

PREFABRICATED BRIDGE ELEMENTS AND SYSTEMS

TRANSPORTATION RESEARCH BOARD National Research Council

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2101 Constitution Avenue Washington, D.C. 20418

REPLY TO: Robert J. Reilly 202/334-3224

October 28, 1985

TO: CHIEF ADMINISTRATIVE OFFICERS STATE HIGHWAY AND TRANSPORTATION DEPARTMENTS

SUBJECT: National Cooperative Highway Research Program Synthesis of Highway Practice 119, "Prefabricated Bridge Elements and Systems," the Final Report on Project 20-5, Topic 15-10, of the FY '83 Program

I am enclosing one copy of the synthesis report resulting from research administered by the National Cooperative Highway Research Program. The research was conducted by the Transportation Research Board. In accordance with the selective distribution system of the Transportation Research Board, copies of this report will be directed to all persons having requested the subject areas of Maintenance, Structures Design and Performance, and Cement and Concrete together with the highway transportation mode.

The NCHRP staff has provided a foreword that succinctly summarizes the scope of the work and indicates the personnel who will find the results of particular interest. This will aid in its distribution within your department and in practical application of the research findings. These findings add substantially to the body of knowledge concerning prefabricated elements that can be used to construct new bridges or rehabilitate existing bridges. The major benefit from use of the procedures and materials described in this report is the minimizing of the reduction in level of service to motorists due to bridge construction and rehabilitation.

Sincerely yours, Thomas B. Deen

Executive Director

Enclosure

NATIONAL COOPERATIVE HIGHWAY RESEARCH PROGRAM 119

PREFABRICATED BRIDGE ELEMENTS AND SYSTEMS

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RESEARCH SPONSORED BY THE AMERICAN ASSOCIATION OF STATE HIGHWAY AND TRANSPORTATION OFFICIALS IN COOPERATION WITH THE FEDERAL HIGHWAY ADMINISTRATION

TRANSPORTATION RESEARCH BOARD

NATIONAL RESEARCH COUNCIL WASHINGTON, D.C.

AUGUST 1985

NATIONAL COOPERATIVE HIGHWAY RESEARCH PROGRAM

Systematic, well-designed research provides the most effective approach to the solution of many problems facing highway administrators and engineers. Often, highway problems are of local interest and can best be studied by highway departments individually or in cooperation with their state universities and others. However, the accelerating growth of highway transportation develops increasingly complex problems of wide interest to highway authorities. These problems are best studied through a coordinated program of cooperative research.

In recognition of these needs, the highway administrators of the American Association of State Highway and Transportation Officials initiated in 1962 an objective national highway research program employing modern scientific techniques. This program is supported on a continuing basis by funds from participating member states of the Association and it receives the full cooperation and support of the Federal Highway Administration, United States Department of Transportation.

The Transportation Research Board of the National Research Council was requested by the Association to administer the research program because of the Board's recognized objectivity and understanding of modern research practices. The Board is uniquely suited for this purpose as: it maintains an extensive committee structure from which authorities on any highway transportation subject may be drawn; it possesses avenues of communications and cooperation with federal, state, and local governmental agencies, universities, and industry; its relationship to the National Research Council is an assurance of objectivity; it maintains a full-time research correlation staff of specialists in highway transportation matters to bring the findings of research directly to those who are in a position to use them.

The program is developed on the basis of research needs identified by chief administrators of the highway and transportation departments and by committees of AASHTO. Each year, specific areas of research needs to be included in the program are proposed to the National Research Council and the Board by the American Association of State Highway and Transportation Officials. Research projects to fulfill these needs are defined by the Board, and qualified research agencies are selected from those that have submitted proposals. Administration and surveillance of research contracts are the responsibilities of the National Research Council and its Transportation Research Board.

The needs for highway research are many, and the National Cooperative Highway Research Program can make significant contributions to the solution of highway transportation problems of mutual concern to many responsible groups. The program, however, is intended to complement rather than to substitute for or duplicate other highway research programs.

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NOTICE

The project that is the subject of this report was a part of the National Cooperative Highway Research Program conducted by the Transportation Research Board with the approval of the Governing Board of the National Research Council. Such approval reflects the Governing Board's judgment that the program concerned is of national importance and appropriate with respect to both the purposes and resources of the National Research Council.

The members of the technical committee selected to monitor this project and to review this report were chosen for recognized scholarly competence and with due consideration for the balance of disciplines appropriate to the project. The opinions and conclusions expressed or implied are those of the research agency that performed the research, and, while they have been accepted as appropriate by the technical committee, they are not necessarily those of the Transportation Research Board, the National Research Council, the American Association of State Highway and Transportation Officials, or the Federal Highway Administration of the U.S. Department of Transportation.

Each report is reviewed and accepted for publication by the technical committee according to procedures established and monitored by the Transportation Research Board Executive Committee and the Governing Board of the National Research Council.

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The Transportation Research Board evolved in 1974 from the Highway Research Board, which was established in 1920. The TRB incorporates all former HRB activities and also performs additional functions under a broader scope involving all modes of transportation and the interactions of transportation with society.

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PREFACE

A vast storehouse of information exists on nearly every subject of concern to highway administrators and engineers. Much of this information has resulted from both research and the successful application of solutions to the problems faced by practitioners in their daily work. Because previously there has been no systematic means for compiling such useful information and making it available to the entire highway community, the American Association of State Highway and Transportation Officials has, through the mechanism of the National Cooperative Highway Research Program, authorized the Transportation Research Board to undertake a continuing project to search out and synthesize useful knowledge from all available sources and to prepare documented reports on current practices in the subject areas of concern.

This synthesis series reports on various practices, making specific recommendations where appropriate but without the detailed directions usually found in handbooks or design manuals. Nonetheless, these documents can serve similar purposes, for each is a compendium of the best knowledge available on those measures found to be the most successful in resolving specific problems. The extent to which these reports are useful will be tempered by the user's knowledge and experience in the particular problem area.

FOREWORD

By Staff Transportation Research Board This synthesis will be of interest to bridge designers, maintenance and construction personnel, and others concerned with the design, maintenance, and rehabilitation of bridges. Information is presented on the use of prefabricated elements that can be used to construct new bridges or rehabilitate old ones.

Administrators, engineers, and researchers are continually faced with highway problems on which much information exists, either in the form of reports or in terms of undocumented experience and practice. Unfortunately, this information often is scattered and unevaluated, and, as a consequence, in seeking solutions, full information on what has been learned about a problem frequently is not assembled. Costly research findings may go unused, valuable experience may be overlooked, and full consideration may not be given to available practices for solving or alleviating the problem. In an effort to correct this situation, a continuing NCHRP project, carried out by the Transportation Research Board as the research agency, has the objective of reporting on common highway problems and synthesizing available information. The synthesis reports from this endeavor constitute an NCHRP publication series in which various forms of relevant information are assembled into single, concise documents pertaining to specific highway problems or sets of closely related problems.

Prefabricated bridge elements can be used to reduce design effort, simplify construction, and reduce delay to the traveling public. This report of the Transportation Research Board presents information on how highway agencies have used prefabricated elements, problems that were encountered and their solutions, costs, and benefits. To develop this synthesis in a comprehensive manner and to ensure inclusion of significant knowledge, the Board analyzed available information assembled from numerous sources, including a large number of state highway and transportation departments. A topic panel of experts in the subject area was established to guide the researcher in organizing and evaluating the collected data, and to review the final synthesis report.

This synthesis is an immediately useful document that records practices that were acceptable within the limitations of the knowledge available at the time of its preparation. As the processes of advancement continue, new knowledge can be expected to be added to that now at hand.

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Valuable assistance in the preparation of this synthesis was provided by the Topic Panel, consisting of Bernard F. Kotalik, Region Manager, Robson-Downes Associates; Warren J. Sunderland, Assistant Chief Engineer, Bridges and Structures Division, New Jersey Department of Transportation; and Carl E. Thunman, Rochester, Illinois; and Liaison Member Walter Podolny, Structural Engineer, Bridge Division, Federal Highway Administration.

William G. Gunderman, Engineer of Materials and Construction, Transportation Research Board, assisted the NCHRP Project 20-5 Staff and the Topic Panel.

Information on current practice was provided by many highway and transportation agencies. Their cooperation and assistance were most helpful.

PREFABRICATED BRIDGE ELEMENTS AND SYSTEMS

SUMMARY

Prefabricated elements and systems are usually used to achieve economy through the repeated use of forms and to reduce on-site construction time and labor by concentrating the construction effort in a fabrication facility rather than at the bridge site. The use of the elements can reduce design effort, reduce the impact on the environment in the vicinity of the site, and minimize the delays and inconvenience to the traveling public, saving time and money.

Many prefabricated elements and systems are available for use in highway bridge construction. The most frequently used elements are the prestressed concrete I-beam, precast and prestressed box beam, precast and prestressed channel, and precast slab span. In recent years, steel stay-in-place forms, prestressed concrete subdeck panels, precast parapets, and precast full-depth deck panels have been used on an increasing number of bridges. Prefabricated steel orthotropic plate deck units have been used to achieve a reduction in deadload and allow for deck replacement during off-peak traffic periods. Glued-laminated timber members have been used to replace bridges on rural roads.

As the highway program moves from an era of bridge construction to one of bridge maintenance, rehabilitation, and replacement, the use of prefabricated elements and systems will certainly increase. Bridges subjected to high volumes of traffic can usually be closed for repair only during off-peak traffic periods. Prefabricated elements that can be installed and opened to traffic in a short period of time provide a practical way to repair these bridges. Because of the large number of bridges on low-volume roads in need of repair, rehabilitation, and replacement, identical, mass-produced elements, which may be quickly assembled, will be used to reduce design time and cost, minimize forming and labor costs, and minimize lane closure time.

Early problems with the use of prefabricated elements have been largely eliminated, and bridges containing the elements are expected to provide many years of service with minimal maintenance. The most significant continuing problem is the high cost of the elements in areas where they are not readily available or where demand is insufficient to justify mass production. Even at a higher cost, the use of the elements on bridges subjected to high volumes of traffic can be justified because excessive lane closure times can be avoided.

Significant evolution has occurred in the use of prefabricated elements and systems. Early efforts centered on precasting, and later prestressing, of single elements such as slab spans, channels, and I-beams. Acceptance and use of the elements increased with improvements in quality control and efficiency at precast plants. Efforts were expanded to include the substructure and portions of the deck as precast subdeck panels gained acceptance. The connections between elements surfaced as a major area of concern as innovators attempted to prefabricate the deck and the parapet and every other element of a bridge. These problems are gradually being resolved with improvements in the design of connections and with developments in high-early-strength, quick-setting materials, such as polymers. It is currently possible to economically replace almost any portion of a bridge with a prefabricated element and to complete the installation during off-peak traffic periods and with a minimum of disruption to the environment.

2

CHAPTER ONE

INTRODUCTION

The synthesis reports both the state of the art and the state of the practice for prefabricated bridge elements and systems and is based on a review of pertinent literature and ongoing research along with an examination of current practices.

Many prefabricated elements and systems are available for highway bridge construction. Prefabricated elements and systems can be used with less disruption at the site, can reduce much of the environmental impact in the surrounding areas during construction, can reduce design effort, and can speed up field construction, saving time and money.

Prefabricated elements and systems currently utilized for bridges are listed in NCHRP Report 222 (1) and NCHRP Report 243 (2). Descriptions of these are reproduced herein as Appendix A. To help condense the synthesis, the synthesis panel ranked these elements and systems and concluded that the synthesis should focus primarily on the six elements and systems that were believed to be more promising or most frequently used: precast concrete slab spans (C-1 in Appendix A), precast box beams (C-2), prestressed I-beams (C-8), precast deck panels (S-3), permanent bridge-deck forms (M-4), and parapet and rail systems (M-5). However, the synthesis also covers the other systems in Reports 222 and 243 as well as additional systems that have potential.

STATEMENT OF PROBLEM

Although much of the information that would be in a synthesis on prefabricated bridge elements and systems has been published in NCHRP Reports 222 and 243, the titles of these reports give no indication of this because the reports were aimed at rehabilitation and replacement methods for bridges on secondary roads. One of the methods was the use of prefabricated elements and systems, and 32 of these are covered in Reports 222 and 243. However, the nature of the information is more like a catalog than a synthesis; that is, there is no information on successes, problems, costs, reasons for selection, etc. This synthesis is a compilation of this kind of information and adds to that contained in NCHRP Reports 222 and 243.

PURPOSE AND SCOPE

This synthesis is a study and evaluation of the systems from NCHRP Reports 222 and 243 noted above including history of use, reasons for use, fabrication, construction and maintenance practices, structural effectiveness, cost-effectiveness, serviceability, durability, resolved and unresolved problems, and other aspects. The other systems from NCHRP Reports 222 and 243 are also covered in the synthesis, although in less detail, as well as any additional systems that were found in the literature or practice that have potential.

For the synthesis, a prefabricated bridge element is defined as a part of a bridge that is fabricated or assembled away from its final position and used to minimize design effort, on-site construction time, or disruption or environmental impact in the vicinity of the site. A prefabricated bridge system is a combination of prefabricated bridge elements. Structural steel beams and solid sawn timber members are not considered as prefabricated elements. A bridge is defined as a structure having a span of 20 ft (6 m) or greater (although there is no reason that prefabricated elements cannot be used on shorter spans).

BACKGROUND

The synthesis results from a survey of the literature, the identification of ongoing research, and a compilation of information on the past and present practices of transportation agencies. Much information on past and present practices was obtained from a questionnaire that was distributed to the bridge engineers in most of the 50 states, the District of Columbia, and other selected transportation authorities (Appendix B). They were asked to complete the questionnaire with regard to the use of prefabricated bridge elements and systems in bridges under their authority. They were questioned on the six types of prefabricated elements considered by the synthesis panel to be the most promising. In addition, space was provided for answers to questions about other prefabricated bridge elements or systems that they use. In addition to information on the type and frequency of use of an element, questions on how, when, where, and particularly why an element or system was used were asked. Also, questions were asked about the fabrication and transportation of prefabricated elements; the construction, maintenance, and cost of bridges containing the elements; and resolved and unresolved problems with the elements or bridges containing the elements. It was requested that when possible, answers be based on information on record, but good estimates would be accepted if precise answers were not feasible. Appendix B provides a summary of the responses to the questionnaire.

Thirty-six usable responses were received including replies from 34 states, the District of Columbia, and Alberta. The responding agencies (excluding Alberta, which is responsible for 6,000 bridges) were responsible for approximately 223,000 bridges or approximately 39% of the estimated 570,000 bridges in the United States (3). It is believed that the responses provide an accurate indication of the current practice of the use of prefabricated bridge elements and systems in the United States. The 36 responding agencies indicated that approximately 35,000 bridges (15%) contained prefabricated elements but only about 1,200 bridges (0.5%) contained a completely prefabricated superstructure. The use of prefabricated bridge elements is likely greater than that indicated by the questionnaire for two reasons. First, prefabricated elements lend themselves to mass production and use on multispan bridges; therefore the percentage of bridge spans with prefabricated elements is likely to be higher than the

percentage of bridges with prefabricated elements. Second, prefabricated bridge elements are frequently used on secondary highways and local roads, and many are not under the authority of the state highway and transportation departments that responded to the questionnaire. Obviously, a significant number of bridges contain prefabricated elements and a discussion of the most popular elements follows.

CHAPTER TWO

MOST POPULAR PREFABRICATED ELEMENTS

Table 1 shows the use of prefabricated elements based on the responses to the questionnaire. The table shows the number and percent of responding agencies reporting use of the elements and the number and percent of bridges in which the elements have been used. Information on the first seven elements was requested in the questionnaire and zero answers were recorded as a response but blanks were not. The responses for the last five elements were volunteered and therefore there were no zero-use replies; it is reasonable to expect that the number of users is somewhat greater than indicated by the responses.

TABLE 1

USE OF PREFABRICATED ELEMENT	s
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		Agencies Using		Bridg Used	es On
Element	Replies	No.	% ^a	No.	% ^b
Precast concrete slab span	34	26	76	3,002	1.3
Precast box beam	34	26	76	5,948	2.6
Prestressed I-beam	36	35	97	18,299	8.0
Precast deck panel	29	5	17	8	c
Steel stay-in-place for m	22	18	82	1,926	0.8
Prestressed subdeck panel	21	14	67	702	0.3
Precast parapet	26	8	31	331	0.1
Double-tee and channel	9	9 ^d	-	4,482	2.0
Single-tee	3	3^{d}	-	25	c
Precast substructure	4	4 ^d	-	22	c
Bulb-tee	2	2^{d}	-	18	c
Other	8	8 ^d	-	32	c

^aPercentage of the agencies responding to the survey.

^bPercentage of the 229,000 bridges under the jurisdiction of the responding agencies.

^CLess than 0.1 percent.

Responses to the questionnaire indicated that the most frequently used prefabricated element is the prestressed concrete I-beam, which was used in approximately 18,300 bridges or 8% of the population included in the survey. The second most commonly used element is the precast concrete box beam, which was used in approximately 6,000 bridges or 3% of the population included in the survey. The precast concrete double-tee or channel beam is the third most frequently used element as it has been used in approximately 4,500 bridges or 2% of the population included in the survey. However, approximately 3,000 of these bridges are located in Alberta. The double-tee and channel accounted for 95% of the bridges with elements for which information was volunteered under the other elements category of the questionnaire. The fourth most frequently used element is the solid or voided slab span. Approximately 3,000 bridges or more than 1% of the population included in the survey contain the slab span. Approximately 2,600 bridges contain prefabricated steel or concrete forms that are a permanent part of the deck. Only approximately 300 bridges were reported to contain a precast parapet and on about half of these bridges the use was temporary for purposes of construction. Only eight bridges were reported to have precast concrete deck panels. Other occasionally used elements noted from the questionnaire included precast single-tee beam, precast substructure elements (such as reinforced earth, piles, bents, and piers), and precast bulb tees. The Alaska Department of Transportation reported that the bulb tee was used on many bridges but did not cite a number.

PRECAST CONCRETE SLAB SPANS

Precast concrete slab spans (Figure 1) may be fabricated in various lengths and widths to accommodate a range of spans and roadway widths. Solid slabs are frequently used for spans up to 30 ft (9 m) but more structurally efficient pretensioned or post-tensioned or voided slabs are commonly used for longer spans (4, 5). Slabs are very easy to transport and erect.

Shear transfer between slabs is usually provided by a grouted keyway or by weld plates $(5, \delta)$. Special consideration should

^dThe number of agencies using is the same as the number of replies because information on these elements was volunteered.



Figure 1 Precast slab spans.

be given to the connection details because premature cracking in the wearing surface and early failures of the system have been attributed to keyway and weld-plate failures (7). Martin provides detailed coverage of the problems and solutions to the problems with the connections between modular precast concrete elements (7).

Most precast concrete producers are properly equipped to produce slabs. Also, some state and local bridge crews fabricate the slabs because of the ease with which the slabs can be precast. The slabs can be precast by maintenance forces during off-peak maintenance periods when there is a surplus of labor (6, 8).

The slabs are particularly suited for the rapid replacement of short-span superstructures because they are easily installed while traffic is maintained in an adjacent lane (9). Figure 2 illustrates a bridge maintenance crew replacing a superstructure of steel beams and timber decking with precast concrete slab spans while stopping traffic on the secondary road for very short periods of time. Because the individual slabs are usually not designed to support an HS20-44 loading without being connected, one lane of traffic can usually be maintained as the slabs are placed by limiting the loads that cross the bridge or by connecting the slabs as they are placed. When replacing a lighter superstructure, the capacity of the substructure should be evaluated to ensure that it can support the weight of the slabs.

The most frequently used alternatives to the precast slab span are the culvert (system M-8 in Appendix A), cast-in-place (CIP) concrete, and steel beams with a CIP concrete deck (system S-9).

