

**Project No. 5-19**

**ANALYSIS OF SAFETY EFFECTS FOR THE  
PRESENCE OF ROADWAY LIGHTING**

FINAL REPORT

Prepared for  
National Cooperative Highway Research Program  
Transportation Research Board  
of  
The National Academies

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June 2009

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The results should not be considered sufficient to change the existing recommendations regarding the accident modification factors that should be used when considering the addition or removal of roadway lighting systems.

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## **ABSTRACT**

This report includes a summary of a statistical analysis to evaluate the association between the presence of fixed roadway lighting and crashes at intersections, interchanges, and along freeway segments. Electronic roadway inventory data were appended to crash and lighting presence data from several state transportation agencies. The presence of roadway lighting, geometric design, and traffic control features were included in statistical models of nighttime and daytime crash frequency. Night-day crash ratios from negative binomial regression and log-linear models were compared to night-day crash ratios computed only from crash data. The results indicate that the night-day crash ratios are lower at intersections with fixed roadway lighting when compared to intersections without lighting, when controlling for various roadway and traffic control features present at intersections. When computing the night-day ratios at interchanges and along freeway segments, it could not be concluded in the present study that the presence of fixed roadway lighting is associated with a statistically significant reduction in the night-day crash ratio.

## **1. BACKGROUND**

When making cost-effective decisions regarding the installation of roadway lighting at intersections, interchanges and on roadway segments, an important consideration for transportation agencies is the expected safety benefit (i.e., reduction in crash frequency and severity) that results from the lighting system. Reductions in crash frequency and severity coincide with economic savings that may or may not outweigh the costs of lighting installation and maintenance.

The objective of the safety analysis in the present report was to estimate the safety effects of roadway lighting at intersections, interchanges and roadway segments by examining expected crash frequencies, severities and night-to-day crash ratios. The literature review for NCHRP Project 5-19 identified other studies with similar goals (see Rea et al., 2009). Findings were mixed; a major shortcoming in previous research was lack of consideration of geometric and traffic control variables potentially associated with crash frequencies and severities. Without control of site-specific geometric design or traffic control variables, safety benefits associated with fixed roadway illumination systems may be over- or underestimated. Addressing this limitation was an important consideration influencing the methodology of this study outlined below.

## 2. METHODOLOGY

Several alternative data analysis techniques were used to evaluate the safety benefit of roadway lighting at intersections, interchanges and freeway segments. These methods included:

- Computation of night-to-day crash ratios;
- Estimation of negative binomial regression models of annual nighttime and daytime crash frequency;
- Estimation of log-linear models of night-to-day crash ratios;
- Estimation of negative binomial regression models of annual nighttime and daytime crash frequency with an instrumental variable for roadway lighting; and
- Computation of crash severity distributions.

While an observational before-after study was considered in the present study, such an analysis method was not used either because a record of installation dates were not readily available for a large sample of locations included in the statistical analysis, or because an assessment of several electronic roadway inventory databases indicated that roadway lighting was not the sole treatment applied to a location included in the study. In the latter, the safety effect of fixed roadway lighting would be difficult to isolate from the effects of other treatments made at the same site.

It is important to note that the methodology used in the present study was based on comparisons of various roadway types with and without fixed roadway illumination systems. While it was desirable to obtain lighting design data (e.g., uniformity, spacing, and luminance), state transportation agencies do not routinely collect this information or do not archive it in electronic records that can be linked to electronic roadway inventory and crash data. As such, a complementary analytical analysis was performed in NCHRP Project 5-19 as a mechanism to address this issue. In the analytical analysis, various lighting quality data were included in computer simulation models to evaluate the effect of lighting design on relative visual performance.

### 2.1 Night-to-Day Crash Ratios

Computing night-to-day crash ratios is historically the most common analytical method used to evaluate the safety effects of roadway lighting. Observed crash data, segregated by time of day are used to compute the ratios. Comparisons can then be made between night-to-day ratios of a specific roadway type with and without roadway lighting. For example, the percent difference in night-to-day ratio between a lighted and unlighted roadway can be expressed as:

$$\frac{\left(\frac{N}{D}\right)_w - \left(\frac{N}{D}\right)_{wo}}{\left(\frac{N}{D}\right)_{wo}} \quad (1)$$

where:  $N$  = number of nighttime crashes, aggregated over a defined time period and roadway type;  
 $D$  = number of daytime crashes, aggregated over a defined time period and roadway type;  
 $w$  = subscript to denote the presence of fixed roadway lighting on the respective roadway type;  
 $w_0$  = subscript to denote the absence of fixed roadway lighting on the respective roadway type.

A negative value resulting from equation (1) indicates that night-to-day ratios are lower on roadways with fixed roadway lighting compared to those without lighting.

## 2.2 Negative Binomial Regression Models of Annual Nighttime and Daytime Crash Frequency

The second analysis method consisted of estimating negative binomial regression models of annual nighttime and daytime crash frequency. Models were estimated for three roadway types: intersections, interchanges and freeway segments. A negative binomial regression model relates a crash count as a left-hand-side (LHS) variable to a number of right-hand-side (RHS) variables, coefficients that quantify magnitudes of relationships between LHS and RHS variables and a disturbance term. For this study, the negative binomial regression model was assumed to take the following form:

$$\ln(\lambda) = \omega + X\beta + L\theta + \varepsilon \quad (2)$$

where:  $\lambda$  = expected number of crashes per year at an intersection, interchange or roadway segment;  
 $\omega$  =  $n \times 1$  intercept matrix (all rows are constant)  
 $X$  =  $n \times k$  matrix of variables influencing  $\lambda$  (e.g., roadway and roadside geometry, type of traffic control, etc.);  
 $\beta$  =  $k \times 1$  matrix of parameters quantifying the relationship between  $X$  and  $\lambda$  ;  
 $L$  = a binary (dummy) variable indicating the presence of roadway lighting;  
 $\theta$  = parameter quantifying the relationship between roadway lighting presence and  $\lambda$  ;  
 $\varepsilon$  =  $n \times 1$  disturbance matrix (the distribution of  $\varepsilon$  is assumed to be gamma);  
 $k$  = number of variables in  $X$  ; and  
 $n$  = number of observations.

The mean-variance relationship for the negative binomial distribution is:

$$Var(y_i) = E(y_i)[1 + \alpha E(y_i)] \quad (3)$$

where:  $Var(y_i)$  = variance of observed crashes occurring at location  $i$ ;

$E(y_i)$  = expected crash frequency at location  $i$ ;

$\alpha$  = overdispersion parameter.

The regression parameters (i.e.  $\beta$  and  $\theta$ ) were estimated using the method of maximum likelihood.

The appropriateness of the negative binomial regression model is based on the significance of the overdispersion parameter ( $\alpha$ ). When  $\alpha$  is not significantly different from zero, the negative binomial model reduces to a Poisson model. Previous safety research (e.g., Shankar et al., 1995; Poch and Mannering, 1996; Torbic et al., 2007) has shown that  $\alpha$  is nearly always greater than zero (i.e. the variance of crash counts is nearly always greater than the mean).

Regression models were estimated for intersections, interchanges and roadway segments using annual day and night crash frequency as the left hand side variables. The parameter estimates for the presence of roadway lighting ( $\hat{\theta}$ ) were then used to compute the expected percent difference in the night-to-day crash ratios between lighted and unlighted roadways. This computation is as follows:

$$\frac{\exp(\hat{\theta}_N)}{\exp(\hat{\theta}_D)} - 1 \quad (4)$$

where:  $\hat{\theta}_N$  = estimated regression parameter associated with the presence of roadway lighting in the nighttime crash frequency model; and

$\hat{\theta}_D$  = estimated regression parameter associated with the presence of roadway lighting in the daytime crash frequency model;

A negative value resulting from equation (4) indicates that the night-to-day ratios estimated by the regression models are lower on roadways with fixed roadway lighting compared to those without lighting. The advantage of this approach over the approach in the previous section is consideration of variables other than the presence of lighting that may also be associated with the night-to-day crash ratio (e.g. traffic volume, geometrics, etc.).

### 2.3 Log-Linear Models of Night-to-Day Crash Ratios

The third analytical approach used in this study involved computing the observed annual night-to-day crash ratio and modeling the logarithm of this ratio using ordinary least squares (OLS) regression. The objective of this approach was primarily to provide a point of comparison to the negative binomial regression results. OLS is the most commonly used estimator in linear regression modeling and is often used for this purpose. The general form of the log-linear regression model in the present study was:

$$\ln\left(\frac{N}{D}\right) = \omega + X\beta + L\theta + \varepsilon \quad (5)$$

where:  $N$  = number of nighttime crashes, aggregated over a defined time period and roadway type;  
 $D$  = number of daytime crashes, aggregated over a defined time period and roadway type;  
 $\omega$  =  $n \times 1$  intercept matrix (all rows are constant)  
 $X$  =  $n \times k$  matrix of variables influencing  $\ln\left(\frac{N}{D}\right)$  (e.g., roadway and roadside geometry, type of traffic control, etc.);  
 $\beta$  =  $k \times 1$  matrix of parameters quantifying the relationship between  $X$  and  $\lambda$  ;  
 $L$  = a binary (dummy) variable indicating the presence of roadway lighting;  
 $\theta$  = parameter quantifying the relationship between roadway lighting presence and  $\ln\left(\frac{N}{D}\right)$ ;  
 $\varepsilon$  =  $n \times 1$  disturbance matrix (the distribution of  $\varepsilon$  is assumed to be normal);  
 $k$  = number of variables in  $X$  ; and  
 $n$  = number of observations.

The following four cases were encountered when modeling the logarithm of night-to-day crash ratios:

- Case I: Night crash frequency  $> 0$ ; day crash frequency  $> 0$ ;
- Case II: Night crash frequency = 0; day crash frequency  $> 0$ ;
- Case III: Night crash frequency = 0; day crash frequency = 0;
- Case IV: Night crash frequency  $> 0$ ; day crash frequency = 0.

In case I, the night-to-day crash ratios were computed and included in the dataset used to estimate the model as all ratios are greater than zero. In cases II, III and IV, the night-to-day crash ratios are either zero or indeterminate. These observations were not included in the sample of data. The major assumption of this approach is that cases II, III and IV are randomly-distributed in the sample of data. If this assumption is violated, the problem becomes one of selectivity bias; the result being biased and inconsistent parameter estimates. Heckman (1979) developed a method to account for sample selection bias for normally-distributed, continuous data; however, application of the method was not pursued in the present study because of the sensitivity of the model parameters to the assumption of normality (Greene, 2008).



