				~	Jul 11			- 111		,,,	——	, 							
Date	Ac		Bı	ı	B <sub>2</sub>		Ва	,	Cı	,	C2		Ca	,	D <sub>1</sub>	,	D <sub>2</sub>	]	D <sub>3</sub>
1925 Feb 23 Difference Mar 19 Difference Apr 8 Difference May 12 Difference July 21 Difference Sept 29	7 3. + 0. 7 3. 7 3. + 0. 7 3. - 0. 7 3.	39 - 51 - 53 - 53 - 53 + 53 - 50 +	6 630 - 009 6 639 - 006 6 634	- - 6 - 6 + - 6	011 701 000 701 009 710 014 696	- 6 - 6 + 6 - 6	010 787 005 782 012 794 014 780	+ -6 -6 + 6 -6	007 621 006 627 004 623	- - - 6 + - 6	010 677 003 674 010 684 013 671	- 6 - 6 + 6 - 6	011 758 004 754 011 765 013 752	- - 5 - 5 + 5 - 5	006 726 006 720 018 738 016 722	- 5 + 5 + 5 - 5	001 837 010	- - 5 - 5 + 5	006 895 027 922 013
Difference 1926 Jan 19	7 40		6 686		749		<i>050</i> <b>830</b>		<i>047</i> 676		055 726		<i>050</i> <b>802</b>	·	789		<i>064</i> 897	Ì	969
Difference	+ 00	3 +	055	+	050	+	052	+	051	+	049	ı	053	+	060	+	067		076
Mar 11	7 46	4	6 741	6	799	6	882	6	727	6	775	6	855	5	849	5	964	6	045
Difference	- 10	-	106		101		098		102	-	100		100	_	119	_	123	-	21 ō
Apr 9	7 3	- 1	6 635	6	698				625		675		755	5	730	5	841	5	830
Difference	= a	71	003	_	003		004		003		005		005	_	007	_	009		
May 19	7 35	62 -  -	6 632		695	-6	780	- 6·	622	6	670		750		723		832	*5	940
Max diff 1925 Max diff 1926 Difference	04 11	- 1	016 109		084 104		050 102		010 105		030 105		046 105		041 1 <b>2</b> 6		054 1 <b>32</b>		066

TABLE X
STATION 72, ROUTE 91
South line of Hudson, Ohio

## SUB-BASE TESTS ON ROUTE 26, WASHINGTON COUNTY, OHIO

003 -

# F H Eno Ohio State University, Columbus, Ohio

In October and November, 1924, a series of sub-base experimental sections was constructed upon the Marietta-Athens road known as State Aid Route 26. These sections varied from 100 to 200 feet in length. The sub-base construction was 2, 4 or 6 inches in thickness, and was constructed of sand, gravel, slag or an admixture of 5 per cent Portland cement, by volume, mixed with the top 2, 4 or 6 inches of the natural sub-base. Adjoining sections of the natural soil base were left at either end of the three divisions of this test work for comparison. The sand and gravel were dredged out of