Examples of the use of precast slab spans can be found in many states. The slabs are frequently used in Illinois, Indiana, Kentucky, New York, North Carolina, Oregon, Virginia, and Alberta, where each has used the slabs on 100 to 500 bridges. Six percent of the bridges in Kentucky contain the slab.

PRECAST BOX BEAMS

Precast box beams (Figure 3) are usually pretensioned but may be post-tensioned and may be precast in various lengths and widths to accommodate a range of spans and roadway widths. Box beams are generally used for spans of approximately 50 to 100 ft (15 to 30 m) (4). Except for the longer spans, the boxes are very easy to transport and erect. Box beams that are placed adjacent to each other are usually connected in the same way slabs are connected (5). A wearing surface is usually used with the box beams. Box beams that are spaced apart (spread boxes) are tied together with diaphragms and a CIP concrete slab is added (10). Like the slab spans, the box is particularly suited for the replacement of short-span superstructures. More expertise is required to fabricate a box than a slab because the box is usually prestressed and because the proper location of the void material must be maintained during the casting operation. Most prestressed concrete producers can manufacture the boxes, usually pretensioned, and occasionally state and local bridge crews have fabricated the boxes, usually conventionally reinforced (8).

The most frequently used alternatives to the box are CIP concrete and steel beams with CIP concrete deck.

Examples of the use of the boxes can be found in many states. The boxes are frequently used in California, Illinois, Indiana, Kentucky, New York, North Dakota, Ohio, Pennsylvania, Texas, Virginia, and West Virginia, where each has used the boxes on 100 to 1,500 bridges. Nineteen percent of the bridges in North Dakota contain box beams.

PRESTRESSED I-BEAMS

The precast, pretensioned I-beam (Figure 4) is widely used because forms for precasting the member are readily available, and the standard cross sections simplify design practice and lead to cost savings (11). The beams are usually used for spans of 40 to 100 ft (12 to 30 m), but spans up to 140 ft (43 m) are reported in the literature (4, 12). A CIP concrete deck is usually used. Although most decks are constructed with removable forms, the current trend is toward the use of permanent forms, such as steel stay-in-place forms or prestressed concrete subdeck panels. Construction time and safety are improved through the use of permanent forms (13, 14). Because of the large amount of CIP concrete required for the deck, other systems better lend themselves to rapid bridge replacement. However, the I-beams provide more rapid construction than CIP concrete beams.

Most prestressed concrete producers can fabricate the beams and they would seldom be cast by state or local crews. The most frequently used alternative to the prestressed I-beam is the steel beam, either the standard rolled shape or the plate girder.

Examples of the use of the I-beam can be found in many states. The I-beam is frequently used in California, Colorado, Georgia, Kentucky, Minnesota, Montana, North Dakota, Pennsylvania, Texas, Virginia, and Washington, where they have been used in approximately 750 to 4,000 bridges. Approximately one third of the bridges in Colorado, Montana, and Washington contain prestressed I-beams.

In recent years, some state highway agencies have developed modified versions of the AASHTO girder that provide more economical cross sections (15-17). According to a recent study,



Figure 2 Precast slab spans replace substandard steel stringer-timber deck superstructure (6).

a new series of sections called the modified bulb-T, shown in Figure 5, can provide savings of up to 17% when used to replace the AASHTO Type IV, V, and VI beams in spans greater than 80 ft (25 m) (17, 18).

PRECAST DECK PANELS

One of the more recent innovations in the use of prefabricated elements is the use of precast concrete deck panels (Figure 6) that are placed on steel stringers (19-25). Shear transfer between transverse panels is usually achieved with grouted keyways or a CIP concrete joint (17, 19, 20, 21, 24). Transverse panels may be post-tensioned parallel to the direction of traffic to improve shear transfer between panels (20, 23). Proper vertical alignment and uniform bearing on the top flanges of the supporting string-

ers can be obtained by placement of a bed of grout or epoxy mortar before setting the slabs, by use of shim pads with grout placed after the panels are placed on the shims, or by use of a detail that includes adjustable slab support on angles or bolts while grout or epoxy mortar is placed (25).

To develop composite action between the deck panel and the stringers, the connection must be adequate to transfer horizontal shear. Composite action was not achieved in the earlier bridges in which the panels were typically attached to the stringers with clips and bolts (19-21). Composite action is being achieved in the more recently constructed bridges through the use of studs or bolts as shear connectors (22, 24). The studs may be welded to the top flange of the stringers, or holes for high-strength bolts may be drilled in the top flanges. The shear connectors may be placed before or after the slabs are positioned, but if they are installed before, it is necessary to fabricate and erect the slabs



Figure 3 Precast box beams.



Figure 4 Prestressed I-beams.

with more precision. The voids around the studs or bolts are typically filled with nonshrink grout or epoxy mortar.

The deck panels eliminate most of the on-site formwork and concreting typically required for a steel stringer-concrete deck bridge (22, 25). Most precast-concrete producers can fabricate the slabs; based on the questionnaire responses, state or local

crews have not fabricated them to date. The use of the slabs to replace the deck of a bridge near Mount Vernon, Virginia is shown in Figure 7.

Berger (25) discusses the use of precast, prestressed bridge deck panels on steel and prestressed concrete beams. He gives several details that can be used for connecting precast panels



Figure 5 Modified bulb-T proposed to replace standard AASHTO-PCI type IV, V, and VI sections (Concrete Technology Laboratories).

to beams, both on new construction and for replacement of existing bridge decks. Berger concludes that the precast slabs are more economical than CIP concrete decks because they may be pretensioned or post-tensioned and therefore are more structurally efficient, requiring less material and fewer supporting elements, and because on-site construction costs are less as the precast slabs may be installed in less time.

The rehabilitation of the Fremont Street Bridge near Pittsburgh utilized precast deck panels set on the floor beams of a concrete arch bridge (26). These panels have the attributes of both deck panels and slab spans; they are longitudinally reinforced two-span continuous slabs (Figure 8). Leveling bolts were used to adjust the elevation of the slabs and dowels were placed and grouted into holes in the slabs and the floor beams to anchor the slabs. Polymer mortar was pumped under the neoprene bearing pads to rigidly connect the slabs to the floor beams after the panels were post-tensioned transversely.

A recent example of the use of precast deck panels on steel beams was the replacement of the deck on the Woodrow Wilson Memorial Bridge on I-495 around Washington, D. C. (17, 23, 27). The deck of the 5,900-ft (1800-m) long, six-lane bridge was replaced during a period of twelve months without halting the flow of traffic, which averaged 125,000 vehicles per day.

The major work on the bridge was done each night for 10 hours, leaving open two of the six lanes to traffic as illustrated in Figure 9. A concrete-cutting circular saw cut the existing deck away in 40-ton (36 Mg) segments. These segments were replaced by precast, lightweight concrete panels that were posttensioned transversely at the plant. A typical panel was 46 ft 8 in. wide, 10 to 12 ft long, and 8 in. thick (14.2 m wide, 3.0 to 3.6 m long, and 200 mm thick). The new panels widened the bridge by 4 ft (1.2 m). After placement, the panels were posttensioned longitudinally in groups of 17 to reduce cracking, seal the transverse joints between adjacent panels, and eliminate water intrusion.

The concrete deck panels are supported by CIP polymer concrete bearing pads on the exterior girder and interior stringers. The polymer concrete is a methyl methacrylate product that reached 4,000 psi (27.6 kPa) compressive strength after one hour and 8,000 psi (55 kPa) after 24 hours. Each pad includes







Figure 7 Precast deck panel is lowered onto stringers, which are covered with epoxy mortar (24).

a sliding steel bearing plate on the stringer's flange that is tied into the polymer concrete by welded studs. The sliding plates prevent the introduction of stresses in the structural steel caused by shrinkage, creep, and foreshortening during post-tensioning of the deck.

Each night the contractor covered the gap between the old and the new deck with a steel grating deck that carried traffic during the day. The following night, crews lifted away the grating to install new deck while other workers removed concrete.

The redecking of the Woodrow Wilson Bridge exemplifies how, with proper planning and design that takes advantage of recent developments in high-early-strength materials and technology, prefabricated deck panels can be erected and connected with a minimum of disruption to the environment and at a savings to the public.

The alternative to the precast concrete deck panels is CIP concrete, which requires considerable on-site construction time and subsequent lane closure time for strength development (24, 25). Precast concrete deck panels have been used in a limited number of states but an increase in use is anticipated as highway agencies are confronted with replacing the decks of bridges during off-peak traffic periods and with minimal lane closure time. Although the New York Thruway Authority has not experienced the cost savings and reduced construction time anticipated, their nine years of experience indicates that precast panels are an acceptable approach to deck replacement (2). Other examples of the use of the panels in highway bridges can be found in Alabama, California, Indiana, Maryland, Massachusetts, New York, Pennsylvania, Virginia, and West Virginia. Examples of use on railroad bridges can be found in Delaware, New Mexico, and British Columbia (24).

PERMANENT BRIDGE-DECK FORMS

The concrete required for site-cast concrete bridge decks must be formed with temporary or permanent bridge-deck forms. In recent years, steel stay-in-place forms and prestressed concrete subdeck panels (Figure 10) have become popular because the high cost of the form removal is eliminated (7, 14, 28). Prestressed concrete subdeck panels provide an added advantage in that less concrete and reinforcing steel must be placed at the bridge site because the panels become an integral part of the deck. Most prestressed concrete producers can fabricate the subdeck panels, and the steel forms are available from most steel fabricators.



Figure 8 Use of precast deck panels in rehabilitation of Fremont Street bridge.



Figure 9 Precast post-tensioned lightweight concrete panels were installed at night to replace the deck of the Woodrow Wilson Bridge (23).

The prestressed panels are usually pretensioned and precast in widths of approximately 4 ft (1.2 m), but have been precast in widths of up to 8 ft (2.4 m), and in lengths that are controlled by the spacing of the beams in the bridge (29). On earlier installations the panels were set on a grout bed, approximately $\frac{1}{2}$ in. (13 mm) thick, which was placed along the supporting edge of the beams in the bridge (see Figure 11). The grout provided for the uniform bearing of the panel by compensating for camber and surface irregularities. Because the panels are a constant thickness, they followed the camber in the supporting beams, and the thickness of the CIP concrete typically varied from a maximum at the bearings to a minimum at midspan. On more recent installations the thickness of the grout bed was varied to account for the camber in the supporting beams and to provide a deck of constant thickness.

The rectangular panels can be used on skewed bridges by cutting the end panels to the desired skew with a portable power saw and a concrete cutting blade (29). The installation of the panels can proceed rapidly with a minimum of labor and without the need for temporary platforms. Once the panels are in place, the finished grade of the deck surface can be set and the required concrete for the overlay placed.

Although cracks will usually occur in the deck surface directly above the butt joints between the panels, the cracks typically extend only halfway through the CIP concrete and are not believed to have a significant effect on the performance of the deck (29). Epoxy-coated rebar can be used for the top mat of the steel in the deck or calcium nitrite can be used in the concrete to curtail the corrosion that might be accelerated by the presence of moisture and salt in the cracks.

Considerable laboratory and field work to evaluate prestressed concrete subdeck panels has been conducted (7, 29-33). Composite action between the panel and the CIP concrete and across adjacent panels has not been a problem (7, 14, 29, 30, 32). The experience to date has generally been good and indicates the panels provide a suitable method for forming a bridge deck

(28, 32, 34). Unfortunately, a recent study for the Florida Department of Transportation concluded that the majority of the approximately 200 bridges that were constructed in Florida with the subdeck panels will have a reduced service life (32, 33). According to the study, the panels in these bridges do not have positive bearing on the girders because they were placed on fiberboard strips rather than grout. The study recommends that positive bearing be required on future subdeck panel installations and that the prestressing strand extensions should be beneficial in maintaining continuity between the panels and the CIP concrete (32). On the other hand, the Illinois Department of Transportation, which considers subdeck panels to be a viable and cost-effective concept, requires that the strand extensions be removed because they interfere with the placement of the shear connectors and the bearing grout (34). Obviously, the state of the art is being refined as the prestressed subdeck panels gain wider acceptance.

Like the prestressed concrete subdeck panels, the steel stayin-place forms can be placed with a minimum of labor. Metal screws are usually used to fasten the forms to metal angles that have been field welded to supporting devices at the proper elevation. The supporting devices are precast into the top flange of a concrete beam and hang from the top flange of a steel beam (see System M-4 in Appendix A).

Opinions vary as to the advantages and disadvantages of using steel stay-in-place forms. Corrosion of the forms can be a problem if moisture has ready access to the form by drainage; penetration through poor quality, permeable concrete; or via other means. The forms are generally accepted in many states that believe the advantages outweigh the potential disadvantages (14, 35, 36).

Examples of the use of the permanent bridge deck forms can be found in many states. The steel stay-in-place forms have been used on three times as many bridges as the prestressed subdeck panels. The steel stay-in-place forms have been used in Georgia, Maryland, and Virginia, where each has used them on 450 to



Permanent Steel Forms



Prestressed Concrete Subdeck Panels

Figure 10 Permanent bridge-deck forms.



Figure 11 Prestressed subdeck panels are set on a grout bed, which is placed along the top edge of the supporting beam (Virginia Highway and Transportation Research Council photo).

650 bridges, and in Pennsylvania, where they have been used on 90% of the bridges built in the last 10 years. The prestressed concrete subdeck panels have been used in Georgia, Illinois, and Texas, where each has used them on 150 to 200 bridges. Approximately 28% of the bridges in Maryland contain steel stay-in-place forms and 3% of the bridges in Illinois contain prestressed concrete subdeck panels.

PRECAST PARAPET

Because placing the forms for conventional CIP concrete parapets can be a costly and time-consuming job, precast parapets have been used in some states in recent years. The parapet lends itself ideally to prefabrication as it has a constant shape suitable for mass duplication (see Figure 12) and is used in sufficient volume statewide to make precasting economical. The standard precast parapets, typically 8 to 12 ft (2.4 to 3.7 m) long, are fabricated upside down to help eliminate honeycombing.

With the aid of a light truck crane, three workers can place and connect the 2-ton (1.8-Mg) parapet sections on a three-span structure in two or three days (37). The parapets may be set in cement mortar spread on top of the deck or they may be set on temporary wooden shims and grouted. The parapets may be anchored to the bridge deck in several ways, which include the use of stainless steel bolts that extend through the base of the parapet and the deck and the use of threaded metal rods that screw into inserts precast into the deck and extend upward through voids cast into the parapet (4, 38). Portland cement mortar is usually used to grout the voids and anchor the parapet. A problem with water and salt leaking between the base of the parapet and the deck needs to be resolved.

Examples of the use of the precast parapet can be found in Missouri, Pennsylvania, Texas, and Virginia, where each has used precast parapets on up to approximately 150 bridges.

DOUBLE-TEE AND CHANNEL

Most prestressed concrete producers have forms in several standard sizes to allow the production of pretensioned or posttensioned double-tee and channel beams (Figure 13) for a range of span lengths (4, 10). However, available forms may not be suitable for the fabrication of members that are heavy enough for bridge loadings (39). Double-tee and channel beams have been fabricated at the bridge site and at precasting plants (40, 41). Channels are usually fabricated in double-tee forms by blocking off a portion of the exterior flanges. Both the channel and double tee may be fabricated for use with or without a topping. Both members are among the easiest to transport and erect. The members are typically used for spans of 20 to 60 ft (6 to 18 m) (4). Shear transfer between the beams may be achieved through the use of grouted keyways or weld plates (40-42).

Numerous examples of the use of the channel can be found in Alberta where approximately 3,000 bridges (50%) contain the beam and in Arkansas, North Carolina, and Pennsylvania where each has used them on 200 to 700 bridges. Approximately 5% of the bridges in Arkansas contain the channel. The doubletee can be found in Missouri, New York, and Oklahoma where each has used them on 20 to 70 bridges.



Figure 12 Modular precast parapet is ideally suited for mass production (37).



Figure 13 Double-tee and channel.



Figure 14 Traffic was maintained as temporary timber planks were replaced with glulam panels (52).



Figure 15 Precast wing wall is placed into position on site-cast concrete footing (Hancock Concrete Products photo).

OTHER ELEMENTS

Brief descriptions and illustrations of numerous other prefabricated bridge elements and systems can be found in Appendix A. The elements are grouped according to the materials used for the primary element of the superstructure and are designated as concrete, steel, timber, or miscellaneous.

Steel Elements

Elsasser (43) reports that nearly all steel work is prefabricated into the largest subassemblies that can be reasonably shipped and handled. However, other than the conventional steel beam and plate girder, which have been used extensively in bridge construction, the use of prefabricated steel elements has been limited. Zuk (44) describes a number of innovative concepts that involve the use of prefabricated steel or aluminum elements in bridges that are relocatable, such as the Bailey bridge. He concludes that the military is at the forefront of the technological development of relocatable bridges.

Prefabricated elements of steel that have been frequently used in deck replacement are steel grids (system S-6 in Appendix A) (45) and orthotropic steel plates (system S-8). (46, 47). The elements are light and easy to install and therefore lend themselves to rapid deck replacement, particularly in situations where lanes can be closed for only short periods of time. The elements are relatively expensive and must be justified on the basis of reduced dead load and rapid installation. Open steel-grid decks have a low skid resistance; the skid resistance can be improved by filling the grids with concrete or installing studs.

The replacement of the deck on the George Washington Bridge was one of the more notable examples of the use of orthotropic steel plates. The panels, which were 11 ft wide and 60 ft long $(3.3 \times 18 \text{ m})$, were prefabricated with a 1 1/2 in. (38 mm) asphaltic concrete wearing surface (2, 48, 49). The panels were installed at night and exemplify how the use of prefabricated elements can minimize delays and inconvenience



Figure 16 Maintenance crew constructs prefabricated abutment (Vir ginia Highway and Transportation Research Council photo).

to the traveling public (50). Orthotropic steel plates are currently being used to replace the deck on the Golden Gate Bridge.

Timber Elements

Glued-laminated timber beams and deck panels, illustrated in systems S-4 and T-1 of Appendix A, provide examples of innovation in the use of prefabricated timber elements. Gluedlaminated (glulam) elements are preferred to solid, sawed elements because defects will be scattered and higher allowable stresses can be used in design. Elements may be laminated according to design stress so that economical, low-strength timbers can be placed in areas subject to low stress. In addition, laminated elements can be more uniformly treated with preservatives, drying shrinkage is more uniform, and elements may be fabricated to much larger dimensions than are available with solid, sawed timbers so that bridges may be assembled in a much shorter time as there are fewer elements to connect (51-54).

Since the late 1950s, glulam stringers and deck panels have been used on a number of bridges (52-58). A bridge with glulam panels on steel beams can be assembled 45% faster than one

with solid, sawn plank on steel beams (see Figure 14) (52). The glulam elements tend to be more expensive than alternative elements in some areas (52, 54) but can be economical for rural bridges where precast concrete and CIP concrete is not readily available (53). Timber bridges are widely used on low-volume roads in the National Forests, Canada, and the western part of the United States (53, 54, 59). The use of prefabricated elements of glulam timber illustrates how far timber bridge construction has advanced since the early native log stringer bridges, and the use of prefabricated elements is at the heart of the innovation.

Substructure Elements

The substructure often consumes 60 to 70% of the time required to construct a bridge (10, 37). Significant reductions in the time required to construct a bridge may be achieved by using prefabricated elements in the substructure as well as the superstructure. Although the number of bridges built with prefabricated substructure elements is low, significant innovation has occurred in recent years (4, 60, 61). Systems M-1 and M-2 of Appendix A illustrate the use of precast concrete abutments



Figure 17 Precast pier segments were lowered from the superstructure of the Linn Cove Viaduct.



and wing walls and prefabricated piling, piers, and caps. Willis (62) reports that county crews make precast abutment and wing wall panels during off-peak winter maintenance periods.