## **2.4 Estimation of Negative Binomial Regression Models of Annual Nighttime and Daytime Crash Frequency with an Instrumental Variable for Roadway Lighting**

In the single-equation negative binomial model illustrated in equation (2), the variables in  $X$  as well as  $L$  were assumed to be exogenous, or independent (i.e., their values vary independently of other variables during a specified time period). However, a review of roadway lighting warrants showed that the likelihood that roadway lighting would be installed on a roadway segment, intersection or interchange (i.e.,  $L = 1$ ) may depend on variables including traffic volumes, geometrics, presence of a traffic signal and crash experience. As such, an instrumental variable approach was considered in this research to address this issue. Both day and night crash frequency models with instrumental variables for roadway lighting were estimated using data for Minnesota intersections. Results of the instrumental variable models were uncertain (large changes in parameter magnitude or inconsistent change in signs for various subsets of the Minnesota data) when compared to negative binomial models with the actual lighting dummy variable. The decision not to continue model estimations with lighting instruments was made for several reasons as follows:

1. Intuitively, the relationship between the presence of roadway lighting and crash frequency is not truly endogenous. Although lighting may be installed at locations with a high number of crashes, the lighting installation is not removed if the crash frequency decreases.
2. A right-hand-side instrument that is not highly correlated with the variable for which it is an instrument (i.e., a “weak” instrument) may result in parameter bias that is larger than that introduced by endogeneity. For many subsets of the Minnesota intersection data, the lighting instruments were weak.
3. The econometrics literature regarding the use of instrumental variables in non-linear models is scarce. Although some methods have been proposed (e.g., Windmeijer and Santos Silva, 1997), general consensus on their use does not exist.

## **2.5 Computation of Crash Severity Distributions**

In addition to the crash frequency analyses described above, crash severity distributions were computed for all roadway types. The severity distributions were computed based on the KABCO scale as follows:

- Fatality (K);
- Disabling injury (A);
- Evident injury (B);
- Possible injury (C);
- No evident injury or property-damage only (PDO).

Using Minnesota intersection and interchange data, California intersection data and Washington State freeway segment data, severity distributions were developed and stratified by daytime and nighttime crashes with and without fixed roadway lighting. The proportion of crashes occurring within each severity level was compared.

### 3. DATABASE DEVELOPMENT

This section is organized into three subsections. The first describes data acquisition and database development for California and Minnesota intersection analyses. In both instances, the Highway Safety Information System (HSIS) maintained by the Federal Highway Administration (FHWA) was used to acquire roadway inventory and crash data files. An indicator for roadway lighting presence was included in the roadway files from both of these states. The second subsection describes data acquisition and database development for Minnesota interchange analysis. Again, HSIS data files were used with a roadway lighting presence indicator coded in the roadway inventory database. The third subsection includes a summary of the process used to acquire roadway inventory, lighting presence and crash data files from Washington State, Oregon, and Virginia. These data were used to estimate models of nighttime and daytime crash frequency along freeways (Interstates) with and without continuous lighting.

#### 3.1 Intersections

##### 3.1.1 California

In order to develop the data files for analysis of California intersections, HSIS data were acquired from the FHWA (HSIS, 2000). These files included crash and roadway inventory and intersection data for the years 1999 through 2002, inclusive. Each observation in the database consists of one intersection for one year. A total of 15,514 intersections were included in the analysis, representing a total of 62,056 annual intersection-level observations. All crash types were included in the analysis. During the analysis period, 46,424 crashes occurred. 8,494 intersection-level observations (13.7 percent) had signal control while the remainder operated under stop control. It was not possible to differentiate between two- and all-way stop-controlled intersections. Three intersection configurations could be distinguished in the California database: four-leg, tee, and wye or offset. Approximately 33.1 percent of the observations were for four-leg intersections; 57.7 percent were tee intersections; and the remaining 9.2 percent of the observations were wye or offset intersections. Although the HSIS roadway inventory data files contained roadway functional classification codes, the rural-urban designation was missing in 64 percent of the cases. As such, the analysis of California data did not differentiate between urban and rural intersection locations. A variety of roadway geometric design data were available for inclusion in the crash frequency models. Table 1 provides definitions and descriptive statistics of variables included in the database.

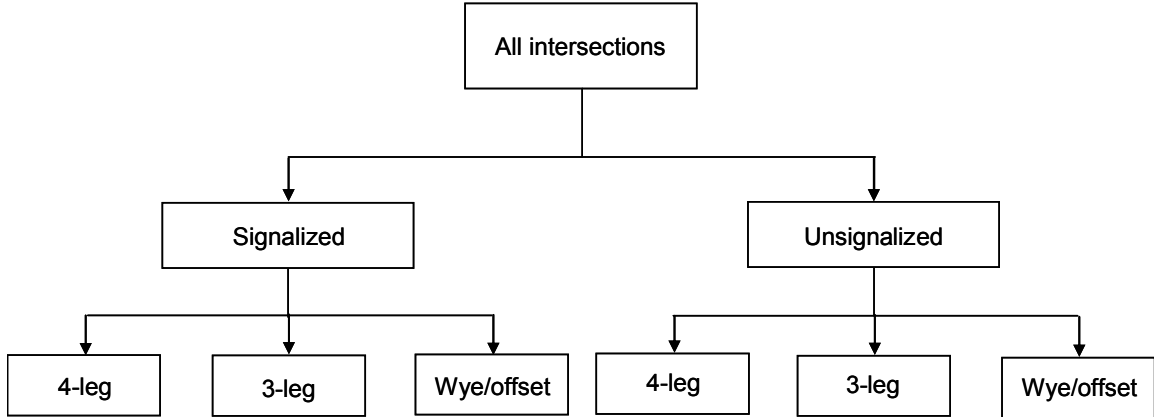
An analysis taxonomy for California intersections is illustrated in Figure 1. The higher-order models (e.g., all intersections) contained indicator variables for traffic control type (signalized vs. unsignalized) and intersection form (4-leg and 3-leg vs. wye/offset). The methodology progressed through the taxonomy as follows:

- Level 1: all intersections
- Level 2: all signalized intersections; all unsignalized intersections (2 models)
- Level 3: all signalized 4-leg intersections; all signalized 3-leg/tee intersections; all signalized wye/offset intersections; all unsignalized 4-leg intersections; all

unsignalized 3-leg/tee intersections; and, all unsignalized wye/offset intersections (6 models).

**Table 1 Variable Definitions and Descriptive Statistics for the California Intersection Database**

<b>Variable Description</b>	<b>Minimum</b>	<b>Maximum</b>	<b>Mean</b>	<b>Standard Deviation</b>
Night crash frequency (per year)	0	10	0.187	0.581
Day crash frequency (per year)	0	21	0.561	1.241
Night-day crsh ratio	0	6	0.243	0.487
Log major road average daily traffic (veh/day)	1.792	11.264	8.587	1.523
Log minor road average daily traffic (veh/day)	0	11.252	5.638	1.842
Four-leg intersection type indicator (1 = four-leg intersection; 0 otherwise)	0	1	0.331	0.470
Tee intersection type indicator (1 = tee intersection; 0 otherwise)	0	1	0.577	0.494
Wye or offset intersection type indicator (1 = wye or offset intersection; 0 otherwise)	0	1	0.092	0.289
Traffic control indicator (1 = signal; 0 = stop-control)	0	1	0.137	0.344
Lighting indicator (1 = present; 0 = not present)	0	1	0.512	0.499
Left-turn channelization on major road indicator (1 = present; 0 otherwise)	0	1	0.417	0.493
Left-turn restriction indicator (1 = left-turns restricted; 0 otherwise)	0	1	0.039	0.194
Right-turn channelization on major road indicator (1 = present; 0 otherwise)	0	1	0.099	0.288
Median on major road indicator (1 = present; 0 otherwise)	0	1	0.373	0.484
Major road number of lanes indicator (1 = major road has two lanes; 0 otherwise)	0	1	0.612	0.487
Major road number of lanes indicator (1 = major road has three or four lanes; 0 otherwise)	0	1	0.326	0.469
Major road number of lanes indicator (1 = major road has five or six lanes; 0 otherwise)	0	1	0.063	0.243



**Figure 1 California Intersection Analysis Taxonomy**

### 3.1.2 Minnesota

Intersection data contained in the Minnesota HSIS roadway inventory, intersection and crash data files were merged to develop the database (Council and Williams, 2001) used for analysis of Minnesota intersections. Four years (1999 through 2002, inclusive) of crash and corresponding roadway inventory data were included. A total of 25,856 observations (or 6,464 intersections) were available for model estimation. 888 of the 6,464 intersections (13.7 percent) had signal control while the remainder operated under stop control. It was not possible to differentiate two- and all-way stop control. There were three intersection forms coded in the database: cross, tee, and skew. Approximately 49 percent of the intersections (3,181 or 6,464) were four-leg cross intersections. Nearly 40 percent (2,576 of 6,464) were three-leg tee intersections. The remaining 11 percent of the intersections were skew. There were 38,437 reported crashes at the intersections included in the analysis database.

Minnesota is a unique HSIS database in that it contains variables for lighting presence and type (i.e., full, partial, point) for at-grade intersections. Although these data were coded as full, partial or point illumination systems, a majority of the analysis used the lighting presence indicator variable. Table 2 provides a summary of Minnesota intersection data included in the analysis. Only geometric design data for the major roadway were included because of considerable missing data for the minor intersecting roadway. These data include a posted speed indicator, percent heavy vehicles, access control indicator, median indicator and right and left shoulder type indicators. More than 42 percent of the intersections contained some form of roadway lighting.