<sup>\*</sup>Broken up

		I	PROC	EE	DI	NC	ß	(	F		SI.	X	ľE	I	A.	N I	VU	A	L	A	E	E'	ľI	N	G					17	71	
	Num- ber of	cracks		9		11	<b>90</b>	7	N Ç	2 '		<b>3</b> 50 1	n ;	13	~	18	23	21	<b>∞</b>	<b>∞</b>	0 (	9	•	=======================================	4	e-	ភ	6	16	<b>z</b>		
0Н10	Foot of crack	per foot of road	Feet	8	_	06 0	8	25	8 6	62 G	6 i	0 74		0 65	0 52	0 78	96 0	1 58	95 0	80 :	8 :	0.46	0 41	0 79	0 44	90	0 68	0 94	1 24	1 48		
UNTY	Total	cracks	Feet	129		83	88	<b>%</b>	88	79	80	100	38	133	105	157	177		106 5	159	0	95	79	158	99	Z	¥	11	194	1,330		
ONO	Section	length	Feet	65 0	_		97 5		99 5	2 66		135 5					196 3	201 7	190 5	146 5			193 5	200	150 5	51 0	79 0		158	0 006		
TOTAL CRACKS ON OCTOBER 12, 1926, UPON SUB-BASE TEST SECTIONS, ROUTE 26, WASHINGTON COUNTY, OHIO	Longitudinal and	center line		Crack continued from			End of above, 3 feet			1 joint				1 thaw (a blowup)	Many cracks at culvert	3 cracks, 7 feet, 1 blowup	1 crack, 4 feet	1 crack, 131 feet (1 joint)	1 joint	1 L, 74 feet and continued	1 joint			1 crack, 12 feet	1 joint	1 joint	1 joint		2 cracks, L, 69 feet	2 cracks, L, 70 and 444 feet		
IONS, RO	racks	Right	Feet				4 cracks, 14	2 cracks, 5						2 cracks, 3		4 cracks, 13	6 cracks, 15	1 crack, 2		1 crack, 3		1 crack, 2						2 cracks, 5				
EST SECT	Corner cracks	Left	Feet	1 crack, 4		2 cracks, 4	_	1 crack, 3		12		2 cracks, 7		3 cracks, 10			7 cracks, 25		2 cracks, 5 5	l crack, 1			1 crack, 1	l crack, 2					2 cracks, 4	Not counted		
SUB-BASE 1	Through	transverse	Feet	2 cracks, 36		4 cracks, 72	4 cracks, 72				racka,		2 cracks, 36	6 cracks, 111	5 cracks, 90	7 cracks, 126	6 cracks, 108	6 cracks, 108	5 cracks, 90	4 cracks, 72		5 cracks, 90	4 cracks, 72	8 cracks, 144	3 cracks, 54	3 cracks, 54	2 cracks, 36		4 cracks, 72	36 oracks, 648	broken up	
26, UPON	Transverse.	nght side	Feet							1 crack, 4				1 crack, 9	1 crack, 11		2 cracks, 17	4 cracks, 24							1 crack, 12		2 cracks, 14		4 cracks, 30	7 cracks, 56		
BER 12, 19	Transverse.	left side	Feet	2 cracks, 24			2 cracks, 21		-					1 joint		1 joint	1 crack, 8	7 cracks, 46	1 crack, 11	1 crack, 9			1 crack, 6				1 crack, 4	2 cracks, 16	4 cracks, 19	5 cracks, 40		
CKS ON OCTO	Ваев			Natural soil		6 ms gravel	6 ms sand	6 ms cem -clay	6 ms slag	2 ins sand	4 ins sand	Natural soil	Natural soil	2 ins sand	4 ms slag	4 ins gravel	4 ms sand	4 ins cem -clay	6 ms sand	Natural soil	Natural soil	2 ins gravel	2 ins slag	2 ins cem -clay	2 ms sand	2 ms to 4 ms sand	4 me sand	6 me sand	Natural soil	Natural soil		
TOTAL CRA	Station to station			129-00 0 to 129-65 0		129-65 0 to 130-68 5	130-68 5 to 131-66 0	131-66 0 to 132-66 5	132-66 5 to 133-66 0	133-66 0 to 134-65 7	134-65 7 to 135-64 5	135-64 5 to 137-00 0	154-00 0 to 154-59 2	154-59 2 to 156-62 5	156-62 5 to 158-63 5	158-63 5 to 160-65 0	160-65 0 to 162-61 3	162-61 3 to 164-63 0	164-63 0 to 166-53 5	166-53 5 to 168-00 0	195-00 0 to 195-51 0	195-51 0 to 197-51 9	197-51 9 to 199-45 0	199-45 0 to 201-45 0	201-45 0 to 202-95 5	202-95 5 to 203-46 5	203-46 5 to 204-25 5	204-25 5 to 205-44 0	205-44 0 to 207-00 0	207-00 0 to 216-00 0		

		TABLE II	. 11				
ADDITIONAL CRACKS ON SUB-BASE TEST SECTIONS, ROUTE 26, WASHINGTON COUNTY, OHIO NOVEMBER 10, 1925, TO OCTOBER 12, 1926	ON SUB-BAS NOVEME	E TEST SECTIOI SER 10, 1925, TO	SUB-BASE TEST SECTIONS, ÄÖUTE 26, WASHIN NOVEMBER 10, 1925, TO OCTOBER 12, 1926	NGTON COI	UNTY, O	BIO	
Sub-base material	Trans	Transverse cracks	2004400	Corner cracks	racks	Center,	172
	Left ade	Right side	Cical act USS	Left	Rught	longitudinal	
rai soul rai soul	2=15 ft		1 = 18 ft 1 and extension = 22 ft	1=4 ft			
'al soil 'al soil 'al soil	No extra No extra		1=18 ft				HIG
soul	·	l extension to		1 = 2.5  ft			‡ <b>H</b> ₩.
al soil adjoining	8=55 ft	4=22 ft	5 = 90 ft	2=5 ft		L extended	ΑY
t natural soil	10 = 70  ft	5=35 ft	8=148 ft	4=11 5 ft		3 113 ft 3 113 ft	RES
gravel gravel	1=2ft	1=2 ft	1 extension = 5 ft $1 = 18$ ft			Burbt lone 2 ft	SEAI
gravel					1=2 ft	tugne tong , o te.	RCH
<b>.</b> 5	1=11 ft	1 extension = 9 ft	1=18 ft		2=5 ft		В
Sand	2=17 ft			_			)A.R
ם י	No extra						2D

