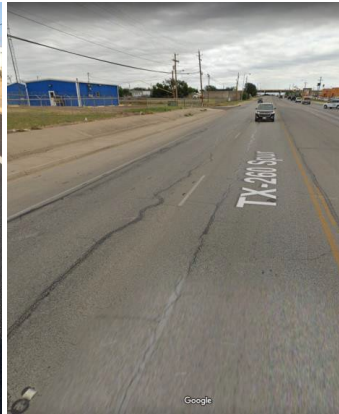
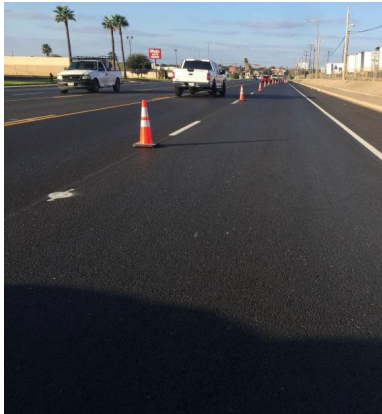
Poker Chip  
Ductility

#20: 7 years

Left – Photo and coring from Nov. 2021; Middle and Right – Google Street from Jan. 2019 and April 2021 showing no cracking over time

---

# Cracking of Asphalt Binders – Future



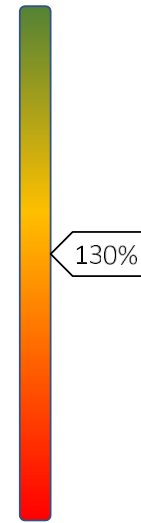
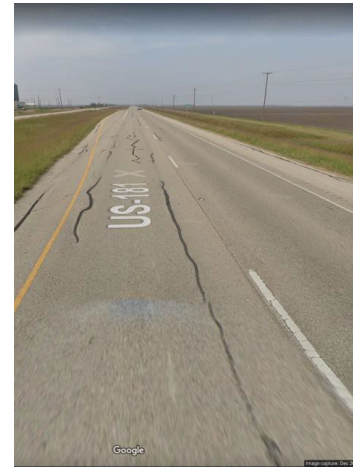
Poker Chip  
Ductility

#19: 7 years

Left – Photo and coring from Nov. 2021 after a recent overlay; Right – Google Street from April 2021 before the overlay showing cracking

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# Cracking of Asphalt Binders – Future



Poker Chip  
Ductility

#3: 6 years

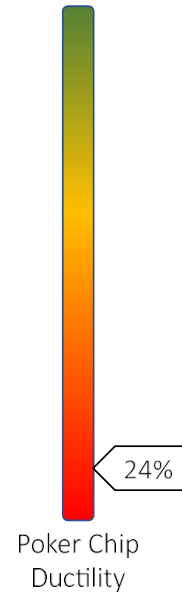
Note: Left – Nov. 2019 during coring; Middle and Right – Google Street, Dec. 2021

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# Cracking of Asphalt Binders – Future



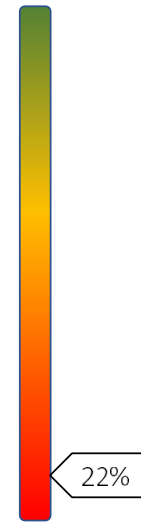
#22: 9 years  
Photo and coring from Nov. 2021





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# Cracking of Asphalt Binders – Future



Poker Chip  
Ductility

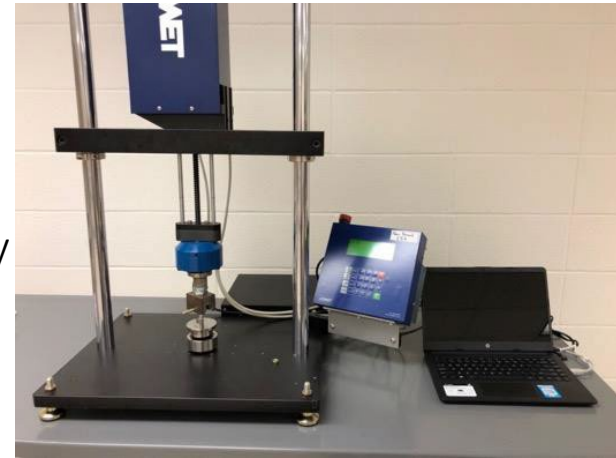
#13: 7 years

Left – Photo and coring from March 2020 after a recent seal coat showing some bleed through cracks; Right – Google Street from April 2018 before seal coat showing cracks

---

## Conclusions

- One additional piece of equipment ( $\cong$  15K)
- + Method  $\rightarrow$  Simple and repeatable
- + Equipment  $\rightarrow$  Low cost, small footprint, plug and play
- + Parameter  $\rightarrow$ 
  - o mechanics based,
  - o induces failure and not a stiffness index,
  - o measured directly,
  - o sensitive to elastomer content,
  - o sensitive to aging
- + 87% of field sections had some form of cracking when ductility  $<$  150%





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[enad.mahmoud@txdot.gov](mailto:enad.mahmoud@txdot.gov)



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 TRANSPORTATION RESEARCH BOARD

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Demand Response Transportation Conference**

A TRB Virtual Event • September 12–16, 2022

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Transportation  
Research Board

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- May provide a path to Standing Committee membership

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**Work with CRP** <https://bit.ly/TRB-crp>

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