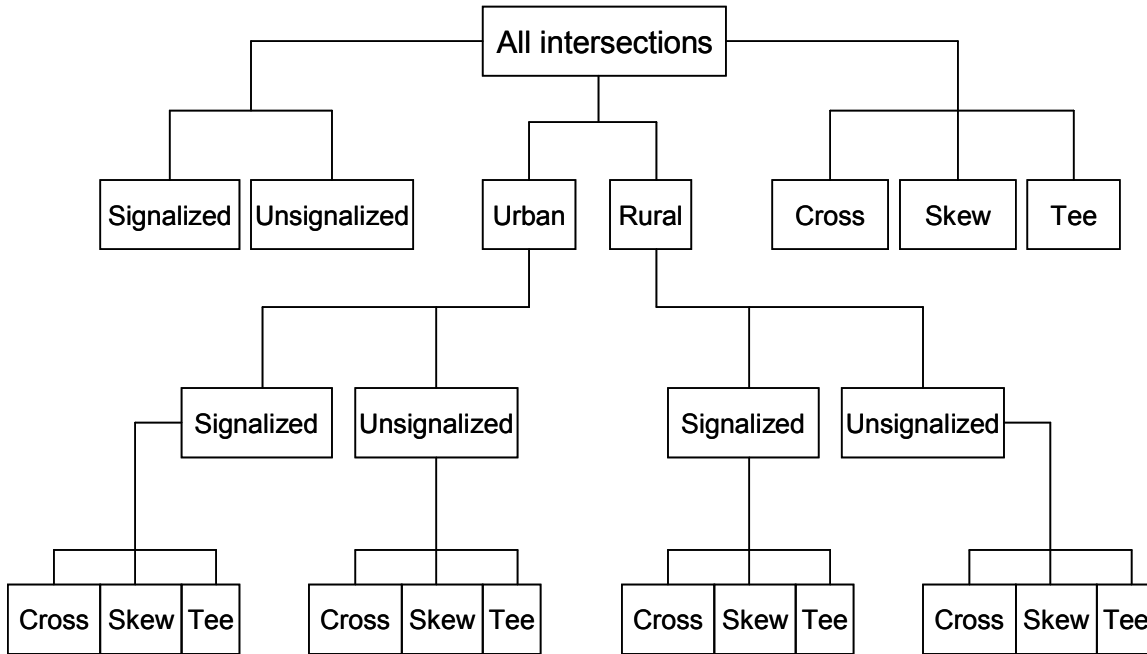
**Table 2 Descriptive Statistics of Minnesota Intersection Data**

Variable	Minimum	Maximum	Mean	Standard Deviation
Night crash frequency (per year)	0	28	0.3655	0.9687
Day crash frequency (per year)	0	55	1.1211	2.4570
Night-day crash ratio	0	5	0.1042	0.3175
Log major road average daily traffic	3.700	11.300	8.4305	1.1451
Percent heavy vehicles on major road	0	61.11	8.8880	5.1092
Log minor road average daily traffic	0	11.300	6.9392	1.7331
Area type indicator (1 = urban/suburban; 0 = rural)	0	1	0.4456	0.4970
Traffic control indicator (1 = signal; 0 = stop-control)	0	1	0.1373	0.3442
Lighting indicator (1 = present; 0 = not present)	0	1	0.4212	0.4938
Intersection type indicator (1 = skew; 0 = cross or tee)	0	1	0.1095	0.3123
Speed indicator* (1 = 50 mph or greater; 0 otherwise)	0	1	0.6731	0.4691
No access control indicator * (1 = no access; 0 = partial access control)	0	1	0.9426	0.2326
Depressed median indicator* (1 = depressed median; 0 = barrier or no median)	0	1	0.1162	0.3204
Paved left-shoulder indicator* (1 = paved shoulder; 0 = unpaved or no shoulder)	0	1	0.4577	0.4982
Paved right-shoulder indicator* (1 = paved shoulder; 0 = unpaved or no shoulder)	0	1	0.5096	0.4999
*indicates that data were used for the major intersecting roadway only				

Like California, an analysis taxonomy was developed for the Minnesota intersection files. The taxonomy is illustrated in Figure 2. Higher-order models (e.g. all intersections) contained indicator variables for traffic control type (signalized vs. unsignalized), area type (urban vs. rural) and intersection form (cross and tee vs. skew). The analysis methodology progressed through the taxonomy as follows:

- Level 1: all intersections
- Level 2: all signalized intersections; all unsignalized intersections; all urban intersections; all rural intersections; all cross intersections; all skewed intersections; and, all tee intersections (7 models)
- Level 3: all urban signalized intersections; all urban unsignalized intersections; all rural signalized intersections; all rural unsignalized intersections (4 models)
- Level 4: all urban signalized cross intersections; all urban signalized skewed intersections; all urban signalized tee intersections; all urban unsignalized cross intersections; all urban unsignalized skewed intersections; all urban unsignalized

tee intersections; all rural signalized cross intersections; all rural signalized skewed intersections; all rural signalized tee intersections; all rural unsignalized cross intersections; all rural unsignalized skewed intersections; all rural unsignalized tee intersections (12 models).



**Figure 2 Minnesota Intersection Analysis Taxonomy**

### 3.2 Interchanges

All data contained in the Minnesota HSIS roadway inventory, intersection/interchange, and crash data files were used to develop the database for analysis of Minnesota interchanges (Council and Williams, 2001). Four years (1999 through 2002, inclusive) of crash and corresponding roadway inventory data were used in the analysis. A total of 2,096 the observations (or 524 interchanges) were available for model estimation, where each observation represented an interchange for one year. Eighty percent of the interchanges were the diamond form while the remainder (i.e. trumpet, semi-direct, cloverleaf, and other) was categorized as non-diamond interchange forms. Nearly 62.1 percent of interchanges in Minnesota were located in an urban or suburban environment while the remainder was classified as rural. There were 36,536 reported crashes in proximity of interchanges included in the database. The crash analysis area was defined as those locations along the mainline through travel lanes between diverge and merge locations plus an additional 1500 feet upstream or downstream of the merge and diverge locations.

Like the intersection data in Minnesota, the interchange data contained lighting presence and type indicators. These data were coded as full, partial or point illumination systems. The lighting variables were analyzed separately and compared to no lighting, as

well as combined into a single lighting presence indicator and compared to interchanges with no lighting. Table 3 is a summary of the data included in the Minnesota interchange analysis.

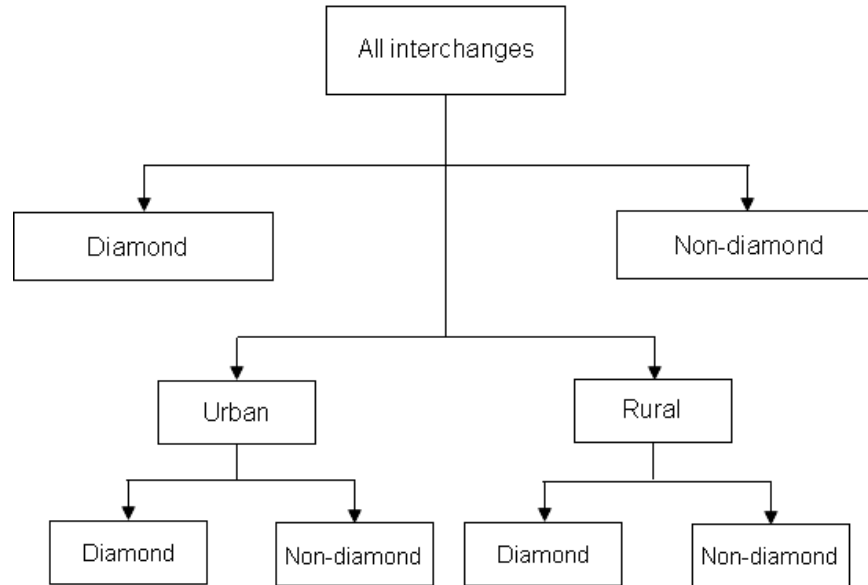
**Table 3 Descriptive Statistics of Minnesota Interchange Data**

Variable	Minimum	Maximum	Mean	Standard Deviation
Night crash frequency (per year)	0	46	5.280	6.200
Day crash frequency (per year)	0	89	12.151	15.026
Night-day crash ratio	0	6	0.590	0.633
Log total entering vehicles (vehicles/day)	4.663	12.985	9.455	1.592
Percent heavy vehicles on major road	0.610	45.804	8.769	5.868
Area type indicator (1 = urban/suburban; 0 = rural)	0	1	0.621	0.485
Interchange form indicator (1 = diamond; 0 = non-diamond)	0	1	0.798	0.402
Lighting indicator (1 = present; 0 = not present)	0	1	0.798	0.402
Posted speed limit on major road (mph)	25	70	60.406	9.249
Indicator for full-access control on major road (1 = full-access control; 0 = otherwise)	0	1	0.781	0.413
Indicator for partial-access control on major road (1 = partial access control; 0 = otherwise)	0	1	0.094	0.291
Indicator for median barrier presence on major road (1 = median barrier present; 0 = no barrier present)	0	1	0.256	0.436
Pavement surface indicator (1 = concrete pavement; 0 = asphalt pavement)	0	1	0.485	0.500
Lane width indicator for major road (1 = lane width $\geq$ 13-feet; 0 = otherwise)	0	1	0.145	0.352
Number of lanes on major road indicator (1 = Five or more lanes; 0 = otherwise)	0	1	0.250	0.433

An analysis taxonomy was developed for the Minnesota interchange files. The taxonomy is illustrated in Figure 3. Similar to the intersection models, the higher-order models (e.g., all interchanges) contained indicator variables for area type (urban vs. rural) and interchange form (diamond vs. non-diamond). The analysis methodology progressed through the taxonomy as follows:

- Level 1: all interchanges
- Level 2: all diamond interchanges; all non-diamond interchanges; all urban interchanges; all rural interchanges (4 models)
- Level 3: all urban diamond interchanges; all urban non-diamond interchanges; all rural diamond interchanges; all rural non-diamond interchanges (4 models).





**Figure 3 Minnesota Interchange Analysis Taxonomy**

### 3.3 Freeway Segments

Four freeway segment analyses were undertaken in the present study. The first two were based on Interstate roadway segments in Washington State, and the remaining two were based on roadway segments with continuous freeway lighting in Oregon and Virginia. In the first analysis using the Washington Interstate highway segment data, segments were developed based on the presence of contiguous or point segment-level lighting (i.e., interchange lighting was not considered as part of a continuously-lighted segment); however, the number of interchanges per segment were counted and included in the model specifications and these interchanges generally included either partial or full interchange lighting. A second Washington Interstate analysis was performed excluding interchange and overpass locations as well as point lighting locations. As such, this analysis included only roadway segments with through traffic volumes and therefore did not consider the merge and diverge conflicts at interchange locations, or locations underneath roadway overpasses that were not lighted. The second Washington Interstate analysis contained a subset of segments from the first Washington Interstate analysis. The Oregon and Virginia freeway segment analyses considered continuous freeway lighting as defined by the American Association of State Highway and Transportation Officials' *Roadway Lighting Design Guide* (2005). As described below, locations with continuous freeway lighting, and similar locations without lighting, were identified by the NCHRP Project 5-19 panel.