Figure 15 shows a precast wing wall element being placed into position as part of the construction of a precast concrete arch bridge located in Edina, Minnesota (see System M-7 of Appendix A). The 40-ft (12-m) span structure has a 10-ft (3-m) rise and consists of 12 precast arch elements, 2 precast spandrel end walls, and 4 2-piece precast wing wall elements (63). The elements were precast by a local manufacturer, trucked to the site, and positioned on site-cast concrete footings. Grout was used to fill the voids between the footings and the precast elements and a mastic was used to seal the joints. A typical bridge can be constructed in 7 to 14 days, which includes 5 to 10 days for excavation and construction of the footings, 1 to 2 days for setting the precast arch, end wall, and wing wall elements, and 1 to 2 days for backfilling (64). Approximately 100 precast concrete arch bridges have been constructed in Europe since 1967 (63, 64) and 13 bridges have been constructed in the United States since 1981 (Personal communication, Neal FitzSimons, Engineering Counsel, Kensington, Maryland, January 19, 1984).

Hanson (65) and GangaRao (66) have presented concepts for the use of prefabricated substructure elements, but such elements have seen only limited use because typically there are so many differences between bridge sites, such as soil bearing characteristics, the location of bedrock, and depth at which acceptable bearing can be obtained, that it is difficult to standardize these elements (67, 68). Successful results have often been obtained by prefabricating a part but not all of the substructure. For example, a prefabricated abutment was used in a bridge in Virginia by first constructing a level surface from which to work (the footing was site-cast concrete) and then placing the prefabricated abutment elements on top of the footing (Figure 16). Portland cement mortar was placed in the keyways between the elements and between the site-cast footing and the bottom of the elements, and two post-tensioning strands were used to tie the elements together.

The construction of the Linn Cove Viaduct along the side of Grandfather Mountain in North Carolina provides a spectacular example of the successful use of prefabricated elements in the substructure. To minimize the impact on the environment of the National Park, it was necessary to construct the substructure by working from the superstructure. After the pier foundation piles were placed in holes drilled into the ground, the forms and reinforcing steel for the footing were set. The bottom precast segment of the pier was then lowered into place and supported off the ground in its final position in the forms. Concrete was then site-cast in the footing beneath the bottom segment. After the footing concrete reached sufficient strength, other precast pier segments were placed on top of each other and post-tensioned until the pier was completed (Figure 17). With the completion of a pier, additional precast superstructure box segments were progressively placed and post-tensioned as the superstructure cantilevered past the completed pier to the location of the next pier (17).

Almost all concepts for using prefabricated concrete elements in the substructure require the use of either portland cement grout, mortar, concrete, or post-tensioning to tie the elements together. Whereas prefabricated elements are used routinely in the construction of bridge superstructures, their use in substructures is just beginning but looks promising and should be expanded.

PRACTICES AND PROBLEMS IN USE OF PREFABRICATED ELEMENTS

The questionnaire distributed for this synthesis asked agencies when, where, how, and why prefabricated elements were used. It also asked about problems, both those that had been solved and those that remained.

PERIODS OF USE

Table 2 shows the results of the response to a question as to when the prefabricated elements were used. The table shows the use in the time periods before 1965, 1965 through 1974, 1975 through 1984, and the use anticipated for the next 10 years. Results are in terms of the number of agencies indicating the element was used during the periods and the percent of bridges containing the element that were constructed by those agencies.

From the table it is obvious that the use of the elements has generally increased over the years, with the use during the past 10 years about equal to or exceeding the use during the 1965 to 1974 period. It is anticipated that during the next 10 years the use of deck panels on steel stringers will increase and the use of the other elements will be equal to or slightly less than the use during the past 10 years. The exception is that in Alberta the use of the double-tee and channel has declined over the years with low use anticipated over the next 10 years; because of the large number of bridges with these members in Alberta the trend is reflected in use based on percentage of bridges. In Alberta other prefabricated elements will be used rather than the double-tee or channel. Also, based on the percentage of bridges, the use of the precast parapet anticipated for the next 10 years is low because the majority of the use was in Virginia, and the Virginia response to the questionnaire did not cite anticipated use in terms of numbers of bridges.

WHERE THE ELEMENTS ARE USED

The results of the response to a question as to where the elements are used revealed that the elements are used on all types of roadways (high- or low-volume, Interstate, primary, or secondary roadways). The slab spans and box beams were used most often on the low-volume primary and secondary roadway. The I-beams and permanent deck forms were used equally on all systems. The parapet was used more often on the Interstate system and the number of bridges with deck panels on steel stringers was too small to draw conclusions.

TABLE 2

USE OF PREFABRICATED ELEMENTS BY HIGHWAY AGENCIES DURING VARIOUS TIME PERIODS

Element	Replies	Bef 19 No. ^a	ore 85 % ^b	1965- No.	1974 %	1975- No.	-1984 %	1985- No.	-1994 % ^C
Precast concrete slab span	27	15	22	20	27	20	51	18	89
Precast box beam	25	14	16	20	33	22	51	18	72
Prestressed I-beam	33	22	18	32	39	30	43	27	65
Precast deck panel	7	0	0	0	0	6	100	7	550
Permanent bridge-deck form	22	3	đ	8	36	20	64	16	47
Precast parapet	9	0	0	1	10	8	90	6	17
Double-tee and channel	9	1	51	5	37	9	12	7	14

^aNumber of responding agencies that used prefabricated elements during the period.

^bPercentage of total number of bridges containing the elements that were constructed during the period.

^cPercentage of the 1975-1984 use expected in 1985-1994.

dLess than 1%.

TYPES OF USES

The results of the questionnaire revealed that the elements were used for most types of construction; for new construction, the widening of a structure, and the replacement of a structure. The box beam, I-beam, permanent deck form, parapet, and double-tee and channel beam were used most often in new construction. The slab span and deck panel on steel beams were used slightly more often in bridge replacement than in new construction.

REASONS FOR USE OF THE ELEMENTS

Table 3 shows the results of the replies to the question as to why the elements were selected for use and, as would be expected, the principal reasons were to reduce first cost and to accelerate construction. Improved quality and reduced life-cycle cost were cited on a small percentage of the replies. The slab span and box beam were also frequently selected to minimize the depth of the superstructure and thereby provide more clearance below the structure. Low first cost, minimal maintenance, and rapid construction are frequently cited in the literature as reasons for using precast prestressed concrete elements (4, 11).

RESOLUTION OF PROBLEMS

According to replies to the questionnaire, a number of the early problems with the use of prefabricated elements have been resolved. The replies indicated that quality control at precast plants has improved, first costs have decreased, problems caused by a lack of experience have been eliminated, and elements have become more standard. Several replies also indicated that the problem of deck deterioration and rebar corrosion in slab spans and boxes have been solved by using CIP concrete overlays, epoxy-coated rebar, and/or waterproofing membranes.

The replies to the questionnaire also revealed that some construction problems have been eliminated because of the use of prefabricated elements and these include excessive on-site construction time, excessive depth of superstructure because thinner sections can be achieved with prestress, and the need for shoring and on-site form removal.

CONTINUING PROBLEMS

Based on the replies to the questionnaire, some problems with the use of prefabricated elements have continued and therefore the elements have not been used extensively. As can be seen from Table 4, the most frequently cited continuing problem was high first cost. A high percentage of the replies indicated no continuing problems and others cited length and weight limitations, deck deterioration and corrosion, and supply. Although connections have been cited as a problem in some of the literature (7, 11), those responding to the questionnaire noted it was a significant problem only for the precast parapet. Other problems cited at least once in the response to the questionnaire include inability to use slab spans and I-beams in continuous spans; inability to obtain a satisfactory design for slab spans, deck panels on steel beams, and prestressed subdeck panels; camber in I-beams; fabrication difficulties with box beams; poor REASONS ELEMENTS ARE USED

		Repl	ies N	oting Use	Indica	ted
Element	Replies	Accelerate Construction	Improve Quality	Reduce First Cost	Reduce Life-Cycle Cost	Other
Precast concrete slab span	27	19	3	18	2	8
Precast box beam	26	17	4	21	2	5
Prestressed I-beam	33	13	3	26	9	5
Precast deck panel	6	4	0	2	0	0
Permanent bridge-deck form	21	15	3	19	3	3
Precast parapet	10	8	1	8	1	1
Double-tee and channel	9	8	3	5	4	3

alignment of precast parapets; and reflective cracking, grading problems, and inability to obtain skews greater than 15° with prestressed subdeck panels. Obviously, the majority of those responding to the questionnaire believe that with the exception of high first cost there are few continuing problems with the use of most prefabricated elements. The problem of high cost can be minimized by specifying larger quantities of the elements, eliminating design details that are difficult to fabricate, and taking into account benefits, such as the savings to the motorist of reduced lane closure time and off-peak traffic construction.

TABLE 4

CONTINUING PROBLEMS

		Re	plies I	ndicat	ing P	roblen	n
	Replies	First Cost	None	Length and Weight	Deterioration and Corrosion	Supply	Keyways and Connections
Precast concrete slab span	20	10	4	2	3	2	1
Precast box beam	19	9	4	2	3	2	. 0
Prestressed I-beam	23	10	8	4	0	2	0
Precast deck panel	5	2	1	1	0	0	0
Permanent bridge-deck form	13	5	5	0	0	1	• 0
Precast parapet	6	1	1	0	1	0	5
Double-tee and channel	5	2	2	0	1	0	0

Some specific deficiencies noted in the literature are as follows. A number of states have reported problems with the placement and the long-term stability of epoxy mortar shear keys between standard PCI box beams (11). A deficiency with the double-tee is that the slab thickness is insufficient to adequately anchor typical bridge railings (11). The New York Thruway Authority has reported minor problems with the use of precast concrete deck panels, including hairline cracks in the slabs, difficulties in placing the epoxy mortar bedding between the top of stringers and the bottom of the slabs, and excessive cure times for epoxy mortar placed in cold weather (2). It is anticipated that improvements in quality control will likely minimize the number of cracks, the installation of neoprene strips to retain the epoxy bedding will eliminate the bedding difficulties, and the use of cold weather polymeric materials will permit installation in cold

weather (2). A recent study in Virginia indicates that the concrete used in precast elements (with accelerated curing) is typically more permeable to chloride ions than the CIP concrete used in bridge decks (69). Problems that could result from the higher permeability can be minimized by applying the technology for curtailing the corrosion of the reinforcement and the deterioration of the concrete caused by freezing and thawing, which is well established for bridge decks (70). Alternative protective systems, such as epoxy-coated reinforcement, one of a number of waterproofing membranes or sealers of epoxy or polymer materials, and dense concrete overlays such as latexmodified concrete, can be used to extend the service life of the prefabricated elements (69-72). The value of sealers, membranes, and epoxy-coated reinforcement in extending the life of precast concrete elements should be studied.

CHAPTER FOUR

CONSTRUCTION AND MAINTENANCE

The principal advantage of using prefabricated bridge elements and systems is to achieve a reduction in the number of work days at the bridge site. With a reduction in on-site construction time there is less inconvenience to the motorist, the appearance and condition of the bridge site is restored in a short. time, fuel is conserved because there are fewer delays for the motorist and fewer work trips to the bridge site, and working conditions are improved because most of the construction takes place in the convenience and safety of a fabricating plant (4, 10, 25, 37).

Another reason for using prefabricated elements is to improve design and construction efficiency. For economy, prefabricated elements should be mass produced. Mass production requires that many elements have the same design. Sufficient quantity can be obtained by either specifying an element for a long multispan bridge or by specifying an element for many short bridges. Design costs are less when the same element is specified for many spans because one design may replace a number of individual designs. Also, forming costs are less because the same forms can be used to produce elements for many spans.

In addition, construction is more efficient when prefabricated elements are specified because fabrication can proceed in an established, repetitive, and systematic manner; fabrication can proceed in bad weather; the number of man-hours lost in traveling to and from a bridge site is reduced; concrete is sometimes cheaper, because it does not have to be hauled a long distance; and high-quality concrete is more easily obtained in a fabricating plant than at a bridge site because the plant provides for repetitive process and environmental control (13, 37). The principal disadvantages in using prefabricated bridge elements are in handling the large units and making sure they fit properly.

FABRICATION OF ELEMENTS

Quality control and efficiency at the fabrication plant are probably the most essential ingredients for the successful construction of a structure containing prefabricated elements. Prefabricated elements will fit together satisfactorily in the field if they are fabricated with the tolerance prescribed by the Prestressed Concrete Institute (73, 74). The allowable tolerances must be obtainable with economical precasting methods; sometimes the use of CIP concrete is more practical than precasting to a close tolerance (13, 68). Because the major portion of the construction of a bridge containing prefabricated elements takes place in the factory, the major portion of the supervision and inspection must take place there. Fabrication errors that are not detected at the plant can be very costly and time-consuming to remedy in the field. Prefabricated elements that are cast in a good set of forms and under close supervision will fit together quickly and securely in the field.

Based on results of the questionnaire, the elements are usually fabricated by a precast concrete producer (with the exception of the steel stay-in-place forms, which are fabricated by a steel fabricator). Only 24% of the replies indicated that the slab spans are occasionally fabricated by a contractor. Only 12 and 4% of the replies, respectively, noted that the slab spans and box beams were occasionally fabricated by state and local crews. Elements are usually fabricated by state and local crews during off-peak maintenance periods when there is a surplus of manpower (37, 62)

FORMS

Based on the questionnaire, the elements (with the exception of the precast deck panels on steel stringers) are usually fabricated in forms and casting beds that are versatile and suited to producing members for many projects (multiple-project forms). Sixty-seven percent of the replies indicated the deck panels are fabricated in special forms, but only 23% or less of the replies indicated the other elements were fabricated in special forms. Thirty-eight percent of the replies indicated the prestressed concrete subdeck panels are fabricated in more versatile forms that are suited for producing elements for use in construction other than bridges (multi-purpose forms). Fewer replies noted the multi-purpose forms were used to fabricate the other elements.

For economy it is desirable to use multiple-project forms but it is usually not possible to use multi-purpose forms for most members because the sections required for bridge construction are usually heavier than those required for other types of construction (4). Forms can be designed to provide members for many bridge projects by specifying the same section for many projects, which was typical when the I-beam, parapet, subdeck panel, and double-tee and channel were specified, and less typical when the slab span and box beam were specified. Forms that provide for some adjustment in either width or depth can be made without much added expense to allow the precasting of slab spans and box beams with slightly different sections. Also, most forms are suited to providing elements of various lengths.

HANDLING AND STORAGE OF ELEMENTS

Precasting operations should be organized to minimize the number of times an element must be moved (75). Excessive handling is not only costly and time-consuming but increases the chances for damaging an element. It is desirable to move elements from the casting bed as soon as strength requirements are satisfied so that new elements may be cast. Elements that cannot be hauled to the field when removed from the form should be stored in such a manner that they will not have to be moved again until they are needed in the field.

The hardware, rigging, and equipment required for satisfactory handling of elements are dictated by the size and weight of the units and the handling requirements. Care should be taken in the selection of lifting hardware and the location of lifting points to minimize handling stresses.

Elements should be stored to induce the same dead load stresses that will be encountered in the field. Elements such as slabs may be stored on top of each other to save space, and timber spacers may be placed between them directly above the timbers that support the bottom slab.

LOCATION OF PLANTS

Based on replies to the questionnaire, the plants at which the elements were fabricated were usually located between 1 and

200 miles (1.6 and 320 km) from the bridge site. Fifty percent of the replies indicated the double-tee and channel were transported more than 200 miles and a lower percentage of the replies indicated the other elements were transported more than 200 miles. Only 13% of the replies indicated the slab span and the double-tee or channel were transported less than one mile and fewer replies indicated the other elements were transported less than one mile. The response suggests that the members are usually fabricated at a permanent plant and only occasionally fabricated at a temporary plant next to the bridge. A temporary plant should be economical for precasting elements for bridges with many spans.

TRANSPORTATION OF ELEMENTS

The elements are almost always transported to the site by commercial truck. Ninety-five percent or more of the replies indicated a truck was used to transport the members. Fourteen percent of the replies indicated that the I-beam was transported by rail and 17% of the replies indicated that the deck panels were transported by barge. A lower percentage of the responses indicated that the other elements were transported by rail or barge.

The recommended practice for transporting the elements to the bridge site is to load them so that they are properly balanced on the trailer and are supported during transportation as they were during storage. Also, elements should be properly braced and secured so that the flexure of the trailer bed is not transferred to them, and trailer movements will not cause them to shift (75). Small pieces of timber make excellent pads for distributing the forces from the chains that secure the elements to the trailer.

Elements should be transported to the bridge site in the order in which they are to be placed, and deliveries should be scheduled so that they can be placed as soon as possible after they arrive (75). Proper communication between the fabricator and erector is essential.

The number of elements that can be transported on a trailer is usually controlled by the weight of the elements but size can also be a factor. The roadway clearance and the capacity of structures between the bridge site and the casting yard will occasionally dictate the number of elements that can be hauled in one trip. For some bridges, the weight of the elements will be such that the use of lightweight concrete or voided material will allow one more element to be transported on each trip than if solid elements of normal-weight concrete were fabricated. Requirements may vary from state to state, and therefore the weight, length, depth, and width of the element and the need for a special permit must be considered when designing and fabricating an element (76).

ERECTION AND CONNECTION OF ELEMENTS

Eighty-eight to 100% (depending upon the element) of the replies to the questionnaire indicated the elements are usually installed by a contractor. However, 50% of the replies indicated that the double-tee and channel are erected by the precast concrete producer and 38% indicated that these elements are erected by state and local crews. Other elements sometimes erected by producers or state and local crews are the slab spans

and box beams. Evidently, it is acceptable practice to purchase the members as delivered or as installed.

Personnel and equipment should be ready at the bridge site when the elements arrive. Lifting equipment should be secured in appropriate, predetermined locations. When possible, lifting equipment should be located so that it will not interfere with traffic and will have to be moved as few times as possible. At times a considerable amount of time and effort will be required to get the lifting equipment to the site and to the most appropriate location. When lifting equipment is to be placed on a structure, the design should be checked to ensure that the structure will not be overloaded.

The lifting equipment should be large enough to handle the elements and it is better to have equipment that is too large than equipment that is too small. The boom distance, weight of the crane, weight of the elements, and crane cost should be taken into account when selecting a crane for a particular job.

Bearing areas should be properly prepared before the elements arrive. Once an element is placed, it is examined for fit. If acceptable bearing is not obtained when the element is placed, corrective measures must be taken. Neoprene bearing pads are usually adequate for providing acceptable bearing below large elements such as the I-beam. A variety of combinations of grouts and mortars of portland cement concrete, epoxy, and polymer concrete have also been used to obtain acceptable bearing for prefabricated elements. Usually temporary wooden shims or other devices must be used to support the element until the leveling mortar or grout has adequate strength. Elements that are fabricated accurately will fit together in the field easily and quickly and elements that do not bear properly will require additional time and attention. The best procedure is to try to achieve a properly prepared supporting surface and an accurately fabricated element and to be ready at the site to apply some suitable corrective measure. Typically, elements can be lifted from a trailer and put into place and connected in a few minutes. On-site construction time is primarily a function of the time required to apply the necessary corrective measures for poor fitting elements and to otherwise connect the element into the structure (6). The development of high-early-strength epoxy and polymer mortars has minimized the time and problems associated with providing suitable bearing and connection between prefabricated elements.

TABLE 5

MAINTENANCE OF PREFABRICATED ELEMENTS

		Maintenance Require (No. of agencies)						
Element	Replies	None or Routine	Patching	Overlays	Joints	Connections	Other	
Precast concrete slab span	20	8	5	3	3	1	4	
Precast box beam	21	13	- 3	2	1	1	5	
Prestressed I-beam	28	20	4	1	2	0	6 -	
Precast deck panel	5	3	1	1	0	0	0	
Permanent bridge-deck form	15	12	2	1	0	0	1	
Precast parapet	5	4	0	0	0	1	0	
Double-tee and channel	8	7	1	0	1	0	1	

MAINTENANCE

Depending on the element, 83 to 100% of the replies to the questionnaire indicated that state or local forces maintain the bridges and 17 to 33% of the replies indicated maintenance is performed under contract.