2 = 17 ft No extra No extra

sand sand sand

119 ft 6 m 196 ft 4 m

190 ft 6 m sand

1000 ft natural soil adjoining

50 ft natural soil 51 ft natural soil 56 ft natural soil

Total, 1,417 ft natural soil

200 ft 2 in gravel 103 ft 6 in gravel 202 ft 4 m gravel 98 ft 6 in sand

TABLE II

65 ft natural soul 136 ft natural soil 59 ft natural soil Longitudinal, 3 ft

2 short extensions = 7 ft

2 = 12 ft

4 = 27 ft

No extra

100 ft 6 m cem -clay 202 ft 4 m cem -clay

203 ft 2 m sand

202 ft 2 in sand

79 ft 4 in sand 99 ft 2 in sand

100 ft 4 in

cem -clay

200 ft 2 m

100 ft 6 m slag 201 ft 4 m slag 194 ft 2 m slag

2=36 ft .

No extra

1=6 ft

1=2ft

4 = 66 ft

1 = 6 ftl = 4 ft1 = 9 ft1 = 12 ft

1 = 18 ft

Longitudinal, 3 ft

the Ohio River a short distance below Marietta The granulated slag was shipped in from the Steubenville District

The road is an 18-foot concrete road with thickened edges, 7 inches thick at the center and 9 inches at each edge, reinforced with one 34-inch bar along either edge and with no center joint. Transverse joints were placed only at the end of the day's work.

The experimental work was constructed in three sections of 800, 1,000 and 1,200 feet in length, made up of the smaller 100 or 200 feet sections of the individual test bases

The soil in each division was of dark red color, fairly fat in clay and in appearance to the eye seemed to be all of the same type. There was perfectly dry weather throughout the construction of the experimental sections. No difficulty was experienced in getting a good admixture of the cement and soil

A survey of the cracks was made on November 10, 1925, and another survey made on October 12, 1926

Table I gives a record of the total number of cracks showing on October 12, 1926, with their total number of feet in length

Table II shows the additional cracks that have appeared from November 10, 1925, to October 12, 1926.

The results for the total number of cracks from the time of construction is summed up in Table III

TABLE III
SUMMARY OF TOTAL CRACKS

Pavement in feet	Type of base	Total feet of cracks	Ratio
1,513	Natural soil	1,950	1 29
502	Cement-clay	561	1 12
2,015 4	Combined natural soil and cement and clay	2,511	1 25
1,285	Sand	946 5	0 74
505 5	Gravel	342	0 68
494	Slag	220	0 45
2,284 5	Combined porous base	1,508 5	0 66

Slag appears to have a slight advantage over any other treatment. The porous bases show approximately one-half as many cracks as appear in the natural soil base. The additional cracks showing from November, 1925 to October, 1926, are summed up in Table IV

Pavement in feet	Type of base	Total feet of cracks	Ratio
1,417	On natural base	377 5	0 266
502	Cement-clay	49 0	0 098
1,285	Sand	177 0	0 133
494	Slag	45 0	0 091
505	Gravel	32 0	0 063

TABLE IV SUMMARY OF ADDITIONAL CRACKS

The natural base compared with the treated base consists of the adjoining sections of natural base at either end of each main division of the experimental work, these lengths ranging in length from 50 to 139 feet, together, with a section 1,000 feet long adjoining the westernmost division of the sub-base tests

Considering the fact that the additional cracks appearing in the second year show the same good effects caused by the treated bases that the total cracks show for two years service, it would seem safe to assume that the treated bases really have meant improved road construction

It will not be safe to draw any conclusions as to the sufficiency or insufficiency of 2, 4 or 6 inch treatment. At present some of the two inch treatments show less cracks than the 4 or 6 inch

Table V gives the soil analyses for a number of soils along Route 26 where these sub-base tests are being tried

TABLE V

Sand Sut - 1	-	SOIL AN	ALYSIS OF	THE	SOILS	ALON	G ROU	TE 26
	Soil			Sand	Silt	Susp clay	ì	Volu change