#### 3.3.1 Washington Interstates

Table 4 shows descriptive statistics for key variables in the lighting segment dataset for Washington State Interstate roadway segments. A total of 1,528 centerline miles of the

Interstate network covering Washington State was scanned using online video photologs to determine many of the variable characteristics included in the analysis. The Interstate network was scanned by direction of travel.

Because the roadway inventory data were coded by direction of travel, a lighting presence indicator was also noted based on travel direction. Fixed roadway lighting in Washington existed either in the median or along the roadside adjacent to the right shoulder location. For the purposes of the analysis, fixed roadway lighting was coded as either continuous or point. If luminaires were present within 0.025 miles of adjacent luminaires, then contiguous luminaires meeting this requirement were combined to form a lighting segment. Point lighting locations were those where a single luminaire was observed along a roadway segment, but not part of a contiguous system. The mean length of lighting segment according to the aforementioned definition was 1.40 miles. The minimum segment length was 0.01 miles, while the maximum segment length was 64.84 miles. The percent of urban segments included in the analysis database was 71 percent, while segments with no lighting constituted 49.77 percent of observations. Continuous lighting segments constituted 32.33 percent of the entire network while point lighting segments constituted 17.90 percent of the network.

The percent of lighted or unlighted segments varied by direction of travel since the Interstate network is a divided highway network. Interchange and overpass data were gathered using the online video photolog system maintained by the Washington State Department of Transportation. The count of interchanges and overpasses was derived on the basis of presence or absence in a segment. The mean number of interchanges per segment was 1.22, with a maximum of 13, while the mean number of overpasses per segment was 0.73 with a maximum of 15. Mean average daily traffic (AADT) per segment was 26,804 with a minimum of 988 vehicles per day and a maximum of 65,109 vehicles per day. Average daily traffic data were obtained in one-mile increments and weighted on the basis of segment lengths.

Using the Washington Interstate segment database, negative binomial regression models were estimated for both daytime and nighttime crashes. Additionally, the night-day crash ratio using only the crash data was also computed. Lastly, a severity distribution for freeway segment with and without fixed roadway lighting is reported, stratified by daytime and nighttime crashes.

### *3.3.2 Supplemental Washington Freeway Segment Analysis*

Revised segment models for evaluating the effect of continuous roadway lighting on crash occurrence were constructed after excluding locations with point lighting. Six models were constructed, including models combining urban and rural segments, models for urban segments only, and models for rural segments only. The effect of interchange and overpass locations on model behavior was also examined. The relative change in daytime crashes, nighttime crashes, and night-day crash ratios were computed from negative binomial regression models for segments including interchanges and overpasses, and for those without interchanges and overpasses.

**Table 4 Descriptive Statistics of Washington Freeway Segment Data**

Variable	Mean	Minimum	Maximum
Segment length in miles	1.40	0.01	64.84
Percent of segments direction of travel (increasing milepost and decreasing milepost respectively)	0.53/0.47	0	1
Percent of segments urban	0.71	0	1
Percent segments with no lighting presence	0.50	0	1
Percent segments with point lighting presence	0.18	0	1
Percent segments with continuous lighting presence	0.32	0	1
Number of interchanges in segment	1.22	0	13
Number of overpasses in segment	0.73	0	15
Average daily traffic	26,804	988	65,109
Number of vertical curves in segment	3.25	0	81
Number of horizontal curves in segment	1.82	0	57
Number of lanes in segment	2.91	1	6.83
Left shoulder width in feet	6.85	1.28	14
Right shoulder width in feet	6.64	0.18	24
Number of daytime property damage only crashes in segment	5.24	0	107
Number of daytime possible injury crashes in segment	2.28	0	55
Number of daytime evident injury crashes in segment	0.66	0	22
Number of daytime disabling injury crashes in segment	0.08	0	5
Number of daytime fatal crashes in segments	0.02	0	5
Number of nighttime property damage only crashes in segment	1.88	0	48
Number of nighttime possible injury crashes in segment	0.69	0	23
Number of nighttime evident injury crashes in segment	0.32	0	12
Number of nighttime disabling injury crashes in segment	0.05	0	2
Number of nighttime fatal crashes in segments	0.02	0	4

### 3.3.3 Oregon Freeways

To estimate the safety effects of continuous freeway lighting in Oregon, roadway inventory, lighting presence, and traffic crash data were acquired and appended from a variety of sources. Dr. Christopher Monsere from Portland State University provided an electronic database of limited-access roadway segments with and without roadway lighting from a study that was performed while he was employed by the Oregon Department of Transportation (ODOT) Traffic Engineering Services Unit (Monsere and

Grile, 2002). The database included daytime and nighttime crash frequencies, daytime and nighttime traffic volumes, and an indicator for lighting presence on the following roadways during the period 1996 through 2000 (inclusive):

- Interstates 5, 82, 84, 205, and 405;
- U.S. Route 26; and,
- Oregon State Route 217.

Because the database provided by Dr. Monsere did not include any roadway inventory data, the research team requested these data from ODOT staff. Data for the year 2008 were provided to the research team and included roadway cross-section information (number of lanes, lane width, shoulder width, median width), posted speed limit data, and area type (urban vs. rural) information. Additionally, roadway segment information (begin and end milepost and segment length) were also included in the roadway inventory datafiles provided by ODOT.

To verify that the roadway segments identified by Monsere and Grile (2002) contained continuous freeway lighting as defined by AASHTO, the ODOT video photolog system was used. Once this process was completed, the 2008 roadway segment data provided by ODOT and the data provided by Dr. Monsere were appended. The percentage of daytime and nighttime traffic estimates developed by Monsere and Grile (2002) were used in the present analysis to estimate daytime and nighttime traffic volumes. Finally, the daytime and nighttime crash frequency data provided by Dr. Monsere were appended to the roadway inventory and lighting presence data. To develop the final analysis database, ODOT's video photolog system was used to count the number of interchanges, horizontal curves, and vertical curves in each analysis segment. Roadway segments with continuous lighting were defined by the limits of the fixed illumination section.

Table 5 shows the descriptive statistics for all explanatory variables and total daytime and nighttime crashes for each roadway segment included in the analysis database. A total of 680.6 miles of the limited-access highway segments were included in the analysis database. The percentage of urban segments included in the analysis database was 46 percent – approximately 54 percent of the segments were classified as rural. Segments with lighting constituted 11 percent of the observations, while approximately 89 percent of segments did not contain continuous lighting. There were two lanes per direction 77 percent of the roadway segments in the analysis while the remainder had more than two through travel lanes per direction. Approximately 50 percent of segments in the analysis database contained a fixed longitudinal median barrier while the remainder contained an earth-divided, traversable median.

The average roadway segment length was 3.80 miles, ranging from 0.1 to 47.9 miles. The left (median) paved shoulder width in the analysis segments ranged from 0 to 20 feet, while the right (outside) paved shoulder width ranged from 2 to 19 feet. The mean width of the left and right paved shoulders was 7.98 and 7.79 feet, respectively. The average median width of the analysis segments was 50.60 ft, ranging from 0 to 106 feet. The average number of horizontal curves per segment was 4.33, ranging from 0 to 59. The number of vertical curves per segment ranged from 0 to 78. The number of interchanges in an analysis segment ranged from 0 to 17.

The average daytime average daily traffic was 32,817 vehicles per day while the average nighttime daily traffic in the analysis database was 9,292 vehicles per day. Approximately 70 percent of the analysis segments had a posted speed limit of 65 mph or higher.

The average number of daytime crashes along the analysis segments was 61, while the average number of nighttime crashes was 21. Negative binomial regression models were estimated for both daytime and nighttime crashes using the continuous and categorical data shown in Tables 1 and 2. Additionally, the night-day crash ratio was also computed using only the descriptive statistics from the analysis database.

**Table 5 Descriptive Statistics of Variables in Oregon Freeway Segment Database**

Continuous Variable	Mean	Standard deviation	Minimum	Maximum
Number of daytime crashes in segment	61	188.77	0	2,043
Number of nighttime crashes in segment	21	51.73	0	537
Left paved shoulder width (feet)	7.98	3.14	0	20
Right paved shoulder width (feet)	7.79	2.89	2	19
Average daily daytime traffic (veh/day)	32,817	28,432	6,131	116,584
Average daily nighttime traffic (veh/day)	9,292	8,572	1,669	37,700
Segment length (miles)	3.80	7.13	0.1	47.9
Number of horizontal curves in segment	4.33	8.36	0	59
Number of vertical curves in segment	8.24	14.32	0	78
Number of interchanges in segment	1.34	2.50	0	17
Median width (feet)	50.60	33.30	0	106
Categorical Variable	Definition		Proportion	
Area type	1 if the segment is in an urban area		0.46	
	0 if the segment is in a rural area (baseline)		0.54	
Lighting presence	1 if lighting is present		0.11	
	0 if lighting is not present (baseline)		0.89	
Number of lanes	1 if number of through lanes per direction = 2		0.77	
	0 if number of through lanes per direction > 2 (baseline)		0.23	
Median barrier presence	1 if median barrier is present		0.50	
	0 if no median barrier is present (baseline)		0.50	
Posted speed limit	1 if posted speed limit = 65mph		0.70	
	0 if posted speed limit < 65mph (baseline)		0.30	

### 3.3.4 Virginia Freeway Segments

Freeway segments with and without roadway lighting were identified by Virginia Department of Transportation (VDOT) staff. The roadways included in the analysis database included segments with and without continuous freeway lighting on Interstates 66, 95, 395, and 495. Electronic roadway inventory and crash data were also obtained

from VDOT staff for the segments with and without roadway lighting. In all, approximately 113 miles were included in the analysis database.

Table 6 shows descriptive statistics for the continuous and categorical variables included in the analysis dataset. All of the roadway segments included in the analysis database were in an urban area. Segments with continuous freeway lighting constituted 15.5 percent of the observations. Approximately 19.8 percent of the roadway segments had two through travel lanes per direction, while 37.0 percent of the segments had three through lanes per direction, and 43.3 percent of the segments had four or more through travel lanes per direction. Approximately 65.9 percent of the roadway segments in the analysis database contained a longitudinal median barrier.

The average roadway segment length was 0.33 miles, ranging from 0.01 to 2.45 miles. The mean width of the left shoulder was 2.35 feet, while the mean width of the right shoulder was 9.34 feet. The left shoulder width ranged from 0 to 12 feet, while the right shoulder ranged from 0 to 14 feet. The average median width was 48.11 feet, ranging from 2 to 285.5 feet. Interchange locations within each roadway segment were identified by VDOT staff. The number of interchanges per analysis segment ranged from 0 to 1.