Table 5 shows the replies to the questionnaire that noted that the indicated type of maintenance was performed on bridges containing the indicated element. It is apparent from the replies shown in Table 5 that bridges containing the elements are relatively maintenance free; the majority of the replies indicated that no maintenance or only routine maintenance is required. Only 25% or less of the replies, depending on the element, indicated that a particular type of maintenance was required. The most frequently cited types of maintenance were patching and maintenance of overlays and joints. Although connections are sometimes cited in the literature as a problem with prefabricated elements (7, 11), the response to the questionnaire did not support this conclusion.

COSTS AND BENEFITS OF PREFABRICATED ELEMENTS AND SYSTEMS

CONSTRUCTION COSTS

In the responses to the questionnaire, reduced first cost was one of two principal reasons cited for the use of prefabricated elements and systems. Table 6 shows the average first cost based on the replies to questions that asked for the first cost in dollars per ft² of deck surface for the elements and the most frequently used alternative.

The most frequently used alternative to the box beam, I-beam, and double-tee and channel is steel beams with CIP concrete deck and, on average, the prefabricated elements cost less than the alternative. A CIP concrete superstructure costs slightly less than the box beam and I-beam and more than the double-tee and channel, but is not frequently used as an alternative evidently because it requires a larger section for the same span or because more spans are required, and consequently substructure costs are greater. A precast slab span typically costs less than a CIP slab and slightly more than steel beams and CIP concrete deck. Also, one reply indicated that a culvert costs less than a bridge with precast slabs. A CIP concrete deck on steel beams costs less than precast deck panels on steel beams, a CIP parapet costs about the same as a precast parapet, and the formwork for a CIP concrete deck costs slightly more than the cost of permanent bridge-deck forms.

Other values for first cost that were found in the literature are shown in Table 7. It is obvious from Tables 6 and 7 that the alternatives to the prefabricated elements are not necessarily cheaper or more expensive. Because of the many factors that affect first cost, either the prefabricated element or the alternative can have the lower first cost in a given situation.

Factors that affect cost include availability of one material relative to another, availability of forms and equipment for fabricating and handling one type of element relative to those for another, the qualifications and experience of the available labor force, and the characteristics desired in the finished bridge. In general, a bridge that utilizes elements that are a stock item, or can be cast in forms that are readily available and can be constructed with locally available labor, equipment, and expertise, will almost always have a lower first cost than a bridge that requires nonstandard elements, the purchase of special forms or equipment, and the use of specialized labor. Because the decision to use a prefabricated element is usually based on first cost, it is necessary to develop cost estimates for each site condition to ensure that the most economical alternative is selected; the values shown in Tables 6 and 7 are for illustrative purposes only.

Quantity can have a significant effect on cost. A precast concrete producer must foresee future demand for a prefabricated element or else will most certainly include the cost of forms in the bid for the first bridge that is advertised (10, 78). Consequently, the cost of the first bridge can far exceed the cost of a conventional alternative. For example, a research project by the Texas Department of Highways and Transportation developed five precast superstructure types, and arranged for the advertisement of two of them (box beam and double-tee) as alternative superstructures to a standard CIP concrete superstructure (11). The study concluded that the alternative superstructures with the prefabricated elements were not competitive with the standard CIP concrete superstructure because the precast producers were not willing to invest in new forms for only one job (11). It is likely that some transportation departments believed that prefabricated elements are more expensive than conventional bridges because they have had a similar experience. Clearly, when determining the cost of bridges with prefabricated elements that have not been previously used, the cost of the forms should be separated from the other costs so that a fair assessment of the costs of the new elements can be made. To minimize the cost of the forms for each bridge, the transportation departments should advertise a sufficient number of bridge spans with the same prefabricated element.

Other ways to minimize the cost of prefabricated elements are as follows. Use welded wire fabric rather than reinforcing bars (11). Work with local producers throughout the planning

TABLE 6

			Alternatives					
	Prefabr Elem	Prefabricated Elements		orete	Steel E CIP E	Beam/ Deck		
Element	Replies	Cost	Replies	Cost	Replies	Cost		
Precast concrete slab span	13	26.11	5	28.69	5	25.02		
Precast box beam	13	25.64	2	21.77	10	29.61		
Prestressed I-beam	18	21.11	3	20.87	14	24.87		
Precast deck panel	3	19.34	4	17.89	· _	-		
Permanent bridge-deck form	4	3.00	5	3.50	-	-		
Precast parapet	3	2.67	4	2.54	-	-		
Double-tee and channel	4	19.30	1	24.81	2	27.27		

INSTALLED FIRST COST OF ELEMENTS AND ALTERNATIVES^a

 a^{1}/ft^{2} of deck surface; based on 1984 survey.

stage, advertise a large number of identical spans, avoid diaphragms and other projections from the elements, avoid skews (limit the skew to 30° or less), avoid special details, minimize the quantity of reinforcing steel, and specify elastomeric bearing pads (4).

MAINTENANCE COSTS

Those responding to the questionnaire seldom provided estimates for life-cycle cost and maintenance cost and the few replies that were received seemed to indicate that maintenance costs were negligible for properly constructed structures, whether prefabricated or not, and therefore the life-cycle costs were the same as the first costs. The response from the Minnesota DOT indicated the life-cycle cost was 20% greater than the first cost for a concrete deck on steel beams and 5% greater for concrete deck on prestressed I-beams. Evidently 5% is for routine maintenance and 15% is for repainting the steel beams (4). Based on the response to the questionnaire, life-cycle costs and maintenance costs are not a factor in the selection of alternatives and all alternatives are considered to have a long life with near zero maintenance despite the fact that some maintenance, as cited in Chapter 4, is required for bridges containing all types of elements. Alexander (79) warns that it is possible to spend more on first cost than will ever be recovered in reduced maintenance costs. Bridges on low-volume roads should be designed to minimize first cost rather than maintenance cost, and bridges on high-volume roads should be designed to minimize maintenance so that it does not interfere with traffic. Clearly research should be directed at the development of estimates for maintenance cost and service life for all types of bridges, and bridge engineers should choose between alternatives based on life-cycle costs rather than first costs.

REDUCED CONSTRUCTION TIME

In the response to the questionnaire, a principal reason cited for the use of prefabricated elements and systems was to accelerate construction. However, almost no quantitative response was made to the question, "What is the lane closure time per square foot of deck surface for the installation of the elements and the alternatives?" Evidently, because of the many factors that affect construction time, it is difficult to provide estimates that would be applicable to the general case, but it should be possible to develop estimates for specific site conditions. Obviously there is strong feeling by the users of the prefabricated elements and systems that on-site construction time is less, but it would be helpful to direct research at the development of estimates. The information should be helpful when considering the use of alternative elements in the construction and replacement of bridges.

The response from the Kentucky DOT indicated that bridges with the precast slab spans, box beams, and I-beams could be constructed with 17% of the lane closure time required for bridges requiring CIP concrete. The Minnesota DOT noted that bridges with precast slab spans could be constructed with half the lane closure time required for bridges with CIP concrete decks. The New York DOT noted that less lane closure time was required for bridges with precast slab spans and box beams. The Wyoming DOT indicated that the same time was required for all bridges because a CIP substructure was used with all bridges. Alberta indicated a culvert bridge could be opened to traffic in 60% of the time required for a bridge with precast slab spans because a CIP substructure was required to support the slabs. The replies to the questionnaire somewhat support the theory that lane closure time can be reduced through the use of prefabricated elements.

Additional evidence is provided by the case studies of on-site construction time that were noted from the literature. For example, in Virginia state forces were able to install a precast slab span superstructure in 13% of the on-site time required for a CIP concrete superstructure and 24% of the on-site time required for a superstructure of steel stringers and timber plank deck (6). Similarly, it was estimated that in Virginia, a concrete deck on steel beams could be replaced with precast concrete deck panels in 21% of the on-site time required for a CIP concrete deck (24). Similarly, Berger (25) estimates that precast concrete for CIP concrete. Use of the prestressed subdeck panels on a new four-span prestressed concrete I-beam bridge in Indiana allowed the contractor to complete the job six weeks ahead of schedule (28).

On-site construction time and cost, the two principal reasons prefabricated elements are used, are somewhat interdependent. Construction can be accelerated by providing a cost incentive for rapid construction and a penalty for delays in situations where the contractor would otherwise not benefit economically by accelerating construction. For example, a small contractor, in particular, might have a considerable increase in overhead cost to accelerate construction because more investment in manpower and equipment would likely be required. Unless daily operating costs for items such as traffic control are adequate incentive to promote accelerated construction, it is likely that an incentive in the form of a bonus or penalty will be required to achieve a more rapid rate of construction.

An incentive of \$5,000 per day, up to a maximum of 100 calendar days, was offered for early completion of the renovation of the Third Avenue Bridge over the Mississippi River and the work was completed almost one year ahead of schedule (80). Similarly, the contract for the rehabilitation of the deck of the Woodrow Wilson Bridge contained a clause that provided a bonus for each day the deck work was completed ahead of schedule (17, 23, 27). A number of DOTs have used incentives to accelerate repairs (81, 82).

VALUE TO TRAVELING PUBLIC

The traveling public is inconvenienced by almost any lane closure. The magnitude of the inconvenience is a function of the volume of traffic and the traffic capacity of the bridge being restricted, or the location of an alternative route and the volume of traffic and capacity of the alternative route (22). The higher the volume-to-capacity ratio, the greater the chance a motorist will be delayed. For example, an increase in the volume-to-capacity ratio from 0.5 to 1.0 can cause a decrease in the average speed of the motorist from 53 mph to 32 mph (85 to 51 km/h) (83). This could occur if one of two lanes of a bridge is closed or if one of two bridges is closed for construction and repair. The motorist can also be delayed if forced to take an

TABLE 7

Element or alternative	Item Used for Cost Estimate and Source							
	Element (<u>10</u>)	Super- structure (<u>9</u>)	Element (<u>11</u>)	Super- structure (77)	Deck (<u>24</u>)	Deck (<u>25</u>)		
Precast concrete slab span	-	9.39	-	-	-			
Precast box beam	7.12	-	16.33	7.35	-	-		
Prestressed I-beam	5.37	-	-	6.87	-	-		
Precast deck panel	-	-	-	-	11.01	13.97		
Permanent bridge-deck form	3.14	-	-	-	-	-		
Precast parapet	2.42	-	-	-	-	-		
Double-tee and channel	7.89	-	15.58	-	-	-		
Single-tee	8.78	-	-	6.41	-	-		
Cast-in-place deck	-	13.30	11.71	-	10.03	15.90		
Steel beam with CIP deck	-	-	-	9.15	-	-		

LITERATURE SURVEY OF INSTALLED FIRST COST OF PREFABRICATED ELEMENTS AND ALTERNATIVES^a

 a^{1}/ft^{2} of deck surface.

alternative route that is longer. Obviously, if travel time is assigned a dollar value, the use of prefabricated elements that reduce lane closure time would result in savings to the traveling public.

As an example of the magnitude of the dollar value to the traveling public, consider the replacement of a concrete deck with precast concrete deck panels as compared to CIP concrete. Assuming a lane closure during the day causes an average decrease in speed of 21 mph (34 km/h) over a 10-mile (16-km) segment of roadway, an average wage rate of \$1 per hour per vehicle, and a traffic volume of 1,300 vehicles per hour, the cost of the reduction in speed is \$161 per hour. The precast panels can be installed at night and opened to traffic in the day; therefore, the cost of the lane closure is negligible because it occurs when the traffic-to-capacity ratio is low. On the other hand the use of CIP concrete requires forming, rebar installation, concrete placement, and curing of the concrete to obtain sufficient strength. Even with the use of high-early-strength concrete mixtures, it is unlikely the lane could be opened to traffic in one day. If it is assumed that the delays associated with the lane closure last for 8 hours each day and 10 days are required to replace a deck 40 by 350 ft (12 imes 107 m), the cost to the motorist is \$12,880 or \$0.92/ft² (\$10/m²) of deck surface. An increase in the average wage rate to \$3 per hour per vehicle increases the cost to $\frac{2.76}{ft^2}$ ($\frac{30}{m^2}$).

The cost to the motorist would increase with increases in the number of days of lane closure, the volume of traffic, and the dollar value placed on driving time. Only a few examples of the dollar value to the traveling public of reduced lane closure time could be found in the literature (72, 80, 84). Research should be directed at quantifying the value to the traveling public of reduced lane closure time that results from the use of prefabricated elements and systems.

In many situations a lane closure during peak-hour traffic periods is out of the question because of the reduction in level of service owing to the inconvenience to the traveling public that would result. For example, in the replacement of the deck of the Woodrow Wilson Bridge, a lane closure during peakhour traffic periods would require the motorist to choose between a major reduction in travel speed across the bridge or driving an extra 13 miles (21 km) or more over an alternative route that did not have the capacity to carry additional vehicles (17, 27). Most public agencies plan repairs to avoid this reduction in level of service to the public. A temporary bridge or ferry service would have been economically unfeasible. The deck replacement had to be done in stages that were restricted to the duration of the off-peak traffic period. The replacement of the deck of the Woodrow Wilson Bridge illustrates one of the principal benefits to be obtained from the use of prefabricated elements-the ability to construct or replace in stages. Most prefabricated elements (slab spans, box beams, deck panels, parapets, etc.) are suited for stage construction or construction during off-peak traffic periods. Research should be conducted to quantify the value to the traveling public of the stage construction that can be accomplished with prefabricated elements and systems.

CHAPTER SIX

CONCLUSIONS AND RECOMMENDATIONS

CONCLUSIONS

Approximately 15% of the bridges in the United States and Alberta contain prefabricated elements and systems. The most frequently used elements are the prestressed concrete I-beam, precast and prestressed box beam, precast and prestressed and channel, and precast slab span. In recent years, steel stay-inplace forms, prestressed concrete subdeck panels, and the precast parapet have been used on a large number of bridges, and the decks of a small number of bridges with steel stringers have been replaced with precast deck panels.

The use of prefabricated elements has increased over the years and this trend is likely to continue. The elements are used on all types of roadways but the slab span and box beam are used most frequently on low-volume roads. The elements are used in new construction and in bridge replacement. The primary reasons the elements are used is to reduce first cost and to accelerate construction.

The elements are usually fabricated in forms that are suited for producing elements for many bridge spans. The elements are usually fabricated by a precast concrete producer and the precast plant is usually located within 200 miles (320 km) of the bridge site. The elements are usually transported by commercial truck and erected by a contractor. Sometimes the precast slab spans, and occasionally the other elements, are fabricated by a contractor or erected by the precast concrete producer. Also, state and local crews will occasionally fabricate and erect the elements, particularly the precast slab spans and box beams. Bridges containing the elements have required very little maintenance and that which was needed was usually done by state and local forces. The use of overlays, waterproof membranes, and sealers may have contributed to the low maintenance cost.

The cost of bridges containing the elements is usually not significantly different from the cost of alternative types of bridges and can be a function of local supply and demand.

On-site construction time can be significantly less for bridges

containing the elements. Precast slab spans and box beam superstructures can be constructed in approximately 20% of the time required for CIP concrete superstructures. On-site construction time can be significantly affected by the procedures and decisions of the contractor and therefore a cost incentive may be needed to reduce on-site construction time.

Early problems with the use of prefabricated elements were usually caused by a lack of quality control and experience and have been largely eliminated. The most significant continuing problem is high first cost in some locations. The cost is usually a function of local supply and demand. By placing a dollar value on driving time, a higher cost can be justified on bridges subjected to high volumes of traffic because of the reduced lane closure time that can be achieved with prefabricated elements and because the prefabricated elements allow for stage construction and can be installed during off-peak traffic periods.

RECOMMENDATIONS

Special attention should be directed toward the resolution of the continuing problems cited in Chapter 3. Use of prefabricated elements and systems should be continued when cost savings can be achieved. The potential of prefabricated substructure elements should be developed. Research should be directed at the development of cost estimates for the value of the reduced lane closure time that can be achieved and the value of off-peak traffic period stage construction that can be accomplished when bridges are rehabilitated with prefabricated elements. Also, estimates for service life, first cost, and maintenance cost should be developed and bridge engineers should base decisions on the use of the elements on life-cycle costs, the value of lane closure time, and the value of the stage construction that can be accomplished. The role of sealers and epoxy-coated reinforcement in extending the life of prefabricated concrete elements should be evaluated.

REFERENCES

- Virginia Highway and Transportation Research Council, NCHRP Report 222: Bridges on Secondary Highways and Local Roads Rehabilitation and Replacement, Transportation Research Board, National Research Council, Washington, D. C. (May 1980) pp. 74-111.
- Virginia Highway and Transportation Research Council, NCHRP Report 243: Rehabilitation and Replacement of Bridges on Secondary Highways and Local Roads, Transportation Research Board, National Research Council, Washington, D. C. (Dec. 1981) pp. 7-12, 36-46.
- FHWA, "Highway Bridge Replacement and Rehabilitation Program, Fifth Annual Report to Congress," Federal Highway Administration, Washington, D.C. (May 1984) pp. 43-44.
- 4. Prestressed Concrete Institute, "Short Span Bridges," Chicago, Illinois (1975).
- FHWA, "Standard Plans for Highway Bridges—Vol. 1, Concrete Superstructures," Federal Highway Administration, Washington, D. C. (Aug. 1968).
- Sprinkel, M. M., "In-house Fabrication of Precast Concrete Bridge Slabs," *VHTRC 77-R33*, Virginia Highway & Transportation Research Council, Charlottesville, Virginia (Dec. 1976) pp. 1, 3, 9, 11.
- Martin, L. D. and A. E. N. Osborn, "Connections for Modular Precast Concrete Bridge Decks," FHWA/RD-82/106 (Aug. 1983) pp. 2, 33-58.
- "County Highway Department Casts Its Own Prestressed Bridge Beams," Public Works (June 1975) pp. 84-85.
- Sprinkel, M. M. and W. H. Alcoke, "Systems Bridge Construction in Virginia," *American Transportation Builder* (June 1977) pp. 11-13.
- Virginia Prestressed Concrete Association, "New Approaches in Prestressed, Precast Concrete for Bridge Superstructure Construction in Virginia" (Aug. 1973) pp. 4, 6, 10, 14, 17, 19, 25.
- Panak, J. J., "Economical Precast Concrete Bridges," Texas State Department of Highways & Public Transportation, Research Report 226-1F (March 1982) pp. 1, 12-18, 27-32.
- Anderson, A. R., "Systems Concepts for Precast and Prestressed Concrete Bridge Construction," *HRB Special Report 132: Systems Building for Bridges*, Highway Research Board, National Research Council, Washington, D.C. (1972) pp. 9-14.
- TRB, NCHRP Synthesis 53: Precast Concrete Elements for Transportation Facilities, Transportation Research Board, National Research Council, Washington, D. C. (1978) 48 pp.
- 14. "State of the Art: Permanent Bridge Deck Forms," Transportation Research Board Circular 181, Transportation Re-

search Board, National Research Council, Washington, D. C. (Sept. 1976) pp. 1-18.