Road sta	Coarse maternal	Sand	Sılt	Susp clay	Total clay	Volu change	Moist equiv
71+50	14 1	28 2	23 5	29	48 3	18 5	16 8
129 + 50	1 1	96	29 5	63	60 9	22 8	21 6
133+85	26	93	27 1	10 1	63 6	17 3	24 3
132+50	66	11 3	29 9	8 2	58 8	17 7	23 1
167+50	0 0	7 7	22 9	67	69 4	24 6	24 3
260+30	3 4	06	16 0	67	83 4	21 4	20 0
201+00	4 4	80	23 0	3 4	69 0	19 7	20 0
467+50	0 0	02	8 8	17 7	91 0	30 2	43 1
	71+50 129+50 133+85 132+50 167+50 260+30 201+00	71+50 14 1 129+50 1 1 133+85 2 6 132+50 6 6 167+50 0 0 260+30 3 4 201+00 4 4	71+50 14 1 28 2 129+50 1 1 9 6 133+85 2 6 9 3 132+50 6 6 11 3 167+50 0 0 7 7 260+30 3 4 0 6 201+00 4 4 8 0	71+50         14 1         28 2         23 5           129+50         1 1         9 6         29 5           133+85         2 6         9 3         27 1           132+50         6 6         11 3         29 9           167+50         0 0         7 7         22 9           260+30         3 4         0 6         16 0           201+00         4 4         8 0         23 0	sta         material         clay           71+50         14 1         28 2         23 5         2 9           129+50         1 1         9 6         29 5         6 3           133+85         2 6         9 3         27 1         10 1           132+50         6 6         11 3         29 9         8 2           167+50         0 0         7 7         22 9         6 7           260+30         3 4         0 6         16 0         6 7           201+00         4 4         8 0         23 0         3 4	sta         material         clay         clay           71+50         14 1         28 2         23 5         2 9 48 3           129+50         1 1         9 6 29 5         6 3 60 9           133+85         2 6         9 3 27 1         10 1 63 6           132+50         6 6         11 3 29 9 8 2 58 8           167+50         0 0         7 7 22 9 6 7 69 4           260+30         3 4         0 6 16 0 6 7 83 4           201+00         4 4         8 0 23 0 3 4 69 0	rate al         clay         clay         change           71+50         14 1         28 2         23 5         2 9 48 3         18 5           129+50         1 1         9 6         29 5         6 3 60 9         22 8           133+85         2 6         9 3 27 1         10 1 63 6         17 3           132+50         6 6         11 3 29 9 8 2 58 8         17 7           167+50         0 0         7 7 22 9 6 7 69 4 24 6           260+30         3 4 0 6 16 0 6 7 83 4 21 4           201+00         4 4 8 0 23 0 3 4 69 0 19 7

#### CONCLUSIONS

- 1 The cement-clay admixture appeared during construction, and shows in results since to be little if any different than the natural soil base
- 2 The porous bases show thus far much less cracking than do the natural soil and admixture of cement and soil bases
- 3 The increase in cracks during the second year show similarly favorable results for the porous bases
- 4 It is unsafe at this time to draw conclusions upon the sufficiency of 2, 4 or 6 inch porous bases to save the road maintenance an equivalent of their first cost

## IMPACT FORCES EXERTED BY THE MOTOR TRUCK ON THE HIGHWAY

JAMES A BUCHANAN

U & Bureau of Public Roads, Washington, D C

### THE COOPERATIVE MOTOR TRUCK IMPACT PROJECT

Two years ago, a progress report on the Motor Truck Impact Project was submitted to the Highway Research Board This project is cooperatively conducted by the Bureau of Public Roads, the Rubber Association of America, and the Society of Automotive Engineers All of the tests scheduled at that time have been completed and additional tests have also been made <sup>1</sup>

The investigation has so far been confined principally to the measurement of the vertical reaction between the road and the wheel and determination of the influences of tire equipment, load, speed, and road surface roughness. The procedure and apparatus are substantially as outlined in the earlier report, and may be found in detail in the June. 1926, issue of *Public Roads* 

The results of the tests reported below are illustrative of the effects of the variables and are believed to be generally accurate within 10 per cent. They were obtained with equipment specified by a joint committee representing the three agencies cooperating in the Motor Truck Impact Tests, and the results apply specifically to the tire equipments used, which were standard at the time of the tests

The term "cushioning effect" as used refers only to the vertical reaction between the road and the wheel, and, although exerting an influence thereon, is not to be confused with the popular term

<sup>&</sup>lt;sup>1</sup> More than 150 truck and tire combinations have been tested to date