The mean average daily traffic was 68,519 vehicles per day, ranging from 18,945 to 133,528 vehicles per day. The posted speed limit ranged from 45 to 65 mph; however, posted speed limit data were missing for approximately one-half of the analysis segments. The average percentage of truck traffic was 4.56 percent, ranging from 0.29 to 10.19 percent.

The average number of daytime crashes in the analysis database was 6.0, ranging from 0 to 100. Among all the daytime crashes, 65.9 percent were property-damage-only crashes, 34.0 percent were injury crashes, and 0.2 percent was fatal crashes. The average number of nighttime crashes in the analysis database was 2.0, ranging from 0 to 29 per segment. Among all nighttime crashes, 65.2 percent were property-damage-only crashes, 34.2 percent were injury crashes, and 0.6 percent was fatal crashes.

Using the Virginia Interstate segment database, negative binomial regression models were estimated for both daytime and nighttime crashes. Additionally, the night-day crash ratio using only the observed crash data was also computed.

**Table 6 Descriptive Statistics of Variables in Virginia Freeway Segment Database**

Continuous Variable	Mean	Standard Deviation	Minimum	Maximum
Segment length (miles)	0.33	0.39	0.01	2.45
Number of interchanges in segment	0.18	0.38	0	1
Average daily traffic (veh/day)	68,519	24418.23	18945	133,528
Number of lanes per direction	3.29	0.85	2	6
Travel way surface width (feet)	39.43	10.20	22	72
Right shoulder width (feet)	9.34	3.35	0	14
Left shoulder width (feet)	2.35	3.65	0	12
Percentage of truck traffic	4.56	2.84	0.29	10.19
Speed limit (mph)	57.48	3.91	45	65
Median width (feet)	48.11	49.41	2	285.5
Daytime crash count	6.17	8.97	0	100
Nighttime crash count	2.47	3.43	0	29
Daytime property-damage-only crash count	4.07	6.00	0	61
Daytime injury crash count	2.10	3.35	0	39
Daytime fatal crash count	0.01	0.11	0	1
Nighttime property-damage-only crash count	1.61	2.37	0	18
Nighttime injury crash count	0.84	1.38	0	12
Nighttime fatal crash count	0.02	0.12	0	1
Categorical Variable	Definition		Proportion	
Lighting presence	1: if lighting is present		0.79	
	0: if lighting is not present (baseline)		0.21	
Median barrier	1: if median barrier is present		0.66	
	0: if no median barrier is present (baseline)		0.34	
Two lanes indicator	1: if number of through lanes per direction = 2		0.20	
	0: otherwise		0.80	
Three lanes indicator	1: if number of through lanes per direction = 3		0.37	
	0: otherwise		0.63	
Four or more lanes indicator (baseline)	1: if number of through lanes per direction $\geq 4$		0.43	
	0: otherwise		0.57	

## 4. ANALYSIS RESULTS

This section is divided into two subsections. The first contains results of the crash frequency modeling efforts. Included are the higher-order daytime and nighttime crash frequency models estimated using the Minnesota and California intersection databases, the Minnesota interchange database and the Oregon, Virginia, and Washington State freeway segment database. The higher order models are those shown at the top of each analysis taxonomy (see Figures 1, 2, and 3). Estimation results of the lower-order nighttime and daytime crash frequency models results are also briefly summarized with statistical output contained in Appendixes A, B, and C for the California intersection, Minnesota intersection, and Minnesota interchanges, respectively. The first subsection also includes estimation results of the log-linear models of night-to-day crash ratios for the higher-order taxonomy levels. The second subsection describes the severity analysis. Results are presented in tabular form for the Minnesota and California intersections, Minnesota interchanges and Washington State freeway segment databases.

### 4.1 Crash Frequency Models

#### 4.1.1 *Intersections*

Included in this section are night-to-day crash ratios, nighttime and daytime crash frequency negative binomial regression models, and log-linear night-day crash ratio models for the California and Minnesota intersection models. The instrumental variable model for all Minnesota intersections is also presented.

##### 4.1.1.1 California

Per the methodological process described previously, both daytime and nighttime crash frequency models were estimated using negative binomial regression. The results of these models are shown in Tables 7 and 8. Because a small proportion of the geometric data were missing from the analysis database, a total of 62,027 observations were included in the analysis. The variables included in Table 7 all contain a reasonable level of statistical significance. Those positively correlated with the expected number of daytime crashes are: major and minor road traffic volumes, four-leg intersection type, indicator for signal control, indicator for roadway lighting presence, indicators for left- and right-turn channelization on the major road, and number of lanes indicators on the major road approach. The variables negatively correlated with the expected number of daytime crashes are: tee intersection type indicator, left-turn restriction indicator, and the median presence indicator.



**Table 7 California Intersection Daytime Crash Frequency Model**

Variable	Parameter Estimate	Standard Error	z-statistic	p-value
Constant	-4.518	0.068	-66.85	<0.001
Log major road average daily traffic (veh/day)	0.115	0.007	17.66	<0.001
Log minor road average daily traffic (veh/day)	0.374	0.006	60.38	<0.001
Four-leg intersection type indicator (1 = four-leg intersection; 0 otherwise)	0.397	0.029	13.52	<0.001
Tee intersection type indicator (1 = tee intersection; 0 otherwise)	-0.183	0.029	-6.23	<0.001
Traffic control indicator (1 = signal; 0 = stop-control)	0.058	0.022	2.60	0.009
Lighting indicator (1 = present; 0 = not present)	0.169	0.020	8.36	<0.001
Left-turn channelization on major road indicator (1 = present; 0 otherwise)	0.345	0.021	16.75	<0.001
Left-turn restriction on major road indicator (1 = left-turn restrictions present; 0 otherwise)	-0.467	0.048	-9.75	<0.001
Right-turn channelization on major road indicator (1 = present; 0 otherwise)	0.158	0.022	7.07	<0.001
Median on major road indicator (1 = present; 0 otherwise)	-0.102	0.023	-4.44	<0.001
Major road number of lanes indicator (1 = major road has three or four lanes; 0 otherwise)	0.138	0.022	6.17	<0.001
Major road number of lanes indicator (1 = major road has five or six lanes; 0 otherwise)	0.151	0.035	4.34	<0.001
Dispersion Parameter ( $\alpha$ )	0.994	0.020	49.70	<0.001
Number of observations = 62,027 Log-likelihood (constant only) = -60732.833 Log-likelihood of the fitted model = -52061.488 Pseudo $R^2$ = 0.1428				

The variables included in Table 8 (total nighttime crashes) all contain a reasonable level of statistical significance, except the median indicator. Those positively correlated with the expected number of nighttime crashes are: major and minor road traffic volumes, four-leg intersection type, indicator for signal control, indicators for left- and right-turn channelization on the major road, and number of lanes indicators on the major road approach. The variables negatively correlated with the expected number of nighttime crashes are: tee intersection type indicator, lighting indicator, and the left-turn restriction indicator.

**Table 8 California Intersection Nighttime Crash Frequency Model**

Variable	Parameter Estimate	Standard Error	z-statistic	p-value
Constant	-5.430	0.102	-53.06	<0.001
Log major road average daily traffic (veh/day)	0.092	0.010	9.39	<0.001
Log minor road average daily traffic (veh/day)	0.369	0.009	39.39	<0.001
Four-leg intersection type indicator (1 = four-leg intersection; 0 otherwise)	0.442	0.047	9.51	<0.001
Tee intersection type indicator (1 = tee intersection; 0 otherwise)	-0.103	0.047	-2.20	0.028
Traffic control indicator (1 = signal; 0 = stop-control)	0.379	0.032	11.67	<0.001
Lighting indicator (1 = present; 0 = not present)	-0.086	0.032	-2.68	0.007
Left-turn channelization on major road indicator (1 = present; 0 otherwise)	0.345	0.032	10.84	<0.001
Left-turn restriction on major road indicator (1 = left-turn restrictions present; 0 otherwise)	-0.397	.074	5.37	<0.001
Right-turn channelization on major road indicator (1 = present; 0 otherwise)	0.198	0.030	6.50	<0.001
Median on major road indicator (1 = present; 0 otherwise)	0.014	0.034	0.42	0.674
Major road number of lanes indicator (1 = major road has three or four lanes; 0 otherwise)	0.062	0.034	1.82	0.070
Major road number of lanes indicator (1 = major road has five or six lanes; 0 otherwise)	0.146	0.050	2.95	0.003
Dispersion Parameter ( $\alpha$ )	1.002	0.040	25.05	<0.001
Number of observations = 62,027 Log-likelihood (constant only) = -31129.769 Log-likelihood of the fitted model = -26401.153 Pseudo R <sup>2</sup> = 0.1519				

The relative effects of each indicator variable were computed as  $e^{\beta_k} - 1$ . The data shown in Table 9 are relative effects for the daytime and nighttime crash frequencies. Assuming all other explanatory variables are held constant, the relative effects of a four-leg intersection are a 48.7 percent increase in the expected daytime crash frequency when compared to wye or offset intersections. The relative effects of a tee intersection are a 16.7 percent reduction in the expected daytime crash frequency when compared to wye or offset intersections. The relative effect of a signalized intersection is a 6 percent increase in the expected daytime crash frequency when compared to a stop-controlled intersection. The relative predicted effect of fixed roadway lighting is an 18.4 percent increase in the expected daytime crash frequency when compared to intersections with no fixed roadway lighting. Left-turn and right-turn channelization on the major road increases the expected daytime crash frequency at California intersections increases the expected daytime crash frequency by 41.2 and 17.1 percent, respectively, when compared to intersections without left- and right-turn channelization. Left-turn restrictions on the major road decreases the expected daytime crash frequency by 37.3 percent when compared to intersections without left-turn restrictions. The presence of a median on the major road decreases the expected daytime crash frequency by 9.7 percent when compared to intersections without

a median on the major road. Major roads with more than two-lanes increases the expected crash frequency when compared to major roads with two approach lanes.