- 15. "RTP Markets Instant Bridges," Concrete Products (Feb. 1968) pp. 48-51.
- "Modern Concepts in Prestressed Concrete Bridge Design," PCI Bridge Bulletin, Second Quarter (1972).
- "Concrete Today: Markets, Materials and Methods," Engineering News Record, Special Advertising Section (May 17, 1984) pp. 6, 8, 19, 20.
- Rabbat, B. G., T. Takayanagi, and H. G. Russell, "Optimized Sections for Major Prestressed Concrete Bridge Girders," U. S. Department of Transportation, Federal Highway Administration, Report No. FHWA/RD-82/005, Washington, D. C. (Feb. 1982) 178 pp.
- U. S. Steel Corporation, "Short Span Steel Bridges" (Sept. 1973) p. 128.
- Biswas, M., J. S. B. Iffland, R. E. Schofield, and A. E. Gregory, "Bridge Replacements with Precast Concrete Panels," *Special Report 148: Innovations in Construction and Maintenance of Transportation Facilities*, Transportation Research Board, National Research Council, Washington, D. C. (1974) pp. 136-148.
- 21. "Low-Cost No-Care Bridge," Better Roads (Feb. 1971) p. 11.
- TRB, NCHRP Synthesis of Highway Practice 25: Reconditioning High-Volume Freeways in Urban Areas, Transportation Research Board, National Research Council, Washington, D. C. (1974) 58 pp.
- Lutz, J. G. and D. J. Scalia, "Deck Widening and Replacement of Woodrow Wilson Memorial Bridge," *Journal of Prestressed Concrete Institute*, Vol. 29, No. 3 (May-June 1984) pp. 74-93.
- Sprinkel, M. M., "Precast Concrete Replacement Slabs for Bridge Decks," Virginia Highway & Transportation Research Council, VHTRC 83-R2 (July 1982) pp. 2-4, 13.
- Berger, R. H., "Full-Depth Modular Precast, Prestressed Bridge Decks," *Transportation Research Record 903:* Bridges and Culverts, Transportation Research Board, National Research Council, Washington, D. C. (1983) pp. 52-59.
- Smyers, W. L., "Rehabilitation of the Fremont Street Bridge," *PCI Journal*, Vol. 29, No. 5 (Sept.-Oct. 1984) pp. 34-51.
- "Woodrow Wilson Memorial Bridge, Washington, D. C.: Concrete Deck Reconstruction." TRNews, No. 111 (March-April 1984) pp. 2-7.
- Kelly, J. B., "Applications of Stay-in-Place Prestressed Bridge Deck Panels," *PCI Journal*, Vol. 24, No. 6 (Nov.– Dec. 1979) pp. 20–26.
- 29. Barker, J. M., "Research, Application and Experience with
Precast, Prestressed Bridge Deck Panels," PCI Journal, Vol. 20, No. 6 (Nov.-Dec. 1975) pp. 66-85.

- PCI Bridge Committee, "Tentative Design and Construction Specifications for Bridge Deck Panels," *PCI Journal*, Vol. 23, No. 1 (Jan.-Feb. 1978) pp. 32-39.
- 31. Hilton, M. H., "A Field Installation Using Prestressed Panel Subdecks," Virginia Highway & Transportation Research Council (Dec. 1978).
- Fagundo, F. E., C. O. Hays, Jr., and J. M. Richardson, "Study of Composite Deck Bridges in Florida," Final Report U69F, University of Florida, Gainesville, Florida (July 1983) pp. 1-9, 138-144.
- 33. Hays, C. O., Jr., F. E. Fagundo, and E. C. Callis, "Study of Cracking of Composite Deck Bridge on I-75 over Peace River." *Transportation Research Record 903: Bridges and Culverts*, Transportation Research Board, National Research Council, Washington, D. C. (1983) pp. 35-44.
- Thunman, C. E., Jr., "Precast Prestressed Concrete Deck Planks," Memorandum to District Bridge Engineers, Illinois Department of Transportation (June 1, 1984) 2 pp.
- 35. "Bridgform," Buffalo Specialty Products, Inc., Bethlehem, Pennsylvania (May 1984) 8 pp.
- Hilton, M. H., "An Experience Survey on the Use of Permanent Steel Bridge Deck Forms," Virginia Highway & Transportation Research Council (Oct. 1975).
- Sprinkel, M. M., "Systems Construction Techniques for Short Span Concrete Bridges," *Transportation Research Record 665: Bridge Engineering, Vol. 2,* Transportation Research Board, National Research Council, Washington, D. C. (1978) pp. 226-227.
- 38. Virginia Department of Highways and Transportation, "Precast Concrete Parapet Details," Richmond, Virginia (1974).
- Tokerud, R., "Economical Structures for Low-Volume Roads," Transportation Research Board Special Report 160: Low-Volume Roads, Transportation Research Board, National Research Council, Washington, D. C. (1975) pp. 273– 277.
- McDonald, J. E. and T. C. Liu, "Precast Concrete Elements for Structures in Selected Theaters of Operations," U. S. Army Waterways Experiment Station Technical Report C-78-1, Vicksburg, Mississippi (Feb. 1978) pp. 15-24.
- 41. Mississippi State Highway Department, "Standard Plans for Precast Posttensioned Channel Bridge Spans," Jackson, Mississippi (June 1969).
- 42. Prestressed Concrete of Colorado, Stanley Structures, LTD, "Plans for Tee-Beam Bridges" (1969).
- Elsasser, H. B., "Current Practices in Steel Construction," *HRB Special Report 132: Systems Building for Bridges,* Highway Research Board, National Research Council, Washington, D. C. (1972) pp. 31, 32.
- Zuk, W., "Kinetic Bridges," Virginia Highway & Transportation Research Council, VHTRC 81-R6, Charlottesville, Virginia (July 1980) pp. 2-33.
- 45. "Bridge Redecked in Less Than 150 Days," Highway and Heavy Construction, Vol. 127, No. 8 (Aug. 1984) p. 70.
- 46. "Pittsburgh's Troubled Bridges: What To Do About Them?," Civil Engineering (Jan. 1978) pp. 46-51.
- "Design Aid for Orthotropic Bridge Decks Using Bethlehem Standard Ribs," Bethlehem Steel Corporation, Bethlehem, Pennsylvania (May 1968).

- "George Washington Bridge Deck Replacement," Public Works (May 1974) p. 60.
- 49. "Bridge Gets Prepared Deck Overnight," *Engineering News* Record (Nov. 10, 1977) p. 24.
- 50. "George Washington Bridge Redecked with Prefabricated Panels and No Traffic Delay," *Civil Engineering* (Dec. 1977).
- 51. American Institute of Timber Construction, "Glulam Bridge Systems—Plans and Details" (1975).
- Sprinkel, M. M., "Glulam Timber Deck Bridges," Virginia Highway and Transportation Research Council, Charlottesville, Virginia (Nov. 1978) pp. 28.
- 53. Bruesch, L. D., "Timber Bridge Systems," FCP Conference, Atlanta, Georgia (Oct. 3-9, 1977).
- 54. "Weyerhaeuser Glulam Wood Bridge Systems," Weyerhaeuser Company, Western Wood Structures, Inc., Beaverton, Ohio (1980) pp. 8, 12, 13.
- 55. "Modern Timber Highway Bridges a State-of-the-Art Report," American Institute of Timber Construction (July 1, 1973) pp. 1, 43, 62.
- Hale, C. Y., "Field Test of a 40-ft. Span Two-Lane Weyerhaeuser Panelized Wood Bridge," Weyerhaeuser Company (May 1975).
- 57. Virginia Department of Highways and Transportation, "Plans for Glulam Bridge over Pohick Creek, Fairfax County, Virginia," Richmond, Virginia (1975).
- Virginia Department of Highways and Transportation, "Standard Plans Steel Beams with Glulam Flooring," Richmond, Virginia (July 1976).
- U. S. Steel Corporation, "Bridge Structural Report—Nine Steel Bridges for Forest Development Roads South Tonguss National Forest Alaska" (June 1973).
- 60. Thompson, P., "County's Precast Bridges Aid Roads and Wheat Markets," Rural and Urban Roads (Sept. 1976).
- Imel, K. D., "The Bridge Program for Rural Oklahoma," FCP Conference, Atlanta, Georgia (Oct. 3-6, 1977).
- Willis, S. K. and W. R. Sachse, "Standard Bridges Save County Dollars," *Better Roads* (Jan. 1973) pp. 16–19.
- 63. Lambert, A. V., "Instant Arches-European Style," Concrete International (Jan. 1982) pp. 44-47.
- 64. "Bebo Precast Concrete Arches Built to Last," Hancock Concrete Products, Hancock, Minnesota, pp. 1-4.
- Hanson, T. A. & Associates, "Systems Bridges Phase Two: Substructure," Feasibility Study for Virginia Highway and Transportation Research Council, Charlottesville, Virginia (May 1, 1972).
- GangaRao, H. V. S., "Conceptual Substructure Systems for Short-Span Bridges," *Transportation Engineering Journal*, ASCE, New York, N. Y. (Jan. 1978).
- Wigginton, W. B., "Systems Building: Foundations," *HRB* Special Report 132: Systems Building for Bridges, Highway Research Board, National Research Council, Washington, D. C. (1972) p. 8.
- Elsasser, H. B., "Erection," *HRB Special Report 132: Systems Building for Bridges*, Highway Research Board, National Research Council, Washington, D. C. (1972) pp. 49, 50.
- Sprinkel, M. M., "Overview of Latex Modified Concrete Overlays," VHTRC 85-R1, Virginia Highway and Transportation Research Council, Charlottesville, Virginia (July 1984) pp. 25-30.

- TRB, NCHRP Synthesis 57: Durability of Concrete Bridge Decks, Transportation Research Board, National Research Council, Washington, D. C. (May 1979) 61 pp.
- Pfeifer, D. W. and M. J. Scali, NCHRP Report 244: Concrete Sealers for Protection of Bridge Structures, Transportation Research Board, National Research Council, Washington, D. C. (Dec. 1981) 137 pp.
- 72. Sprinkel, M. M., "Polymer Concrete Overlay on Big Swan Creek Bridge—Interim Report No. 1—Installation and Initial Condition of Overlay," VHTRC 84-R26, Virginia Highway and Transportation Research Council, Charlottesville, Virginia (Feb. 1984) pp. A-3, A-4.
- 73. "Manual for Quality Control for Plants and Production of Precast Prestressed Concrete Products," Prestressed Concrete Institute, Chicago, Illinois (1977).
- PCI Committee on Industry Standards, "Precast Prestressed Concrete Industry Code of Standard Practice for Precast Concrete," *PCI Journal*, Vol. 23, No. 1 (Jan.-Feb. 1978) pp. 14-31.
- Waddell, J. J., Precast Concrete: Handling and Erection, American Concrete Institute, Iowa State University Press (1974).
- Holesapple, J. C., "Transportation," *HRB Special Report* 132: Systems Building for Bridges, Highway Research Board, National Research Council, Washington, D. C. (1972) p. 47.
- 77. Curtis, R. B., "Single-Tee Bridges," Journal of the Prestressed Concrete Institute (April 1967) pp. 76-81.

- Brown, H. E., W. T. McKeel, Jr., and W. G. Gunderman, "Introduction," *HRB Special Report 132: Systems Building* for Bridges, Highway Research Board, National Research Council, Washington, D. C. (1972) p. 2.
- Alexander, J. A., "Application of Maintainability and Expected Cost Decision Analysis to Highway Design," TRB Special Report 148: Innovations in Construction and Maintenance of Transportation Facilities, Transportation Research Board, National Research Council, Washington, D. C. (1974) p. 4.
- Miller, D. O. and R. D. Beckman, "Renovation of the Third Avenue Bridge Over the Mississippi River," *Proceedings* Second Bridge Engineering Conference, TRR 950, Vol. 1 (Sept. 24-26, 1984) p. 153.
- "Push Repair Jobs Faster? DOTs Vary on Incentives," Highway and Heavy Construction, Vol. 127, No. 8 (Aug. 1984) pp. 46-47.
- 82. "Unique Repair Contracts Spur Fast Jobs," Highway and Heavy Construction, Vol. 127, No. 8 (Aug. 1984) p. 48.
- TRB, NCHRP Report No. 255: Highway Traffic Data for Urbanized Area Project Planning and Design, Transportation Research Board, National Research Council, Washington, D. C. (1982) p. 140.
- Memmott, J. L. and C. L. Dudek, "A Model to Calculate the Road User Costs at Work Zones," *Texas Transportation Institute Research Report 292-1*, Austin, Texas (Sept. 1982) p. 20.

BIBLIOGRAPHY

- Bender, B. F., "Prestressed Concrete Bridges," *Preprint 2742*, ASCE Annual Convention, (Sept. 27–Oct. 1, 1976) 20 pp.
- Blaha, B., "Skyscraper-size Concrete Piers for New Tampa Bay Crossing," Concrete Products (Oct. 1984) pp. 16-19.
- Byrd, Tallamy, MacDonald & Lewis, NCHRP Report 161: Techniques for Reducing Roadway Occupancy During Routine Maintenance Activities, Transportation Research Board, National Research Council, Washington, D. C. (1975) 55 pp.
- "Contractor Earns Big Bonus Redecking Busy Bridge Fast," Highway & Heavy Construction (June 1984) pp. 48-50.
- Degenkolb, O. H., Concrete Box Girder Bridges, American Concrete Institute (1977) 106 pp.
- "Earth Structures Reinforced with Steel Strips Resist Lateral Pressures," Concrete Construction (July 1984) pp. 653-655.
- "Genstar Structures Ltd.: Alberta's Premier Precaster," Concrete Products, Chicago, Illinois (January 1984) p. 19.
- "Instant Bridge Erected in 17 Hours," *Better Roads*, Vol. 48, No. 5 (May 1978) p. 25.
- Munjal, S. K., "Evaluation of 'BEBO' System Culvert," Maryland Department of Transportation (July 1983) 19 pp.
- PCA Research and Development Bulletin, RD080.01E, Portland Cement Association, Skokie, Illinois (1982).
- PCI Committee on Connection Details, "PCI Manual on Design of Connections for Precast Prestressed Concrete," Prestressed Concrete Institute (1973) 99 pp.
- "Permanent Steel Forms," American Iron and Steel Institute, New York, New York.
- "Precast Concrete Bridge Decks," Portland Cement Association (1953) 20 pp.
- Rabbat, B. G. and H. G. Russell, "Optimized Sections for

Precast Prestressed Bridge Girders," *Journal of the Prestressed Concrete Institute*, Vol. 27, No. 4 (July-Aug. 1982) pp. 88-104.

- Reed, R. L., "Application and Design of Prestressed Deck Panels," TRR 665: Bridge Engineering: Volume 2, Transportation Research Board, National Research Council, Washington, D. C. (1978) pp. 164-171.
- Sack, R. L., "Investigation of Precast and Prestressed Concrete Bridges for Low-Volume Roads," *TRB Special Report 160: Low-Volume Roads*, Transportation Research Board, National Research Council, Washington, D. C. (1975) pp. 105– 115.
- Schaffer, E. L., "Timber Bridges: Implementing the Technology," White Paper on Workshop held in Milwaukee, Wisconsin (October 3-4, 1983).
- Schutz, R. J., "Epoxy Adhesives in Prestressed and Precast Concrete Bridge Construction," *Journal of American Concrete Institute* (March 1976) pp. 155–159.
- Sprinkel, M. M., "Construction of Prestressed Concrete Single-Tee Bridge Superstructures," VHTRC 77-R50, Virginia Highway & Transportation Research Council, Charlottesville, Virginia (May 1977) 96 pp.
- TRB, TRB Special Report 166: Optimizing the Use of Materials and Energy in Transportation Construction, Transportation Research Board, National Research Council, Washington, D. C. (1976) 74 pp.
- TRB, TRR 871: Segmental and System Bridge Construction; Concrete Box Girder and Steel Design, Transportation Research Board, National Research Council, Washington, D. C. (1982) 80 pp.

APPENDIX A

PREFABRICATED BRIDGE ELEMENTS AND SYSTEMS

System	Description	Figure No.
C-Series	- Concrete Structures	
C-1	Precast Concrete Slab Span	1
C-2	Precast Box Beam	2
C-3	Double-Tee and Channnel Beam	3
C-4	Inverted Channel Beam	4
C-5	Multistemmed Beam	5
C-6	Prestressed Single-Tee	6
C-7	Prestressed Bulb-Tee	7
C-8	Prestressed I-Beam	8
C-9	Short-Span Segmental Construction	47, 48
S-Series	- Steel Structures	
S- 1	Prefabricated Steel Bridges	9, 10, 11, 12
S-2	Temporary Bridges	13
S-3	Precast Deck Panel	14, 15, 16
S-4	Laminated Timber Deck on Steel Beams	17
S-5	Timber Plank Deck on Steel Beams	18
S-6	Steel Grid Deck on Steel Beams	19
S-7	Bituminous Concrete Deck on Steel Planks	20
S-8	Orthotropic Steel Plate Deck	21
S-9	Site-Cast Deck on Steel Beams	22
T-Series	- Timber Structures	
T-1	Glued-Laminated Timber	23, 24, 25, 26
T-2	Nail Laminated Timber	27
T-3	Solid Sawn Timber Beams	28
T-4	Plywood Deck Surface	29
M-Serie	s - Miscellaneous Bridge Elements	
M-1	Precast Abutment and Wingwall	30
M-2	Pile Substructures	31, 32, 33
M-3	Span-Shortening Substructures	34
M-4	Permanent Bridge-Deck Forms	35, 36, 37
M-5	Parapet and Rail Systems	38, 39, 40, 41, 42
M-6	Long-Span, Corrugated-Metal, Buried Conduits	43
M-7	Precast Concrete Arch Bridge	44
M-8	Single and Multiple Culverts of Aluminum, Concrete, and Steel	45
M-9	Field-Connected Beams	46



ω Ν ----SYSTEM NUMBER NAME OF SYSTEM: Typical Typical Typical FIGURE C-2 PRECAST BOX BEAM **Prestressed Concrete** Cast-in-Place Concrete Keyway Longitudinal Section Box Beam PAGE 1 OF 2 N (See System M4 for Detail Spread PRECAST DESCRIPTION: Detail Precast, pretensioned or posttensioned box beams with or without wearing surface. Boxes Dimension PROMINENT FEATURES: BOX Subdeck Boxes are modular and therefore may be precast in various lengths and Wearing widths to accommodate a range of spans and roadway widths. Box beams are generally used for spans of approximately 50 to 100 ft. Except 38 Range ; for the longer spans, the boxes are very easy to transport and erect. Box beams which are placed adjacent to each other are usually connected AM Surfac in the same way slabs are connected. See System Number C-1. Box beams which are spaced apart (spread boxes) are tied together with diaphragms and a cast-in-place concrete overlay is added. A wearing surface may Depth be used with the box beams. See Figure 2. N. . ິ ລຸ ອຶ Width (Also Bituminous Grouted Details ω . S Adjacent Boxe σ Keywa System Wearing CASE EXAMPLES: PAGE SYSTEM Widely used. 2 Surface tor Connection NUMBER MANUFACTURERS : IJ Most prestressed concrete plants should be properly equipped for produc-QF tion. 02 **REFERENCES**: N Prestressed Concrete Institute (Reference 1) Federal Highway Administration (Reference 3) Virginia Prestressed Concrete Association (Reference 4) Public Works (Reference 5)





NAME OF SYSTEM: SYSTEM NUMBER INVERTED CHANNEL BEAM C-4 PAGE 1_ OF 2 PAGE 1_ OF 2 DESCRIPTION: Prestressed, inverted channel beams with cast-in-place concrete deck. PROMINENT FEATURES: Prestressed channel members may be precast in conventional or inverted position and in various lengths and depths to accommodate a range of

position and in various lengths and depths to accommodate a range of spans between 30 and 80 ft. If precast in conventional position, the beams must be turned over before they are erected at the bridge site. A voided box beam is achieved by arching corrugated steel forms between the upright legs of the channel. The channels are tied together and the superstructure is completed with the installation of the cast-in-place concrete deck.

A precast trapezoidal beam which is reported to be economical for spans of 100 to 150 ft. has been developed in Ontario. The trapezoidal beam bridge is similar to the inverted channel beam bridge with the exception that the legs of the trapezoidal beam are slanted rather than vertical and the beams are much heavier than channel beams.

CASE EXAMPLES:

Several prototype inverted channel structures have been constructed in Missouri and trapezoidal beam bridges have been constructed in Canada.

MANUFACTURERS:

Ontario Precast Concrete Manufacturers Association Local precast, prestressed concrete producers

REFERENCES:

Salmons, John R. (Reference 11) Salmons, John R. (Reference 12) Nairn, R. D. (Reference 13)



NAME OF SYSTEM:	SYSTEM NUMBER
MULTISTEMMED BEAM	C-5
	PAGE <u>1</u> OF <u>2</u>
DESCRIPTION:	· · · · · · · · · · · · · · · · · · ·
Precast, prestressed multistemmed beams.	
PROMINENT FEATURES:	
Multistemmed beams are modular and therefore e lengths and increments of width to accommodate roadway widths. The members are most suitable 50 ft. The shape is particularly suited for 1 installations. Shear transfer between the mod achieved with a grouted keyway and weld plates	asily precast in various a range of spans and for spans of 25 ft. to ow depth-to-span ratio ular units is usually
CASE EXAMPLES: Several bridges have been constructed in the n	orthwestern states.
MANUFACTURERS:	
Central Premix Concrete Company of Spokane, Wa available, most prestressed concrete producers producing the member.	shington. If forms are should be capable of
REFERENCES:	
rrestressed Concrete Institute (Reference 1) "Instant Bridges" (Reference 8)	



SYSTEM NUMBER NAME OF SYSTEM: C-6 FIGURE PRESTRESSED SINGLE-TEE Precast PAGE 1 OF 2 an 3 ი Deck a6 BLIDK DESCRIPTION: 9 Pocket PRESTRESSED 6 Precast, prestressed single-tee beam. Flange - 6-0 Precast Cement Grouted Part **PROMINENT FEATURES:** Single-tee beams are modular and therefore easily precast in various 9 lengths, widths and depths to accommodate a range of spans and roadway Paste with Deck widths. Single-tee beams are customarily used for spans between 30 ft. to 80 ft.; however, spans up to 130 ft. have been constructed. Transportation and erection difficulties may occur with longer spans. SINGLE Temporary bracing is required during transportation and erection because of the unstable nature of the beam. Single-tee beams may be connected in several ways, but shear transfer between the tee beams is usually achieved through the use of grouted keyways and transverse tie Ł H rods or weld plates. End diaphragms and a cast-in-place concrete topping are also generally used in single-tee construction. When the m full deck thickness is included in the tee flange, a bituminous surface is usually used as a leveling course. CASE EXAMPLES: Single-tee beams have been used in Washington, Connecticut, Virginia, Site -Cast Concrete Bituminous SYSTEM PAGE West Virginia, Idaho, Montana and a number of other states. MANUFACTURERS: If forms are available, most prestressed concrete plants should be NUMBE N Wearing capable of producing the members. 0 F **REFERENCES:** 0 Wearing N Prestressed Concrete Institute (Reference 1) Surfac Prestressed Concrete of Colorado (Reference 6) "Instant Bridges" (Reference 8) Virginia Department of Highways & Transportation (Reference 14) S Curtis, Robert B. (Reference 15) Sprinkel, Michael M. (Reference 16) lace

NAME OF SYSTEM:	SYSTEM NUMBER	Minimum Width and Depth	,
PRESTRESSED BULB-TEE	C-7	60 [*]	
	PAGE_1_0F_2_		
DESCRIPTION:			
Precast, prestressed bulb-tee beams.			
PROMINENT FEATURES:		24	
Bulb-tee beams have a high section modulus-to-wei are economical for longer spans and for precastin A curb is often precast on the exterior beam. Th in the Northwest United States where it is commo 60 ft. to 80 ft. However, spans of up to 160 ft. the literature. Special consideration must be gi erecting the larger beams. The beams are usually plates and grouted keyways. As indicated by Fig depth of the web and the width of the flange may the most economical beam for a given span.	ght ratio and therefore g the deck on the beams. e bulb tee is popular nly used for spans of have been reported in ven to transporting and connected with weld ure 7, the be varied to provide	Maximum Width and Depth	
		331/2	n N
			57-
CASE EXAMPLES:			
Many bridges have been constructed in Idaho, Wash	ington and Montana.	► 9½ -	
MANUFACTURERS :			5 F
Concrete Technology, Central Premix, Ready-to-Pou plants in the Northwest United States.	r Concrete, and other		
REFERENCES: Prestressed Concrete Institute (Refe "Instant Bridges" (Reference 8) Anderson, Arthur R. (Reference 17) "RTP Markets Instant Bridges" (Reference 18) Prestressed Concrete Institute (Reference 19)	erence 1)	*Variable Dimension SYSTEM NUMBER FIGURE 7. PRESTRESSED BULB-TEE PAGE _2 OF	C 7



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NAME OF SYSTEM:	SYSTEM NUMBER	NAME OF SYSTEM:	SYSTEM NUMBER
PREFABRICATED STEEL BRIDGES	S-1	PREFABRICATED STEEL BRIDGES	S-1
	PAGE <u>1</u> OF <u>6</u>		PAGE <u>2</u> OF <u>6</u>
DESCRIPTION: Standard prefabricated steel superstructure comp and topped with a wearing surface to provide a f PROMINENT FEATURES: Typically an orthotropic deck is prefabricated as standard steel superstructure component. The sta components are transported to the bridge site, co covered with a wearing surface to provide a fast- Several types of systems are available. One system consists of prefabricated T-shaped unit together at the site. The units are 80 ft. long suitable for multiple span situations requiring s See Figure 9. (21) Another system consists of prefabricated rectangu- usually bolted together at the site. Four standa which are interchangeable so that many site condi- dated. Two of the units are shown in Figure 10. girder unit, and the other is a one-web unit which either side of a main girder unit or to another on a range of roadway widths. The other two standar to the ones shown in Figure 10 with the exception only 19'-8" and their webs are tapered from a dep end to 19-3/4" at the other end. (22) A third system is made up of prefabricated units eral plate girders or rolled sections which are to bridge plank. The modular units with the plate g spans up to 100 ft. and the units with the rolled for spans up to 50 ft. See Figure 11. (23) A fourth system consists of steel girders and a t	PAGE <u>1</u> OF <u>6</u> ponents are connected ast-assembly bridge. an integral part of a ndard superstructure nnected together and assembly bridge. ts which are bolted and 6 ft. wide and are pans of 50 to 110 ft. lar units which are rd units are available tions can be accommo- One is a two-web main h can be bolted to ne-web unit to provide d units are identical that their length is th of 39-1/2" at one which consist of sev- opped with steel irders can be used for sections are suited reated timber deck.	CASE EXAMPLES: Tee-shaped units fabricated by Nobels-Kline hav America and Europe and are available in the Uni lar units fabricated by Krupp Company have been consisting of bridge plank and plate girders ar west United States, and the units with the roll in the Midwest United States. The units with t are popular in the logging territories of Alask MANUFACTURERS: Nobels-Kline, Ltd., Columbia, South Carolina Krupp Company, Rheinhausen, Germany Spokane Culvert Company, Spokane, Washington Armco Steel Company, Middletown, Ohio Hamilton Construction Company, Springfield, Ore REFERENCES: "Nobels-Kline, Ltd." (Reference 21) Kroger, Elmer (Reference 22) Godfrey, K. A., Jr. (Reference 23) Muchmore, F. W. (Reference 24)	PAGE <u>2</u> OF <u>6</u> e been used in South ted States. Rectangu- used in Germany. Unit e popular in the North- ed sections are popular ne treated timber deck a.
A fourth system consists of steel girders and a t Each prefabricated unit supports one line of whee connected with diaphragms which are bolted to the tures are presently designed for off-highway logg typical span range is 30 to 80 feet. See Figure	reated timber deck. ls and the units are units. The struc- ing loadings and the 12.(24)		
Manufacturers who are known to have supplied thes Indicated below but it is likely that in most ins fabricator could supply comparable prefabricated	e steel bridges are tances a local steel units.		





NAME OF SYSTEM:	SYSTEM NUMBER	
TEMPORARY BRIDGES	S-2	PAGI
	PAGE <u>1</u> OF <u>2</u>	
DESCRIPTION :	•	
Steel truss bridges which are quickly assembled a standard preassembled components.	t the site from .	
PROMINENT FEATURES: Standard preassembled steel components are easily by unskilled labor. The truss bridges come in a can accommodate spans up to 300 ft. The standard bridge are stocked by the manufacturers and can b the site. Some of the bridges can be launched in The bridges are over designed for most installativers versatile as they can be disassembled and used at the bridges can be leased or purchased.	v assembled at the site range of widths and components of the be easily transported to ito place from one end. Jons but are extremely to other sites. Also,	Transom Swaybrace Single Bearing Hase Plate FIGURE 1
CASE EXAMPLES:		
Bridges can be found all over the United States a world.	and other parts of the	St Fran
MANUFACTURERS: Bailey Bridges, Inc., San Luis Obispo, California Acrow Corporation of America, Carlstadt, New Jers	sey	DRARY B
REFERENCES:		
Acrow Panel Bridge, (Reference 25) "Acrow Panel Bridge Replaces Two Spans Destroyed (Reference 26)	by Flood", ENR	m m m m m m m m m m m m m m m m m m m

		_
NAME OF SYSTEM:	SYSTEM NUMBER	
PRECAST DECK PANEL	S-3	
· · · · · · · · · · · · · · · · · · ·	PAGE_1_OF_4_	
DESCRIPTION:		
Precast concrete panels are placed transversely or steel stringers.	longitudinally on	
PROMINENT FEATURES:		
Precast concrete panels are placed transversely or steel stringers. Transverse panels may be prestre direction and are usually connected by a cast-in-p but examples are also cited in the literature wher tensioned parallel to the direction of traffic or grouted keyways. Longitudinal panels are usually place concrete joint which runs parallel to traffi may be easily achieved with the longitudinal syste are precast integrally with the stringers (Figure is not usually achieved with the systems in which to the stringers at the site (Figure 15), but examp literature where composite action was achieved the on-site formwork and concreting typically required concrete deck bridge.	 longitudinally on essed in the transverse place concrete joint, se the panels are post- are connected with connected by a cast-in- ic. Composite action em if the deck panels 14). Composite action the panels are attached ples are cited in the rough the use of studs ms eliminate most of the l for a steel stringer- 	
CASE EXAMPLES:		
New York, Alabama, Indiana, Pennsylvania		
MANUFACTURERS :		
Components can be secured from local precast conc steel fabricators.	rete producers and	
REFERENCES: "Short-Span Steel Bridges, U. S. Stee Biswas, Mrinmay and others (Reference 28) "Low-Cost, No-Care Bridge", <u>Better Roads</u> , (Referen NCHRP (Reference 30)	el Corp. (Reference 27) nce 29)	FIG PR





NAME OF SYSTEM:	SYSTEM NUMBER	5	A
LAMINATED TIMBER DECK ON STEEL BEAMS	S-4	minate	
	PAGE_1_OF_2_	Figure 9d Ti 9l Stt	
DESCRIPTION:		mbe ring	
Laminated timber deck is placed on steel stringers	ì.	ers De	A-161
PROMINENT FEATURES:		Č X	
The timber laminations may be connected with glue laminations are glued together (glulam) the deck i which are fabricated at a plant. Dowels are usual load transfer between panels. When the lamination the deck is usually constructed at the site, in wh not used, however, panels could be nail laminated at the site. The deck is usually connected to a t bolts as shown in Figure 17 or connected directly stringers with bolts and clips as shown in Figure material is generally used on the deck for increas skidding and weathering.	or nails. When the s assembled from panels ly used to provide for is are nailed together, nich case dowels are at a plant and assembled imber bolster with lag to the flange of the 18. A surfacing sed resistance to	g	
			×
CASE EXAMPLES:		$ \rangle \rangle \gamma_{\rm c}$	
Virginia, Alaska and a number of other states.			
MANUFACTURERS :			
Supplies can be obtained from distributors located	d throughout the country		
REFERENCES: U. S. Steel Corporation (Reference 31) "Steel Beams with Glulam Flooring", VDHT (Reference Sprinkel, M. M. (Reference 33)	ce 32)		

PAGE

Timber Bolster 8x10" Steel Stringer Depth 2 to 3 Spaced 8 ± Dowel 11's Diameter x 1 - 7's Spaced 12"± Lateral Bracing Diaphragm Bracket Bituminous Wearing Surface Lag Bolt ¼ Diameter x 12" Lagminated Timber Deck 6¼ Thick 3/4 Bolt through bolster and top flange of stringer

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SYSTEM NUMBER N . ନ୍

S 4 N



5-0				
PAGE 1 OF 2		i weid Grid I Grid I Bei Bea		
stringers.		as Require Deck on ams		
dular open steel grids. ete. A variety of sizes ds of a particular site. in. x 4 in. deep. The needs of a bridge. The erefore lend themselves he grids are unique in low deck system. Skid adding steel studs or illing the grid with		SYS PAG		
		EM NUMBER		-Steel Grid: Depth 5 ± Width 8 ± Length - 1 Steel Beams Spaced 7
steel companies should		N (S 6	n · n ·	- 6 t
bout Them?" (Ref. 36)				Bridge
	stringers. dular open steel grids. ete. A variety of sizes ds of a particular site. in. x 4 in. deep. The needs of a bridge. The erefore lend themselves he grids are unique in low deck system. Skid adding steel studs or illing the grid with steel companies should bout Them?" (Ref. 36)	stringers. dular open steel grids. ete. A variety of sizes ds of a particular site. in. x 4 in. deep. The needs of a bridge. The erefore lend themselves he grids are unique in low deck system. Skid adding steel studs or illing the grid with steel companies should bout Them?" (Ref. 36)	stringers. dular open steel grids. etc. A variety of sizes ds of a particular site. in. x 4 in. deep. The needs of a bridge. The erefore lend themselves he grids are unique in low deck system. Skid adding steel studs or illing the grid with steel companies should bout Them?" (Ref. 36)	stringers. dular open steel grids. etc. A variety of sizes ds of a particular site. in. x 4 in. deep. The erefore lend themselves he grids are unique in low deck system. Skid adding steel studs or illing the grid with Store MNUMBER N 00 F ER N 00 F ER F E

NAME OF SYSTEM:	SYSTEM NUMBER	
BITUMINOUS CONCRETE DECK ON STEEL PLANKS	S-7	Figure Figure
	PAGE_1_0F_2_	
DESCRIPTION:		
Steel stringers support corrugated steel plank whi concrete wearing surface.	ch supports bituminous	
PROMINENT FEATURES:	,	
Standard steel stringers are spaced approximately Stringer spacing and size of beams are, of course, bridge span and live loading. Steel bridge plank and connected by bolting or welding. Some authori rather than welding on structures where the traffi bituminous concrete wearing surface which is usual thickness of about 3 inches is placed on the bridg lends itself to rapid construction because of the cement concrete. See Figure 20.	2 ft. on center. a function of the is used on the stringers ties recommend bolting c count is high. A ly compacted to a e plank. The system absence of portland	rface and Steel Stringers
CASE EXAMPLES:	······	
Used in Ohio, Colorado and Virginia.		sel Brid Winimu Witt or W sel Strii annel f
MANUFACTURERS :		
Materials and labor are usually available locally obtained from Armco, Bethlehem and others.	. Bridge plank may be	lank aring : Deptt
REFERENCES :		B sturs a ture
Schukraft, Bernard (Reference 37) Colorado Department of Highways (Reference 38)		ing tree

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NAME OF BIBIEM.	SYSTEM NUMBER	
ORTHOTROPIC STEEL PLATE DECK	S-8	Figur
	PAGE 1 OF 2	e 2
DESCRIPTION:		0
Steel I-beams support standard orthotropic stee units.	l plate bridge floor	rthotr
PROMINENT FEATURES:		
plate floor units as shown in Figure 21. The of be placed parallel to the stringers in which ca support the plate. The orthotropic plate deck variety of sizes and shapes to accommodate a ra beam spacings typically between 7 to 20 ft. Th ly 3/8 to 3/4" thick and the depth of the ribs 14.0". Although orthotropic steel plate decking has be long span bridges to minimize the weight of the	what of those plates may se floor beams must is available in a nge of stringer or floor e top plate is typical- is typically 8.0 to en used primarily on superstructure, the	its to plate) Steel Plate Deck (
decking has seen occasional use on short span b concern was to provide a bridge which could be short time. Because the orthotropic plate deck and easily handled, it is particularly suited f tion and replacement. An epoxy grit or modifie face is generally used to provide adequate skid protect the steel from water and salt.	ridges where the major installed in a very ing is relatively light or rapid deck construc- d asphalt wearing sur- resistance and to	On Steel Beams
decking has seen occasional use on short span b concern was to provide a bridge which could be short time. Because the orthotropic plate deck and easily handled, it is particularly suited f tion and replacement. An epoxy grit or modifie face is generally used to provide adequate skid protect the steel from water and salt. CASE EXAMPLES: An experimental bridge built Corporation at its Sparrows Point, Md., plant in built to explore the use of prefabricated, all-s the construction of highway bridges in the span MANUFACTURERS: Bethlehem Steel Corporation and Reliance Steel C	ridges where the major installed in a very ing is relatively light or rapid deck construc- d asphalt wearing sur- resistance and to by the Bethlehem Steel 1964. The bridge was teel modular units for range of 20 to 100 ft.	On Steel Beams
decking has seen occasional use on short span b concern was to provide a bridge which could be short time. Because the orthotropic plate deck and easily handled, it is particularly suited f tion and replacement. An epoxy grit or modifie face is generally used to provide adequate skid protect the steel from water and salt. CASE EXAMPLES: An experimental bridge built Corporation at its Sparrows Point, Md., plant in built to explore the use of prefabricated, all-s the construction of highway bridges in the span MANUFACTURERS: Bethlehem Steel Corporation and Reliance Steel C fabricators should be able to fabricate the ort REFERENCES:	ridges where the major installed in a very ing is relatively light or rapid deck construc- d asphalt wearing sur- resistance and to by the Bethlehem Steel 1964. The bridge was teel modular units for range of 20 to 100 ft. ompany. Other steel hotropic plate decks.	On Steel Beams
decking has seen occasional use on short span b concern was to provide a bridge which could be short time. Because the orthotropic plate deck and easily handled, it is particularly suited f tion and replacement. An epoxy grit or modifie face is generally used to provide adequate skid protect the steel from water and salt. CASE EXAMPLES: An experimental bridge built Corporation at its Sparrows Point, Md., plant in built to explore the use of prefabricated, all-s the construction of highway bridges in the span MANUFACTURERS: Bethlehem Steel Corporation and Reliance Steel C fabricators should be able to fabricate the ort REFERENCES:	ridges where the major installed in a very ing is relatively light or rapid deck construc- d asphalt wearing sur- resistance and to by the Bethlehem Steel 1964. The bridge was teel modular units for range of 20 to 100 ft. ompany. Other steel hotropic plate decks.	On Steel Beams



S



NAME OF SYSTEM:	SYSTEM NUMBER	
GLUED-LAMINATED TIMBER	T-1	ure 23
•	PAGE 1_OF_4_	
DESCRIPTION:		
Glued laminated timber "Glulam" beams and deck pa	mels.	Cộn sựp
PROMINENT FEATURES:		
Modular beams and deck panels are plant manufactur standard size lumber. Standard wood treating tec provide a long service life. The panels and beam connected with relatively light equipment and car Two connection details are commonly used. One co provide for shear transfer between panels and lag panels to the beams. See Figures 22 and 24. The patented deck brackets which connect the panels t eliminate the need for the dowels between panels. A bituminous wearing surface must be placed on the timber from wear and to provide skid resistance.	ared by gluing together chniques are used to as may be erected and cpentry oriented labor. msists of dowels which g bolts which tie the e other detail requires to the stringers and . See Figures 23 and 25. The panels to protect the	ions
CASE EXAMPLES: Case examples can be found in Virginia, Oregon, N York, Colorado, and many other states. The bridg areas where timber is abundant.	Washington, Alaska, New ges are most common in	AGE 2 ag Bolt 3/ siulam Pan 6 3/4 Thic bowel Hold bowel Hold bowel Hold bowel 11/2 Spaced siulam Gir Bepth Width Spaced Ngle 6 x il Dimensi
MANUFACTURERS: Contact AITC for a list of fabricators, which are United States.	e located throughout the	OF 4 4 Dia. x 1: 10^{10} X 1: 10^{10} X 1: 10^{10} X 1: 10^{10} X 1: 12^{10} Y 12 12^{10} X 19 Dia. 'X 5/16 '' '' '' ''
REFERENCES: Bruesch, L. D. (Reference 43) Virginia Department of Highways & Transportation Weyerhauser (Reference 45 and 46) AITC (Reference 47), VDHT (Reference 48)	(Reference 44)	

SYSTEM NUMBER

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	SYSTEM NUMBER						٦
NAIL LAMINATED TIMBER	T-2	Figur #		Boit - Typical			
	PAGE <u>1</u> OF <u>2</u>	e 27.		Conn	Cap		
DESCRIPTION:		Nai		D ectio			
Treated lumber is nail laminated and to	pped with a wearing surface.	1		5			
PROMINENT FEATURES: The deck is easily constructed at the julabor. Treated lumber is placed in the nailed to adjacent pieces and alternate pile cap. The deck is usually covered surface. However, concrete may be place composite concrete-timber deck and in the two or more depths to result in a corrus suitable for spans of approximately 20	ob site by carpentry oriented longitudinal direction and pieces are toenailed to the with a bituminous wearing ed on the timbers to provide a his case the laminations are of gated effect. Both systems are ft.	inated Timber Superst	fasher 5x5x % teel Shear Developer [for co imber 1/2 thick olt 34 Dia ile Cap 12 x12	veen Deck		Laminated Timb Bituminous We	
		ructure	mposite action]			er Deck with aring Surface	
		ructure	mposite action]			er Deck with aring Surface T	
CASE EXAMPLES:		ructure	mposite action]			er Deck with SY aring Surface PA Composi	
CASE EXAMPLES: One example in Virginia.		ructure	mposite action]			er Deck with SYSTE aring Surface PAGE Composite C Timber De	
CASE EXAMPLES: One example in Virginia. MANUFACTURERS:		ructure	mposite action $] \checkmark$			er Deck with SYSTEM NUM aring Surface PAGE 2 Composite Concret	
CASE EXAMPLES: One example in Virginia. MANUFACTURERS: May be constructed with locally availab	le materials.	ructure	mposite action $] \checkmark$			er Deck with SYSTEM NUMBER aring Surface PAGE 2 OF _ Composite Concrete La Timber Deck	

NAME OF SYSTEM:

SOLID SAWN TIMBER BEAMS

T-3

SYSTEM NUMBER

PAGE 1 OF 2

DESCRIPTION:

Solid sawn timber beams support various types of decking material.