Assuming all other explanatory variables are held constant, the relative effects of a four-leg intersection are a 55.6 percent increase in the expected nighttime crash frequency when compared to wye or offset intersections. The relative effects of tee intersection are a 9.8 percent reduction in the expected nighttime crash frequency when compared to wye or offset intersections. The relative effect of a signalized intersection is a 46.1 percent increase in the expected nighttime crash frequency when compared to a stop-controlled intersection. The relative predicted effect of fixed roadway lighting is an 8.2 percent decrease in the expected nighttime crash frequency when compared to intersections with no fixed roadway lighting. Left-turn and right-turn channelization on the major road increases the expected daytime crash frequency at California intersections increases the expected daytime crash frequency by 41.2 and 21.9 percent, respectively, when compared to intersections without left- and right-turn channelization. Left-turn restrictions on the major road decreases the expected daytime crash frequency by 32.8 percent when compared to intersections without left-turn restrictions. Major roads with more than two-lanes increases the expected crash frequency when compared to major roads with two approach lanes.

Using equation (4), the percent difference in the night-day crash ratio for California intersections with and without lighting is -22.51 percent. This was computed using the lighting parameter estimate from the nighttime and daytime crash frequency negative binomial regression analysis results presented in Tables 7 and 8. As such, the negative binomial regression modeling approach indicates that fixed roadway lighting at California intersections is associated with a positive safety effect when compared to intersections without fixed roadway lighting.

**Table 9 Relative Effects for Indicator Variables in California Crash Frequency Models**

Variable	Daytime Relative Effects <sup>a</sup>	Nighttime Relative Effects <sup>a</sup>
Four-leg intersection type indicator (1 = four-leg intersection; 0 otherwise)	0.487	0.556
Tee intersection type indicator (1 = tee intersection; 0 otherwise)	-0.167	-0.098
Traffic control indicator (1 = signal; 0 = stop-control)	0.060	0.461
Lighting indicator (1 = present; 0 = not present)	0.184	-0.082
Left-turn channelization on major road indicator (1 = present; 0 otherwise)	0.412	0.412
Left-turn restriction on major road indicator (1 = left-turn restrictions present; 0 otherwise)	-0.373	-0.328
Right-turn channelization on major road indicator (1 = present; 0 otherwise)	0.171	0.219
Median on major road indicator (1 = present; 0 otherwise)	-0.097	N/A
Major road number of lanes indicator (1 = major road has three or four lanes; 0 otherwise)	0.148	0.064
Major road number of lanes indicator (1 = major road has five or six lanes; 0 otherwise)	0.163	0.157
<sup>a</sup> Relative effects are computed for each indicator variable. Relative effects are computed as $[\exp(\beta) - 1]$ .		

The overdispersion parameter,  $\alpha$ , was statistically different than zero in both the daytime and nighttime crash frequency models, indicating that the crash frequency variance exceeds the mean. The pseudo- $R^2$  is computed as follows:

$$R^2 = 1 - \frac{LL(\beta)}{LL(0)} \quad (6)$$

where:  $LL(\beta)$  = log-likelihood for the full model  
 $LL(0)$  = log-likelihood for the constant only model

The low value of the pseudo- $R^2$  statistic (0.1428) in the daytime crash frequency model indicates a relatively poor fit for the daytime crash frequency model. Likewise, the pseudo- $R^2$  statistic in the nighttime crash frequency (0.1519) model indicates a relatively poor fit to the data.

The log-linear night-day ratio linear regression model for all California intersections was estimated and the model results are shown in Table 10. A significant amount of data attrition resulted from the night-day crash ratio log-linear models (5,296 observations). As such, these models are not recommended for interpretation. The presence of lighting decreases the natural logarithm of the night-day crash ratio by 0.054.

**Table 10 Log-linear Regression Model of Night-Day Crash Ratio for California Intersections**

Variable	Parameter Estimate	Standard Error	t-statistic	p-value
Constant	-0.215	0.099	-2.17	0.030
Log major road average daily traffic (veh/day)	0.005	0.009	0.60	0.549
Log minor road average daily traffic (veh/day)	-0.033	0.008	-4.09	<0.001
Four-leg intersection type indicator (1 = four-leg intersection; 0 otherwise)	-0.025	0.045	-0.57	0.570
Tee intersection type indicator (1 = tee intersection; 0 otherwise)	0.130	0.046	2.81	0.005
Traffic control indicator (1 = signal; 0 = stop-control)	0.026	0.027	0.96	0.335
Lighting indicator (1 = present; 0 = not present)	-0.054	0.030	-1.80	0.072
Left-turn channelization on major road indicator (1 = present; 0 otherwise)	-0.032	0.028	-1.18	0.229
Left-turn restriction on major road indicator (1 = left-turn restrictions present; 0 otherwise)	0.003	0.070	0.04	0.969
Right-turn channelization on major road indicator (1 = present; 0 otherwise)	-0.053	0.024	-2.24	0.025
Median on major road indicator (1 = present; 0 otherwise)	0.045	0.028	1.61	0.109
Major road number of lanes indicator (1 = major road has three or four lanes; 0 otherwise)	-0.015	0.029	-0.50	0.615
Major road number of lanes indicator (1 = major road has five or six lanes; 0 otherwise)	-0.057	0.040	-1.41	0.158
Number of observations = 5,296 R <sup>2</sup> = 0.0235 R <sub>adj</sub> <sup>2</sup> = 0.0213				

The third approach to evaluate the safety effects of roadway lighting at California intersections was to use the observed data and compute the night-day crash ratio. To compute the percent difference between the lighted and unlighted intersections, equation (1) was used. From all of the observed data, the night-day crash ratio at intersections with lighting was 0.3313 (9235 night crashes and 27,878 day crashes) while the night-day crash ratio at intersections without lighting was 0.3420 (2373 night crashes and 6938 day crashes). As such the percent difference per equation (1) is -3.1 percent. Alternatively stated, the night-day crash ratio is 3.1 percent lower with fixed roadway lighting at intersections in California when compared to intersections without lighting. When comparing this measure to those obtained in the regression model estimations described previously, it is clear that using the night-day ratio as a measure of safety underestimates the effects of roadway lighting at intersections in California. One possible explanation for this underestimation is the lack of control given to the geometric features and traffic volume present at the intersections.

Rather than show all of the negative binomial regression, log-linear regression, and descriptive statistics analysis results in this section, a summary of these results is provided in Table 10. All of the statistical modeling results for California intersections are shown in Appendix A.

**Table 11 Summary of California Intersection Analysis Results**

Roadway Type	NB Model	Descriptive Statistics	NB Model Sample Size	Night-Day Ratio Model	Night-Day Ratio Sample Size
All Intersections	-22.51	-3.15	62,055	-5.40	17,349
All Signalized	-24.54	-15.40	8494	-16.9	2862
All Stop-control	-23.15	-21.86	53,561	-3.97	2434
All Four-leg	-26.60	1.40	20,514	-10.1	9347
All Tee	-20.02	-11.68	35,828	1.2	6696
All Wye/Offset	-30.58	-15.36	5713	-10.1	1301
Signalized Four-leg	-22.40	-18.93	6290	-16.3	4589
Stop Four-leg	-24.45	-23.43	14,224	-6.9	4758
Signalized Tee	-1.18	12.98	1830	-33.0	966
Stop Tee	-20.52	-19.55	33,998	0.1	5735
Signalized Wye/Offset	-95.77	N/A	374	N/A	190
Stop Wye/Offset	-24.37	-22.16	5339	-10.1	1111

Based on the negative binomial regression analysis results shown in Table 11, intersections with fixed roadway lighting have fewer expected total crashes than intersections without fixed roadway lighting at all levels of the analysis taxonomy. The percent difference between intersections with lighting and those without lighting in California ranges from -1.18 to -95.77 percent. When excluding the lower-order negative binomial regression models (i.e., signalized and stop-controlled four-leg, signalized and stop-controlled tee, and signalized and stop-controlled wye/offset intersections), the percent difference in the expected crash frequency between lighted and unlighted intersection in California is -20.02 to -30.58 percent. The descriptive statistics and night-day ratio model results generally coincide with the negative binomial regression models with respect to the sign, but are lower in magnitude.

#### 4.1.1.2 Minnesota

Per the methodological process described previously, both daytime and nighttime crash frequency models were estimated using negative binomial regression. Because some geometric design data were missing from the analysis database, the number of observations included in the analysis was 22,058. The variables included in Table 12 (total daytime crashes) all contain a reasonable level of statistical significance. Those positively correlated with the expected number of daytime crashes are: major and minor road traffic volumes, indicator for signal control, indicator for lighting presence, skewed intersection form indicator, depressed median indicator, and paved right shoulder indicator. The explanatory variables that are negatively correlated with the expected daytime crash frequency are: percent heavy vehicles on the major road, urban area indicator, posted speed limit indicator, no access control indicator, and the paved left shoulder indicator. Assuming all other explanatory variables are held constant, the relative effects of an urban/suburban intersection are a 9.45 percent decrease in the expected daytime crash frequency when compared to rural intersection locations. High-speed on the major road decreases the expected daytime crash frequency by 15.79 percent compared to low-speed operations. No access control and a paved left-shoulder also

decrease the expected daytime crash frequency when compared to their baseline levels (i.e., partial access control and no or unpaved left shoulders).

Traffic signal control, the presence of lighting, skewed crossing, depressed median, and paved right shoulder all increase the expected daytime crash frequency, holding all other explanatory variables constant. Signal control increases the expected daytime crash frequency by 90.49 percent when compared to stop control. The presence of roadway lighting is associated with an increased expected daytime crash frequency by nearly 5 percent when compared to no lighting. Skewed intersections increase the expected daytime crash frequency by 62.62 percent when compared to cross or tee intersections. This finding was expected because of the limited intersection sight distance often associated with skewed intersections when compared to right-angle intersections. Depressed medians and paved right shoulders increase the expected by approximately 8 to 9 percent when compared to barrier or no medians and unpaved or no shoulders, respectively.

The overdispersion parameter,  $\alpha$ , was statistically different than zero. The low value of the pseudo- $R^2$  statistic (0.1355) in the daytime crash frequency model indicates a relatively poor fit for the daytime crash frequency model.

The nighttime crash frequency model estimation results are shown in Table 13. The relative effects for each indicator variable are shown in Table 14. When comparing the relative effects of the daytime crash frequency model to those from the nighttime frequency model, the signs are all the same except for the lighting indicator. It was expected that roadway lighting would decrease the nighttime crash frequency as a result of improved visibility. During the daytime, one would expect either no change or a slight increase in crash frequency with lighting when compared to intersections without lighting. This may be due to the addition of fixed objects near the travel lane. In the model estimation of nighttime crashes, the overdispersion parameter,  $\alpha$ , was again statistically different than zero. The pseudo- $R^2$  was low (0.1259) indicating a relatively poor model fit.