PROMINENT FEATURES:

The system consists of treated timber stringers approximately 6 in. $x \ 18$ in. deep and spaced approximately 2 to 4 ft. apart to accommodate spans of approximately 20 ft. The stringers may be covered with a timber and bituminous deck or a concrete deck. A timber deck is nailed to the stringers and a concrete deck is cast around the top edge of the stringers.

CASE EXAMPLES:

Several examples in rural Virginia

MANUFACTURERS:

Locally available materials and labor.

REFERENCES:

Federal Highway Administration (Reference 49)



		<u></u>			
NAME OF SYSTEM:	SYSTEM NUMBER				8 6 0
PLYWOOD DECK SUREACE	T-4	Fig	•	\bigwedge	oated DS A
	PAGE <u>1</u> OF <u>2</u>	Ire 2			Plyw pike – 11 Dim
DESCRIPTION:		9. P	The second		rimbe
Polyurethane-resin-coated plywood serves as	deck surface.	ywo	A)		ns T Pla
PROMINENT FEATURES:		a -			ypica
Plywood sheets are supported by subflooring wood sheets are usually 4 ft. x 8 ft. and ar polyurethane resin. The plywood sheets are with glue and spikes. The sheets are typica wearing surface of a plank deck bridge so th to be replaced. This system should be consi low volume roads only.	and stringers. The ply- e coated in the shop with secured to the subflooring lly used to upgrade the at the planks do not have dered for structures on	Deck Surface			
CASE EXAMPLES: New Hampshire					PAGE
MANUFACTURERS:			ilue S		
Contact American Plywood Association			ap 12 [°] x udinal yr Timb yc. +	14 ·	JMBER OF _
REFERENCES:			Beam Beam		т с 4
American Plywood Association (Reference 50)			a ced		

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NAME OF SYSTEM:	SYSTEM NUMBER	
PRECAST ABUTMENT AND WINGWALL	M-1	Dowel Sieeve for Anchorage of Deck Members PAGE 2 0
	PAGE <u>1</u> OF <u>2</u>	Precast Abutment Panel
DESCRIPTION:		
Precast concrète abutment and wingwall pane.	ls.	
PROMINENT FEATURES:	· · · · · · · · · · · · · · · · · · ·	
Panels are modular and therefore easily pre- widths to accommodate a range of abutment he Panels are set on cast-in-place concrete par ported and then connected with weld plates a footing (see Figure 30). Several other sys non-proprietary) which utilize modular prec- used to obtain a comparable abutment.	cast in various lengths and eights and roadway widths. ds, and temporarily sup- and cast-in-place concrete tems (both proprietary and ast concrete units could be	Reinforcing Bar in
		Footing
CASE EXAMPLES:		Footing
A prototype structure has been constructed Washington, and proposed in Oklahoma.	in Garfield County,	
MANUFACTURERS: Central Pre-Mix Concrete Company, Spokane, Corporation, Plainville, Conn. Most precast properly equipped for production.	Washington. Atlantic Pipe concrete plants should be	
REFERENCES:	······································	
Prestressed Concrete Institute (Reference 1 "Instant Bridges" (Reference 8))	
Thompson, Pat (Reference 51) Imel, K	. Dean (Reference 52)	Figure 30. Precast Abutment and Wingwall





Figure 33. **Connection Details for Pile Substructures**

PAGE 3 OF 3



NAME OF SYSTEM:	SYSTEM NUMBER	
PERMANENT BRIDGE-DECK FORMS	M-4	
	PAGE_1_0F_3_	
DESCRIPTION:		
Permanent steel forming or prestressed concrete site-cast concrete deck.	subdeck panels support	
PROMINENT FEATURES: The ready-mix concrete required for site-cast co be formed with temporary or permanent bridge dec permanent deck forms of steel or subdeck panels have become popular because the high cost of the nated. Prestressed concrete subdecks provide ar less concrete and reinforcing steel must be place since the form becomes an integral part of the co	oncrete bridge decks must ck forms. In recent years of prestressed concrete e form removal is elimi- n added advantage in that ced at the bridge site deck.	Reinforcing Steel Steel Beam Stud Support Angles Permanent Steel Form Site-Cast Concrete Deck Figure 35. Permanent Steel Forms Permanent Steel Form
CASE EXAMPLES: Case examples can be found throughout the United	d States.	L Top Flange of Beam Beam Web
ANUFACTURERS:		NOTE: Vertical leg downward allows for higher form support elevations. Vertical leg upward allows for lower form support elevations.
REFERENCES: Engineering News-Record (Reference 20) Hilton, Marvin H. (Reference 57 and 58) Transportation Research Circular 181 (Reference	59)	SYSTEM NUMBER M4 Figure 36. Steel Form Connection Detail PAGE <u>2</u> OF <u>3</u>



Prestressed Concrete Subdeck Panels

Figure 37.

NAME OF SYSTEM: SYSTEM NUMBER M-5 PARAPET AND RAIL SYSTEMS PAGE 1 OF 3 1-0" max. DESCRIPTION: Typical parapet and rail systems suitable for use with most concrete, steel or timber replacement systems. 2-3["] min. PROMINENT FEATURES: A parapet or rail is generally designed to meet Section 1.2.11 of the AASHTO Standard Specifications for Highway Bridges. The post sizes and gauge of bridge rails shown in the following figures are typical. The parapet or rail is in most cases constructed from concrete, steel or timber or some combination of these materials. Aesthetics usually play a role in the choice of materials and the design. Grouted Void ---A concrete parapet is generally constructed on a bridge having a con-#8 Bor ----Metal Rail crete deck. The parapet is usually formed and constructed with ready-Mortar Bed **Reinforcing Bor**mix concrete at the site but precast parapets have begun to see Reinforcing Barlimited use in recent years. Steel reinforcement is typically used to anchor the parapet to the concrete deck. See Figures 38 and 39. Figure 38. Precast Concrete Parapet Figure 39. Site Cast Concrete Parapet Steel and/or timber rails and posts are generally used with bridges having a timber deck. The rail posts may be anchored to the exterior 12 Gage Steel Rail stringer, to the deck, or to both. See Figures 40, 41, and 42. W 6x 25 Posts Wheel Guard **Bituminous Wearing Surface** CASE EXAMPLES: Bolt Examples can be found throughout the United States. MANUFACTURERS: Materials are usually available locally. **REFERENCES:** Virginia Department of Highways and Transportation (Reference 32) Steel Beam Weyerhaeuser Company (Reference 43) SYSTEM NUMBER M 5 C 8 x 11.5 American Institute of Timber Construction (Reference 45) 4 3"x 3"x 5/16 Virginia Department of Highways and Transportation (Reference 60) PAGE 2 OF 3 FHWA Report No. RD-77-40 (Reference 61) Figure 40. Steel Rail and Post Connected to **Deck and Exterior Beam**


NAME OF SYSTEM:	SYSTEM NUMBER
LONG-SPAN, CORRUGATED-METAL, BURIED	M-6
CONDUITS	PAGE <u>1</u> OF <u>2</u>

DESCRIPTION:

Structures are made of corrugated-metal structural plate sections, field assembled in various closed or arch configurations to serve as large culverts or grade separation structures.

PROMINENT FEATURES:

Long span structural plate culverts or grade separation structures made of steel or aluminum are frequently suitable alternatives for small bridges. Maximum span lengths available from the various manufacturers currently range from just under 40 to just over 50 ft., and multiple lines have been used where great waterway openings have been required. These buried structures are covered in Sections 1.9.10 and 2.23 of the current (1977) AASHTO Standard Specifications for Highway Bridges, and an excellent, comprehensive report on them has been published by the FHWA (referenced below). No design capability is usually required of the purchaser beyond the determination of the waterway opening, as the manufacturers commonly check standard designs or design critical structures. Similarly, the presence of a representative of the manufacturer is usually required during construction. Experience on the part of the contractor or agency forces is desirable but not mandatory, as only normal earth moving and compaction procedures and equipment are used.

The AASHTO Specifications require certain minimum geometric and sectional properties and the use of special features such as thrust beams or compaction wings along the edge of the top arch section, soil bins on top of the structure, or transverse ribs. These special features, which are included in the designs of the six major fabricators, aid in compaction during construction and prevent unwanted distortion of the structure.

As is the case with all large, flexible, buried structures proper construction procedures must be followed. Compaction during backfilling is most important in attaining the desired load carrying capacity, and the configuration of the barrel must be held within specified limits.

Assuming that a site will accept a culvert configuration with at least the minimum required cover and that acceptable backfill material is available nearby, considerable economy may be realized. Among the advantages cited by manufacturers are relative ease of delivery in rural areas, savings when the bearing capacity of the subgrade is too poor for economical bridge foundations, and the elimination of deck distress from deicing salts.



NAME OF SYSTEM:	SYSTEM NUMBER
Precast Concrete Arch Bridge	M-7
	PAGE 1_OF 2_
DESCRIPTION:	
Modular precast concrete panels are connected w concrete to form an arched bridge.	ith cast-in-place
PROMINENT FEATURES:	
The system is proprietary and marketed under th arches are temporarily erected at the bridge si standard size precast concrete panels, which ar field welds and cast-in-place concrete. On som larly where the arch is wide and therefore many quired, it may be economical to cast full lengt eliminate the need for the temporary supports. material is compacted over the arch. The system for spans of less than approximately 50 ft.	e name "BEBO." Steel te to support the e joined together with e occasions, particu- segments are re- h segments so as to Conventionaly fill m is typically used
·	•
CASE EXAMPLES: The structures have been principally used in We land but one bridge has been constructed in Min- being considered elsewhere in the United States	st Germany and Switzer- nesota and others are
MANUFACTURERS :	······································
BEBO - International Heierli & Company, Zurich, Hancock Concrete Products Company, Minneapolis,	Switzerland Minnesota
REFERENCES :	
"The Reinforced Concrete Arched Bridge-BEBO Sys <u>Civil Engineering</u> (Refernece <u>64</u>)	stem" (Reference <u>63</u>)



NAME OF SYSTEM:	SYSTEM NUMBER
Single and Multiple Culverts of	M-8
ALUMANUM, WHELELE, and SLEEL	PAGE 1_OF 2_
DESCRIPTION: One or more pipes of aluminum, concrete, or steel provide adequate drainage beneath a roadway.	are placed so as to
PROMINENT FEATURES: Being prefabricated, cul- in a roadway in a short period of time. Metal cu- less than about 5 ft differ from the long-span si (see System M-6) in that little on-site assembly clal bracing is required in backfilling operation- culvert are usually laid end to end and coupled in usually with bolted bands, hugger connections, or tongue and groove joint or sleeve is typically us- sections of concrete pipe or culvert. For diametr 10 ft, the metal culverts are usually assembled tural plate sections. Precast concrete U-shaped a cast concrete units are placed end to end on site- (see Fig. 45). End walls that provide added stab acribed by the manufacturer. The roadway is const material. Culverts have an advantage over bridges in that co seldom required, there is no deck to deteriorate, relatively rapid. The principal disadvantages are flow, they cannot be used on navigable streams, ar maturely in some corrosive environments. Steel ci ized or coated with a bituminous material to preve CASE EXAMPLES: Numerous case studies of the use of culverts can b the United States.	verts can be installed liverts having a diameter tructural plate culverts is required and no spe- s. Sections of metal a variety of ways, sleeve joints. A ed to connect adjacent ers greater than about at the site from struc- sections (no bottom) bout 16 ft. The pre- c-cast footings or floors ility and help prevent crete, metal sheeting, erial in a manner pre- tructed over the fill bonstruction plans are and installation is that they can restrict d they deteriorate pre- ilverts can be galvan- ent corrosion.
MANUFACTURERS	
Manufacturers are located throughout the United St	ates.
REFERENCES: "RTP Markets Instant Bridges" (Re Armco Multi-Plate (Reference <u>65</u>) Corrugated Steel Pipe (Reference American Concrete Pipe Association Aluminum Storm Severs (Reference	ference <u>18</u>) 66) 1 (Reference <u>67</u>) 68)
NAME OF SYSTEM:	SYSTEM NUMBER
Field-Connected Beams	M-9
	PAGE 1 OF 2
DESCRIPTION: Standard, precast, prestressed I are connected end to end in the field so as to al a bridge with a longer span or larger deck joint possible without the field-made connections.	-beams or steel beams low the construction of spacing than is
Without field-made connections the maximum bridge often, the maximum deck joint spacing that can be by the maximum length or weight of the primary su be transported to the bridge site. For steel I-b used in the construction of a bridge superstructu has been common practice in most states for many welded splice plates to connect the beams end to the desired span length or deck joint spacing (se span concrete beams could be constructed by provi- casting the concrete beams to achieve the desired joint spacings. However, the most popular concre recent years are precast and prestressed ones suc ASANTO I-beam (see System C-8), and these beams he connected end to end in the field. A field-made of promise has been developed and tested at the Univ (see Fig. 46). The field connection of the I-bear supporting the I-beam segments on falsework, split between the segments, filling the joint with site- posttensioning the segments.	span length and, quite achieved is controlled pporting beams that can eams or plate girders re (see System S-9), it years to use bolted or end so as to provide e Fig. 46). Long- ding forms and site span length or deck te beams to be used in h as the standard ave not been routinely connection which shows ersity of Illinois a is achieved by ing the reinforcement -cast concrete, and
CASE EXAMPLES: Numerous case examples of ster connected end to end can be found throughout the 1 prototype two-span bridge incorporating three pred I-beam segments was constructed in Illinois in 19 MANUFACTURERS Steel connections-most steel fabricators Concrete connections-most precast, prestressed co can provide on-site posttensioning	el beams that have been Jnited States. A cast, prestressed 73. poncrete producers that
REFERENCES: U.S. Department of Transportation (Reference <u>3</u>) U.S. Department of Transportation (Reference <u>41</u>) Fadl, A. I., Gamble, W. L., and Mohraz, B. (Refere	ence <u>69</u>)





FIGURE 46. Field-Connected Beams

NAME OF SYSTEM:	SYSTEM NUMBER
Short-Span Segmental Construction	C-9
	PAGE 1 OF 3
DESCRIPTION: ' Precast or site-cast concrete segments are tied t tensioning.	ogether by post-
PROMINENT FEATURES: Standard concrete boxes incorporating the full ro or site-cast in a convenient length and postensis al direction to provide a continuous monolithic Although segmental construction has been popular decades, it began to gain popularity in the U.S. It has been used primarily for medium to long (1 multiple-span bridges, but recent studies have ind can be economical for use in constructing a typic crossing (73). Economy requires that all the seg same form and, if precast, that match casting gen for short-span construction, the segments would p falsework or constructed span bridges, the most pop is the balanced cantilever method, but the increm and the progressive placing method have also been requirements are much simpler for short spans. A structed by segmental construction is shown in Fi	hadway width are precast concerte superstructure in Europe for two only in the late 1970's 50 x 400 = ft spans) licated that the concept cal three-span grade ments be cast in the herally be required. brobably be erected on tring trues as shown in bular method of erection nental launching method a used. Postcensioning completed bridge con- igure 48.
The advantage of the system is that the shapes of selves to use in a variety of span lengths. Econ same form to construct segments for many bridges. tages of the system are the investment in forms, required for erection, and the engineering expert satisfactory job.	the segments lend them somy favors use of the The basic disadvan- the large equipment tise required for a
CASE EXAMPLES: Examples of medium- to long-spa can be found in Texas, Indiana, Colorado, Pennsyl 11lionis, and Kentucky. The best example of what short-span construction is the bridge being const Florida, which will have 101 spans 118 ft in let	n segmental construction Lvania, Washington, might be considered ructed in Long Key, gth.
MANUFACTURERS: Some specialized contractors and consultants shou a satisfactory structure.	old be able to provide
REFERENCES: PCI Journal (Reference <u>70</u>) Long Key Bridge (Reference <u>71</u>) Bridge Report (Reference <u>72</u>) Precast Segmental Box Girder Bridg	e Manual (Reference <u>73</u>)

Detail B





APPENDIX A REFERENCES

- 1. Prestressed Concrete Institute, "Short Span Bridges." Chicago, Ill. (1975).
- 2. Louisiana Dept. of Hwys., "Standard Plans for Precast Concrete Slab Units" (1974).
- Federal Highway Administration, "Standard Plans for Highway Bridges—Vol. 1, Concrete Superstructures" (Aug. 1968).
- 4. Virginia Prestressed Concrete Association, "New Approaches in Prestressed, Precast Concrete for Bridge Superstructure Construction in Virginia" (Aug. 1973).
- "County Highway Department Casts Its Own Prestressed Bridge Beams." Public Works (June 1975) pp. 84-85.
- 6. Prestressed Concrete of Colorado, Stanley Structures, LTD., "Plans for Tee-Beam Bridges" (1969).
- 7. Choctaw, Inc., "Standard Plans for Precast, Prestressed Concrete Bridge Slab." Mississippi (1959).
- 8. Central Premix Concrete Company, "Instant Bridges." Spokane, Wash.
- 9. Mississippi State Highway Department, "Standard Plans for Precast Posttensioned Channel Bridge Spans." Jackson, Miss. (June 1969).
- Kentucky Dept. of Transp., Bridge Plans and Correspondence, Frankfort, Ky. (Aug. 2, 1979).
- 11. SALMONS, J. R., "Design and Construction of a Precast-Prestressed Composite Bridge System." FCP Conference, Atlanta, Ga. (Oct. 1977).
- 12. SALMONS, J. R., "Structural Performance of the Composite U-Beam Bridge Superstructure." Jour. of the PCI, Vol. 16, No. 4, pp. 21-23 (July-August 1971).
- 13. NAIRN, R. D., "Precast Trapezoidal Beams for Bridges." Ontario Precast Concrete Manufacturers Association.
- 14. Virginia Dept. of Hwys. and Transp., Plans for Rte. 639 over Little River, Richmond, Va. (July 1974).
- 15. CURTIS, R. B., "Single-Tee Bridges." Jour. of the PCI, Vol. 12, No. 2, pp. 76-81 (Apr. 1967).
- SPRINKEL, M. M., and ALCOKE, W. H., "Systems Bridge Construction in Virginia." American Transportation Builder (June 1977) pp. 11-13.
- 17. ANDERSON, A. R., "Systems Concepts for Precast and Prestressed Concrete Bridge Construction." *HRB Special Report 132* (1972) pp. 9-21.
- 18. "RTP Markets Instant Bridges." Concrete Products (Feb. 1968) pp. 48-51.
- 19. "Modern Concepts in Prestressed Concrete Bridge Design." PCI Bridge Bulletin, Second Quarter (1972).
- 20. "Panels Eliminate Deck Forms." Engineering News-Record (Apr. 1963) p. 79.
- 21. "Nobels-Kline, Ltd.," Columbia, South Carolina.
- KROGER, E., "Fast-Assemble Bridge Over the Aegidientorplatz in Hanover." HRB Special Report 132 (1972) pp. 34-41.
- GODFREY, K. A., JR., "Cutting Cost of Short Span Bridges." Civil Engineering (July 1975) pp. 42-46.