**Table 12 Total Daytime Crash Frequency Estimation Results for Minnesota Intersections**

Variable	Parameter Estimate	z-statistic	p-value
Constant	-6.5373	-43.37	<0.001
Log major road average daily traffic	0.6011	38.88	<0.001
Percent heavy vehicles on major road	-0.0092	-3.30	0.001
Log minor road average daily traffic	0.1603	21.79	<0.001
Area type indicator (1 = urban/suburban; 0 = rural)	-0.0992	-3.39	0.001
Traffic control indicator (1 = signal; 0 = stop-control)	0.6445	21.07	<0.001
Lighting indicator (1 = present; 0 = not present)	0.0477	1.56	0.119
Intersection type indicator (1 = skew; 0 = cross or tee)	0.4862	15.86	<0.001
Speed indicator* (1 = 50 mph or greater; 0 otherwise)	-0.1601	-7.36	<0.001
No access control indicator * (1 = no access; 0 = partial access control)	-0.0416	-1.09	0.276
Depressed median indicator* (1 = depressed median; 0 = barrier or no median)	0.0851	2.53	0.011
Paved left-shoulder indicator* (1 = paved shoulder; 0 = unpaved or no shoulder)	-0.1163	-2.75	0.006
Paved right-shoulder indicator* (1 = paved shoulder; 0 = unpaved or no shoulder)	0.0798	1.93	0.054
Dispersion parameter ( $\alpha$ )	0.9487	40.31	<0.001
Number of observations = 22,058 Log-likelihood (constant only) = -28,954.27 Log-likelihood (full model) = -27,084.31 Pseudo R <sup>2</sup> = 0.1355			



**Table 13 Total Nighttime Crash Frequency Estimation Results for Minnesota Intersections**

Variable	Parameter Estimate	z-statistic	p-value
Constant	-6.8986	-33.53	<0.001
Log major road average daily traffic	0.5737	26.85	<0.001
Percent heavy vehicles on major road	-0.0168	-4.37	<0.001
Log minor road average daily traffic	0.1262	12.29	<0.001
Area type indicator (1 = urban/suburban; 0 = rural)	-0.4212	-10.52	<0.001
Traffic control indicator (1 = signal; 0 = stop-control)	0.7120	17.20	<0.001
Lighting indicator (1 = present; 0 = not present)	-0.0791	-1.86	0.062
Intersection type indicator (1 = skew; 0 = cross or tee)	0.4845	12.17	<0.001
Speed indicator (1 = 50 mph or greater; 0 otherwise)	-0.1131	-3.88	<0.001
No access control indicator (1 = no access; 0 = partial access control)	-0.0148	-0.31	0.754
Depressed median indicator (1 = depressed median; 0 = barrier or no median)	0.1712	3.99	<0.001
Paved left-shoulder indicator (1 = paved shoulder; 0 = unpaved or no shoulder)	-0.2907	-5.44	<0.001
Paved right-shoulder indicator (1 = paved shoulder; 0 = unpaved or no shoulder)	0.2153	4.11	<0.001
Dispersion parameter ( $\alpha$ )	0.8948	21.99	<0.001
Number of observations = 22,058 Log-likelihood (constant only) = -17,842.15 Log-likelihood (full model) = -15,165.85 Pseudo R <sup>2</sup> = 0.1259			

**Table 14 Relative Effects for Indicator Variables in the Minnesota Crash Frequency Models**

Variable	Daytime Relative Effects <sup>a</sup>	Nighttime Relative Effects <sup>a</sup>
Area type indicator (1 = urban/suburban; 0 = rural)	-9.45	-34.30
Traffic control indicator (1 = signal; 0 = stop-control)	90.49	103.80
Lighting indicator (1 = present; 0 = not present)	4.89	-7.61
Intersection type indicator (1 = skew; 0 = cross or tee)	62.62	62.34
Speed indicator (1 = 50 mph or greater; 0 otherwise)	-15.79	-12.29
No access control indicator (1 = no access; 0 = partial access control)	-4.07	-1.47
Depressed median indicator (1 = depressed median; 0 = barrier or no median)	8.88	18.67
Paved left-shoulder indicator (1 = paved shoulder; 0 = unpaved or no shoulder)	-10.98	-25.23
Paved right-shoulder indicator (1 = paved shoulder; 0 = unpaved or no shoulder)	8.30	24.02
<sup>a</sup> Relative effects are computed for each indicator variable. Relative effects are computed as $[\exp(\beta) - 1]$ .		

The night-day ratio linear regression model was estimated and the model results are shown in Table 15. The signs of all of the parameter estimates from linear regression model are the same as those for the nighttime crash frequency model shown in Table 14. Interpretation of the model parameters is straight-forward. For example, the presence of lighting decreases the natural logarithm of the night-day crash ratio by 0.1277. Alternatively stated, the presence of lighting decreases the expected night-day crash ratio by 12.8 percent.

Using the data from the negative binomial regression models, equation (4) is -11.9, or an 11.9 percent reduction in the expected night-day crash ratio at intersections in Minnesota with lighting. This closely matches the results of the linear regression model and suggests that the parameter estimates obtained from the model estimation process are consistent with those obtained from the negative binomial regression modeling process.

**Table 15 Log-linear Night-Day Ratio Crash Estimation Results for Minnesota Intersections**

Variable	Parameter Estimate	t-statistic	p-value
Constant	-10.7040	-23.79	<0.001
Log major road average daily traffic	0.6008	12.98	<0.001
Percent heavy vehicles on major road	-0.0303	-3.68	<0.001
Log minor road average daily traffic	0.1391	6.63	<0.001
Area type indicator (1 = urban/suburban; 0 = rural)	-0.6132	-7.12	<0.001
Traffic control indicator (1 = signal; 0 = stop-control)	1.1086	12.82	<0.001
Lighting indicator (1 = present; 0 = not present)	-0.1277	-1.41	0.159
Intersection type indicator (1 = skew; 0 = cross or tee)	0.5781	6.47	<0.001
Speed indicator (1 = 50 mph or greater; 0 otherwise)	-0.1800	-2.83	0.005
No access control indicator (1 = no access; 0 = partial access control)	-0.0509	-0.48	0.633
Depressed median indicator (1 = depressed median; 0 = barrier or no median)	0.3470	3.60	<0.001
Paved left-shoulder indicator (1 = paved shoulder; 0 = unpaved or no shoulder)	-0.5034	-4.21	<0.001
Paved right-shoulder indicator (1 = paved shoulder; 0 = unpaved or no shoulder)	0.4714	4.03	<0.001
Number of observations = 9,053 R <sup>2</sup> = 0.1324 Adjusted R <sup>2</sup> = 0.1312 Root MSE = 2.8814			

The third approach to evaluate the safety effects of roadway lighting at Minnesota intersections is to use the observed data and compute the night-day ratio. To compute the percent difference between the lighted and unlighted intersections, equation (1) was used. From all of the observed data, the night-day crash ratio at intersections with lighting was 0.2933 (6109 night crashes and 20,831 day crashes) while the night-day crash ratio at intersections without lighting was 0.4096 (3341 night crashes and 8156 day crashes). As such, the percent difference per equation (1) is -28.4 percent. Alternatively stated, the night-day crash ratio is 28.4 percent lower with fixed roadway lighting at intersections in Minnesota when compared to intersections without lighting. When comparing this measure to those obtained in the regression model estimations described previously, it is clear that using the night-day ratio as a measure of safety overestimates the effects of roadway lighting at intersections in Minnesota. One possible explanation for this overestimation is the lack of control given to the geometric features and traffic volumes present at the intersections.

Rather than show all of the negative binomial regression, log-linear regression, and descriptive statistics analysis results in this section, a summary of these results is provided in Table 16. All of the statistical modeling results are shown in Appendix A.

**Table 16 Summary of Minnesota Intersection Analysis Results**

Intersection Type	NB Model	Descriptive Statistics (N/D)	NB Sample Size	N/D Log-linear Model	N/D Log-linear Sample Size
All intersections	-11.91%	-28.00%	22,058	-12.77%	9,053
All signalized	-5.19%	5.04%	3,227	-40.58%	2,834
All unsignalized	-7.45%	-30.91%	18,831	-4.25%	6,219
Cross	-14.66%	-24.26%	10,593	-28.44%	4,955
Skew	-11.09%	-22.49%	2,502	9.96%	1,284
Tee	-8.85%	-30.62%	8,963	-17.14%	2,814
All urban	-14.37%	-8.84%	10,605	-29.91%	5,445
Urban signalized	-6.51%	13.46%	2,875	-39.69%	2,521
Urban unsignalized	-13.27%	-18.96%	7,730	-27.92%	2,924
Urban signalized cross	-26.46%	-7.90%	2,158	-107.70%	1,900
Urban signalized skew	64.62%	98.95%	514	88.38%	450
Urban signalized tee	117.81%	162.93%	203	150.57%	171
Urban unsignalized cross	12.47%	3.47%	3,547	-8.33%	1,475
Urban unsignalized skew	-1.65%	-2.96%	663	40.68%	293
Urban unsignalized tee	-25.33%	-30.98%	3,520	-54.63%	1,156
All rural	-1.44%	-16.87%	11,453	18.56%	3,608
Rural signalized	0.33%	-8.69%	352	-38.23%	313
Rural unsignalized	-1.55%	-7.55%	11,101	19.37%	3,295
Rural signalized cross	-2.58%	-7.99%	248	6.64%	223
Rural signalized skew	-10.23%	-15.06%	48	-136.01%	44
Rural signalized tee	n/a	n/a	0	n/a	0
Rural unsignalized cross	-12.23%	-20.45%	4,640	15.75%	1,357
Rural unsignalized skew	-19.31%	-18.71%	1,277	20.52%	497
Rural unsignalized tee	13.37%	6.07%	5,184	21.41%	1,441

#### 4.1.2 Minnesota Interchanges

Per the methodological process described previously, both daytime and nighttime crash frequency models were estimated using negative binomial regression. Because some geometric design data were missing for some intersections, the number of observations included in the analysis was 2,021. The negative binomial regression model for the expected number of daytime crashes on Minnesota interchanges is shown in Table 17. Those explanatory variables positively correlated with the expected number of daytime crashes are: total entering vehicles, urban/suburban area type, diamond interchange form, lighting presence indicator, indicators for full- and partial-access control on the major road, indicator for median barrier presence on the major road, concrete pavement surface type indicator, and the indicator for major roadways with five or more through lanes (in both directions). The explanatory variables that are negatively correlated with the expected daytime crash frequency are: percent heavy vehicle on the major road, posted speed limit on the major road, and lane width indicator. The relative effects for each

indicator variable in the daytime and nighttime models are shown in Table 18. Assuming all other explanatory variables are held constant, the relative effects of an urban/suburban interchange are a 44.84 percent increase in the expected daytime crash frequency when compared to rural interchange locations in Minnesota. Diamond interchange forms have a higher daytime expected crash frequency than non-diamond interchange forms by 30.47 percent. Interchanges with access control on the major road have a higher expected daytime crash frequency than those with no access control. Interchange locations with a median barrier have a 22.51 percent higher expected daytime crash frequency than interchange locations without longitudinal median barrier. Interchange locations with five or more lanes have a 27.51 percent higher expected daytime crash frequency than interchange locations with fewer travel lanes.