- 24. MUCHMORE, F. W., "Portable Bridges for Use in Logging Roads."
- "Acrow Panel Bridge Unit Construction Bridging and Support System." Thomas Storey (Engineers) LTD., London (1970) p. 5.
- 26. "Acrow Panel Bridge Replaces Two Spans Destroyed by Flood." Engineering News-Record (Oct. 5, 1978) p. 4.
- 27. U.S. Steel Corporation, "Short Span Steel Bridges" (Sept. 1973).
- BISWAS, M., ET AL., "Precast Bridge Deck Replacement Applications." Paper presented at Highway Research Board Summer Meeting, Olympia, Wash. (Aug. 1973).
- 29. "Low-Cost, No-Care Bridge." Better Roads (Feb. 1971) p. 11.
- 30. "Reconditioning High-Volume Freeways in Urban Areas," NCHRP Synthesis of Highway Practice 25 (1974) 56 pp.
- U.S. Steel Corporation, "Bridge Structural Report-Nine Steel Bridges for Forest Development Roads South Tonguss National Forest Alaska" (June 1973).
- 32. Virginia Department of Highways and Transportation, "Steel Beams with Glulam Flooring" (July 1976).
- 33. SPRINKEL, M. M., "Glulam Timber Deck Bridges." Virginia Highway and Transportation Research Council (Nov. 1978).
- 34. Virginia Dept. of Hwys. and Transp., "Standard Steel Beam Bridges" (Sept. 1975).
- 35. Greulich, Inc., "Rural and Urban Roads" (Aug. 1978).
- 36. "Pittsburgh's Troubled Bridges: What To Do About Them?," Civil Engineering (Jan. 1978) pp. 46-51.
- 37. SCHUKRAFT, B., "Stark County Bridge Department: A Profile." Better Roads (Dec. 1971) pp. 12-14.
- Colorado Department of Highways, "Plans for Michigan Creek Bridge, Jackson County Road #12." Colorado Springs, Colo.
- 39. "Orthotropic Plate Design for Steel Bridges." The James F. Lincoln Arc Welding Foundation, Cleveland, Ohio (1965).
- 40. "Design Aid for Orthotropic Bridge Decks Using Bethlehem Standard Ribs." Bethlehem Steel Corporation, Bethlehem, Pa. (May 1968).
- 41. U.S. Department of Transportation, "Standard Plansfor Highway Bridges-Vol. II, Structural Steel Superstructures." Washington, D.C. (Apr. 1968).
- 43. BRUESCH, L. D., "Timber Bridge Systems." FCP Conference, Atlanta, Ga. (Oct. 3-9, 1977).
- 44. Virginia Dept. of Hwys. and Transp., Plans for Rte. 603 over Parting Creek, Richmond, Va. (Feb. 1975).
- 45. Weyerhaeuser Bridge Deck Attachments, Weyerhaeuser Company, Tacoma, Wash.
- HALE, C. Y., "Field Test of a 40-ft. Span Two-Lane Weyerhaeuser Panelized Wood Bridge." Weyerhaeuser Company (May 1975).

- American Institute of Timber Construction, "Glulam Bridge Systems—Plans and Details" (1975).
- Virginia Dept. of Hwys. and Transp., "Plans for Glulam Bridge over Pohick Creek, Fairfax County, Virginia" (1975).
- Federal Highway Administration, "Standard Plans for Highway Bridges." Vol. 3, *Timber Bridges*, Washington, D.C. (Jan. 1979).
- 50. American Plywood Association, "Heavy-Duty Plywood Deck Coating." Tacoma, Wash. (1975).
- THOMPSON, P., "County's Precast Bridges Aid Roads and Wheat Markets." Rural and Urban Roads (Sept. 1976).
- IMEL, K. D., "The Bridge Program for Rural Oklahoma." FCP Conference, Atlanta, Ga. (Oct. 3-6, 1977).
- 53. "Short Span Formula Cuts Costs." Engineering News-Record (June 12, 1969) p. 23.
- 54. "Ardrossan Bridge Employs Precast, Prestressed Components." Civil Engineering (Feb. 1968) p. 48.
- JACQUES, F. J., "Study of Long-Span Prestressed Concrete Bridge Girders." Prestressed Concrete Institute, Vol. 16, No. 2, pp. 24-42 (Mar.-Apr. 1971).
- 56. CASAD, D. D., and BIRKELAND, H. W., "Bridge Features Precast Girders and Struts." *Civil Engineering*, Vol. 40, No. 7, pp. 42-44 (July 1970).
- 57. HILTON, M. H., "A Field Installation Using Prestressed Panel Subdecks." Virginia Highway and Transportation Research Council (Dec. 1978).
- HILTON, M. H., "An Experience Survey on the Use of Permanent Steel Bridge Deck Forms." Virginia Highway and Transportation Research Council (Oct. 1975).
- 59. "State of the Art: Permanent Bridge Deck Forms." Transportation Research Board Circular 181 (Sept. 1976).
- 60. Virginia Dept. of Hwys. and Transp., "Precast Concrete Parapet Details." (1974).
- 61. Federal Highway Administration, "Upgrading Safety Performance in Retrofitting Traffic Railing Systems." *Report No. FHWA-RD-77-40* (June 1976).
- Federal Highway Administration, "Review of the Design and Construction of Long Span, Corrugated-Metal Buried Conduits." Report No. FHWA-RD-77-131 (Aug. 1977).
- 63. "The Reinforced Concrete Arched Bridge—BEBO System." BEBO-International Heierli and Company, Zurich, Switzerland.
- 64. "Precast Concrete Arch Bridge Saves Minnesota Town 17%." Civ. Eng. (Nov. 1981) pp. 26.
- 65. "Armco Multi-Plate." Catalog MP-1676, Armco Steel Corporation, Middletown, Ohio (1976).

- 66. "Corrugated Steel Pipe." National Corrugated Steel Pipe Association, Chicago, Ill.
- 67. "Design Data." American Concrete Pipe Association, Vienna, Va.
- 68. "Aluminum Storm Sewers." Kaiser Aluminum Inc., Form No. HP-103, Edition 2 (1977).
- FADL, A. I., GAMBLE, W. L., and MOHRAZ, B., "Tests of a Precast Posttensioned Composite Bridge Girder Having Two Spans of 124 Feet." Structural Research Series No. 439, University of Illinois, Urbana, Ill. (Apr. 1977).
- 70. Prestressed Concrete Inst. (Jan.-Feb. 1979) pp. 62.
- 71. "Long Key Bridge." Figg and Muller Engineers, Inc., Tallahassee, Fla.
- 72. "Bridge Report." Posttensioning Institute.
- 73. "Precast Segmental Box Girder Bridge Manual." Posttensioning Institute and Prestressed Concrete Institute, Chicago, Ill. (1978).

SELECTED BIBLIOGRAPHY

- GangaRao, H. V. S., "Conceptual Substructural Systems for Short Span Bridges." *Transportation Engineering Journal* (Jan. 1978).
- Johnson, J. R., "A. H. Bridge Technical Handbook." Thomas Storey (Engineers) LTD., London (Sept. 1970).
- McDonald, J. E., and Liu, T. C., "Precast Concrete Elements for Structures in Selected Theater of Operations," U.S. Army Engineering Waterways Experiment Station, Vicksburg, Miss. (Feb. 1978).
- North, M. T., "A Literature Survey on the Prefabrication of Short Span Bridges." Virginia Highway and Transportation Research Council, Charlottesville, Va. (Aug. 1979).
- Sanden, E. J., "Some Developments in Precast and Prestressed Concrete Bridges in Western Canada." AASHO Committee on Bridges and Structures (Oct. 17, 1967).
- Standard Specifications for Highway Bridges, 12th edition. The American Association of State Highway and Transportation Officials (1977).
- Strenge, F. A., "Wood Bridges for Today and Tomorrow." Public Works (Mar. 1971) pp. 84-85.
- Tritt, B., "County Builds New Concrete Bridges in Spare Time." Rural and Urban Roads (Feb. 1967) pp. 42-44, 48, 71-72.
- U.S. Department of the Interior, "Plans for Glulam Bridge on Yorktown Battlefield Road, York County, Virginia." National Park Service (May 1974).
- Willis, S. K., "Standard Bridges Save County Dollars." Better Roads (Jan. 1973) pp. 16-21.
- Zuurbier, G. W., "Testing of a Steel Deck Bridge." Highway Research Record 253 (1968) pp. 21-34.

APPENDIX B

SUMMARY OF RESPONSE TO QUESTIONNAIRE

QUESTIONNAIRE on

Prefabricated Bridge Elements and Systems

- 1) Transportation Department 36
- 2) Name of individual completing questionnaire
- 3) Position of individual
- 4) Telephone number
- 5) How many bridges are under your jurisdiction? 228, 677

For Questions 6 to 16, answers in terms of numbers of bridges are requested but approximate percentages in terms of total number of bridges or total deck surface area may be used if numbers are not known.

1, 197

6) How many bridges contain prefabricated components? 34,983

7) How many bridges are completely prefabricated?

For questions 8 to 23, use the spaces g), h), i), and j) to note other types of prefabricated bridges that are frequently used.

8) How many bridges contain the indicated type of prefabricated element?

Type of Element	Number of Bridges		
a) Precast concrete slab span (Fig. 1)	3,002		
b) Precast box beam (Fig. 2)	5.948		
c) Prestressed I-beam (Fig. 8)	18.299		
d) Precast deck panel (Fig. 16)	8		
e) Permanent bridge-deck form (Fig. 35 & 37)	2,628		
f) Precast parapet (Fig. 38)	331		
g) Double-tee and channel	4.482		
h) Other	97		

i) j)

9) How were the prefabricated elements noted in Question 8 used?

		(Percent)		
	To Provide a	To Widen	To Replace	
Element	New Bridge	a Bridge	a Bridge	Other
a) Slab span	78	41	70	4
b) Box beam	92	64	72	0
c) I-beam	100	56	74	0
d) Deck panel	17	0	33	50
e) Deck form	85	27	42	8
f) Parapet	80	20	40	30
g) Double-ter & channel	78	11	67	. 0
h) Other	86	29	43	21
i)				

j)

10) When were the elements used and what use do you anticipate for the next decade?

	(Percent)	1965 through	1975 through	1985 through
Element	Before 1965	1974	1984	1994
a) Slab span	56	74	74	67
b) Box beam	56	80	88	72
c) I-beam	67	97	91	82
d) Deck panel	0	0	86	100
e) Deck for m	14	36	91	73
f) Parapet	0	11	89	67
B) Double-tee & channel	11	56	100	78
h) Other	50	36	79	36
i)				_
j)				

11) Where were the elements used?

Where were the el	ements used	1?	(Percer	(+)			
	Interstate		Primary		Secondary		
- Flement	High Volume Traffic	Low or Medium Volume Traffic	High Volume Traffic	Low or Medium Volume Traffic	High Volume Traffic	Low or Medium Volume Traffic	Other
a) Slab span b) Box beam c) I-beam d) Deck panel e) Deck form f) Parapet g) Double-tec \$ch. h) Other i)	27 50 72 25 60 63 38 42	23 36 66 05 38 25 33	42 59 72 25 65 13 50	65 64 88 50 85 25 75 75	42 50 50 50 25 50 17	77 86 69 65 38 88 67	
j)							

12) Why were the elements used?

) Why were the elements used?		(Percen	+)		
Element	To Accelerate Construction	To Improve Quality	To Reduce First Cost	To Reduce Life- Cycle Cost	Other
a) Slab span	70	<u> </u>	67	7	30
b) Box beam	65	15	81	8	19
c) I-beam	39	9	79	27	15
d) Deck panel	67	0	33	. 0	0
e) Deck for m	7/	14	90	14	14
f) Parapet	80	10	80	10	10
g) Double-ter & c	hannel 89	33	56	44	33
h) Other i)	60	13	80	20	47
j)					

13) How far from the bridge were the elements fabricated?

Element	<1 mile	1 to 50 miles	51 to 200 miles	>200 miles
a) Slab span	13	79	75	25
b) Box beam	10	67	90	29
c) I-beam	10	65	90	32
d) Deck panel	0	50	7 <i>5</i>	0
e) Deck form	6	65	59	47
f) Parapet	0	71	86	14
g) Double-tee Ech.	13	75	100	.50
h) Other	15	38	46	46

14) What type of forms or equipment were required?

	Special,	Versatile,	2	
	One-Time	Multiple-Project	More Versatile,	
Element	Use	Use	Multiple Purpose	Other
a) Slab span	22	72	22	0
b) Box beam	11	84	26	0
c) I-beam	4	<i>в</i> г	30	0
d) Deck panel	67	0	33	0
e) Deck for m	23	69	3 <i>8</i>	0
f) Parapet	0	100	17	0
g) Double-tre & channel	0	75	25	0
h) Other	38	75	13	13

15) What type of labor was used for the fabrication of the elements?

Element	Precast Concrete Producer	Steel Fabricator	Contractor	State or Local Crews	Other
a) Slab span	92	<u> </u>	24	12	0
b) Box beam	100	o	13	4	0
c) I-beam	100	0	9	ò	Ó
d) Deck panel	100	0	17	0	0
e) Deck for m	<i>55</i>	<i>5</i> 9	5	0	ō
f) Parapet	100	· 0	13	0	ō
g) Double-tee f ch.	100	0	11	0	0
h) Other	64	7	21	0	14
i)					•
j)					

(Percent)

16) What type of labor was used for the installation of the elements?

Element	Precast Concrete Producer	Steel Fabricator	Contractor	State or Local Crews	Other
a) Slab span	30	0	96	26	ò
b) Box beam	33	5	95	24	0
c) I-beam	23	0	97	3	0
d) Deck panel	O .	0	100	0	6
e) Deck for m	10	10	100	. 5	ō
f) Parapet	13	0	100	13	õ
g) Double-tee & c	h. 50	0	88	38	~ ~
h) Other	23	0	92	0	ő

17) How were the elements transported from the plant to the site?

g) Double-tee & ch. h) Other i) j)

Element		Descript	ion of Transportat	ion	
······	Truck	Rail	Barge	Other	
a) Slab span	96	4	8	4	
b) Box beam	95	9	5	5	
c) I-beam	94	14	9	3	
d) Deck panel	83	0	17	ō	
e) Deck for m	95	10	5	5	
f) Parapet	100	13	13	ō	
g) Double-tee & ch.	100	0	õ	õ	
h) Other	92	8	23	8	

18) Who does the maintenance and what type of maintenance is required for the elements?

		(rer	(ent)					
Element	Type of Labor		•	Туре о				
	Stat Force	Contract	None	Patch	Overlay	Joint	GANection	Other
a) Slab span	95	20	40	25	15	15	5	20
b) Box beam	94	22	62	14	10	5	5	24
c) Ibeam	95	18	7/	14.	4	7	0	21
d) Deck panel	83	33	60	20	20	ò	0	Ö
e) Deck form	92	17	60	13	7	0	0	7
f) Parapet	86	29	80	0	0	0	20	ò
g) Double-the & cl	. 100	20	88	13	0	13	0	13
h) Other	63	50	43	14	14	14	29	14
i)							-	
j)								

19) What is the cost in dollars per ft^2 of deck surface for the elements?

		Life-Cycle	Annual	
Element	<u>First Cost</u>	Cost	Maintenance Cost	Other
a) Slab span	\$ 26.11	26.11	_	. –
b) Box beam	25.64	-	0	-
c) I-bea m	21.11	21.81	0	-
d) Deck panel	19.34	-	-	-
e) Deck form	3.00	-	-	-
f) Parapet	2.67	-	-	-
g) Double-tee & ch.	19.30	19.30	-	-
h) Other	23.40	-	· · O	-
i)				
j) .				

20) What is the cost in dollars per ft² of deck surface for the most commonly used alternative to the elements?

Element	Alternative	First Cost	Life-Cycle Cost	Annual Maintenance Cost
a) Slab span	S.B. CIP Deck	\$ 25.02	-	-
b) Box beam	S.B., CIP Deck	29.61	-	-
c) I-beam	S.B., CIP Deck	24.87	-	-
d) Deck panel	CIP Concrete	17.89	-	-
e) Deck for m	CIP Concrete	3.50	-	-
f) Parapet	CIP Concrete	2.54	-	· -
g) Double-tee & channel	S.B., CIP Deck	27. 27	+	-
h)	,			
i)				
j)				

21) What is the lane-closure time in days per ft of lane required for the installation of elements and alternatives noted in Question 20?

Element	Lane Closure Time	Alternative Lane Closure Time
a) Slab span b) Box beam c) I-beam d) Deck panel e) Deck form f) Parapet g) Double-tec & ch. h) Other	17 to 100% of alternation 17 to 100% of alternation Same because CIP deck Same because CIP deck Footen than CIP concre	ive tive required required ete
i) j)	·	

22) What problems have been eliminated so that the elements have been used more frequently?

Element	Problem						Solution			
	None	quality	FirstGst	Experience	Std.	Other				
a) Slab span	36	21	7	7	7	21	(See	**+)		
b) Box beam	30	20	20	0	10	20	`	"		
c) I-beam	33	27	13	7	7	20	**	"		
d) Deck panel	0	0	50	50	0	0		4		
e) Deck form	33	33	11	11	11	0	*	4		
f) Parapet	٥	0	33	67	33	0		•		
g) Double-tee/ch.	40	20	20	20	0	0	••	**		
h)										
i)										
j)										

23) What problems have continued such that the elements have not been used extensively?

Element	Unresolved Problems					
	First Cost	None	Length/Weight	Detiionation / Corrosion	Supply	Connections
a) Slab span	50	20	10	15	10	5
b) Box beam	47	21	11	16	η	0
c) I-beam	43	35	17	0	9	۵
d) Deck panel	40	20	20	0	0	0
e) Deck for m	38	38	0	0	8	0
f) Parapet	17	17	0	17	õ	83
g) Double - teef ch. h)	40	40	0	20	0	0
i)						

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