The percent heavy vehicles, posted speed limit, and wide travel lanes on the major roadway all decrease the expected daytime crash frequency at Minnesota interchange locations, holding all other explanatory variables constant. The relative effects of lane widths 13-feet or wider is -20.63 percent when compared to narrower lanes. This suggests that the expected daytime crash frequency is higher for narrower lanes at Minnesota interchange locations.

The overdispersion parameter,  $\alpha$ , was statistically different than zero. The low value of the pseudo- $R^2$  statistic (0.0994) in the daytime crash frequency model indicates are relatively poor fit for the daytime crash frequency model.

**Table 17 Total Daytime Crash Frequency Estimation Results for Interchanges**

Variable	Parameter Estimate	Standard Error	z-statistic	p-value
Constant	-0.145	0.274	-0.528	0.598
Log total entering vehicles (vehicles/day)	0.219	0.019	11.735	<0.001
Percent heavy vehicles on major road	-0.050	0.005	-9.246	<0.001
Area type indicator (1 = urban/suburban; 0 = rural)	0.368	0.060	6.094	<0.001
Interchange form indicator (1 = diamond; 0 = non-diamond)	0.266	0.060	4.436	<0.001
Lighting indicator (1 = present; 0 = not present)	0.217	0.067	3.219	0.001
Posted speed limit on major road (mph)	-0.009	0.003	-3.299	0.001
Indicator for full-access control on major road (1 = full-access control; 0 = otherwise)	0.638	0.064	9.906	<0.001
Indicator for partial-access control on major road (1 = partial access control; 0 = otherwise)	0.204	0.084	2.417	0.016
Indicator for median barrier presence on major road (1 = median barrier present; 0 = no barrier present)	0.203	0.045	4.474	<0.001
Pavement surface indicator (1 = concrete pavement; 0 = asphalt pavement)	0.051	0.040	1.281	0.200
Lane width indicator for major road (1 = lane width $\geq$ 13-feet; 0 = otherwise)	-0.231	0.063	-3.652	<0.001
Number of lanes on major road indicator (1 = Five or more lanes; 0 = otherwise)	0.243	0.047	5.142	<0.001
Dispersion parameter ( $\alpha$ )	0.554	0.021	25.851	<0.001
Number of observations = 2,021 Log-likelihood (constant only) = -7134.6036 Log-likelihood (full model) = -6425.7234 Pseudo R <sup>2</sup> = 0.0994				

**Table 18 Relative Effects for Indicator Variables in Interchange Crash Frequency Models**

Variable	Daytime Relative Effects <sup>a</sup>	Nighttime Relative Effects <sup>a</sup>
Area type indicator (1 = urban/suburban; 0 = rural)	44.48	27.51
Interchange form indicator (1 = diamond; 0 = non-diamond)	30.47	14.57
Lighting indicator (1 = present; 0 = not present)	31.00	14.57
Indicator for full-access control on major road (1 = full-access control; 0 = otherwise)	89.27	80.22
Indicator for partial-access control on major road (1 = partial access control; 0 = otherwise)	22.63	11.18
Indicator for median barrier presence on major road (1 = median barrier present; 0 = no barrier present)	22.51	18.77
Pavement surface indicator (1 = concrete pavement; 0 = asphalt pavement)	5.23	-3.54
Lane width indicator for major road (1 = lane width $\geq$ 13-feet; 0 = otherwise)	-20.63	-6.20
Number of lanes on major road indicator (1 = Five or more lanes; 0 = otherwise)	27.51	33.38
<sup>a</sup> Relative effects are computed for each indicator variable. Relative effects are computed as $[\exp(\beta) - 1]$ .		

The nighttime crash frequency model estimation results are shown in Table 19. The relative effects for each indicator variable are shown in Table 18. When comparing the relative effects of the daytime crash frequency model to those from the nighttime frequency model, the signs are all the same except for the pavement surface indicator. In the model estimation of nighttime crashes, the overdispersion parameter,  $\alpha$ , was again statistically different than zero, indicating that the variance exceeds the mean of the crash frequency distribution. The psedo- $R^2$  was low (0.0838) indicating a relatively poor model fit.

Using the parameter estimates from the negative binomial regression models, a 7.78 percent reduction in night-to-day crash ratio is expected at interchanges in Minnesota with lighting.

**Table 19 Total Nighttime Crash Frequency Estimation Results for Interchanges**

Variable	Parameter Estimate	Standard Error	z-statistic	p-value
Constant	-0.685	0.048	-2.29	0.022
Log total entering vehicles (vehicles/day)	0.176	0.020	8.96	<0.001
Percent heavy vehicles on major road	-0.034	0.006	-6.12	<0.001
Area type indicator (1 = urban/suburban; 0 = rural)	0.243	0.065	3.77	<0.001
Interchange form indicator (1 = diamond; 0 = non-diamond)	0.136	0.062	2.20	0.028
Lighting indicator (1 = present; 0 = not present)	0.136	0.072	1.90	0.058
Posted speed limit on major road (mph)	-0.004	0.003	-1.22	0.222
Indicator for full-access control on major road (1 = full-access control; 0 = otherwise)	0.589	0.069	8.56	<0.001
Indicator for partial-access control on major road (1 = partial access control; 0 = otherwise)	0.106	0.091	1.16	0.247
Indicator for median barrier presence on major road (1 = median barrier present; 0 = no barrier present)	0.172	0.047	3.68	<0.001
Pavement surface indicator (1 = concrete pavement; 0 = asphalt pavement)	-0.036	0.041	-0.87	0.385
Lane width indicator for major road (1 = lane width $\geq$ 13-feet; 0 = otherwise)	-0.064	0.066	-0.97	0.332
Number of lanes on major road indicator (1 = Five or more lanes; 0 = otherwise)	0.288	0.049	5.88	<0.001
Dispersion parameter ( $\alpha$ )	0.504	0.024	21.00	<0.001
Number of observations = 2,021 Log-likelihood (constant only) = -5559.251 Log-likelihood (full model) = -5093.5436 Pseudo R <sup>2</sup> = 0.0838				

In addition to the lighting presence models shown above, lighting type models were also run using the Minnesota interchange data. Of particular interest in these models is the influence of partial and full lighting on daytime and nighttime crash frequency. The results of these models are shown in Tables 20 and 21. Based on the daytime crash frequency model, the indicator variables for full and partial interchange lighting are statistically significant and the relative effects are 31.9 and 20.4 percent, respectively. This indicates that the expected daytime crash frequency at Minnesota interchanges is higher with full and partial lighting when compared to no lighting. The nighttime crash frequency model suggests the same. The relative effects from the nighttime crash frequency model for full and partial interchange lighting are 18.5 and 12.9 percent, respectively. Using the data from the negative binomial regression models, equation (4) is -10.15 and -6.29 percent, or a 10.15 and 6.29 percent reduction, respectively, in the expected night-day crash ratio at interchanges in Minnesota with full and partial lighting.



**Table 20 Total Daytime Crash Frequency Estimation Results for Interchange Lighting Type**

Variable	Parameter Estimate	Standard Error	z-statistic	p-value
Constant	-0.069	0.274	-0.25	0.803
Log total entering vehicles (vehicles/day)	0.290	0.019	11.08	<0.001
Percent heavy vehicles on major road	-0.051	0.005	-9.39	<0.001
Area type indicator (1 = urban/suburban; 0 = rural)	0.334	0.062	5.43	<0.001
Interchange form indicator (1 = diamond; 0 = non-diamond)	0.255	0.060	4.25	<0.001
Full interchange lighting indicator (1 = present; 0 = otherwise)	0.277	0.073	3.78	<0.001
Partial interchange lighting indicator (1 = present; 0 = otherwise)	0.186	0.069	2.69	0.007
Continuous interchange lighting indicator (1 = present; 0 = otherwise)	0.435	0.092	4.73	<0.001
Posted speed limit on major road (mph)	-0.009	0.003	-3.19	0.001
Indicator for full-access control on major road (1 = full-access control; 0 = otherwise)	0.664	0.065	10.26	<0.001
Indicator for partial-access control on major road (1 = partial access control; 0 = otherwise)	0.229	0.084	2.72	0.007
Indicator for median barrier presence on major road (1 = median barrier present; 0 = no barrier present)	0.172	0.046	3.74	<0.001
Pavement surface indicator (1 = concrete pavement; 0 = asphalt pavement)	0.045	0.040	1.12	0.262
Lane width indicator for major road (1 = lane width $\geq$ 13-feet; 0 = otherwise)	-0.231	0.063	-3.65	<0.001
Number of lanes on major road indicator (1 = Five or more lanes; 0 = otherwise)	0.235	0.047	4.99	<0.001
Dispersion parameter ( $\alpha$ )	0.550	0.021	25.80	<0.001
Number of observations = 2,021 Log-likelihood (constant only) = -7134.6036 Log-likelihood (full model) = -6418.4594 Pseudo R <sup>2</sup> = 0.1004				

**Table 21 Total Nighttime Crash Frequency Estimation Results for Interchange Lighting Type**

Variable	Parameter Estimate	Standard Error	z-statistic	p-value
Constant	-0.566	0.281	-2.01	0.044
Log total entering vehicles (vehicles/day)	0.165	0.020	8.34	<0.001
Percent heavy vehicles on major road	-0.034	0.006	-6.12	<0.001
Area type indicator (1 = urban/suburban; 0 = rural)	0.222	0.065	3.39	0.001
Interchange form indicator (1 = diamond; 0 = non-diamond)	0.115	0.062	1.86	0.062
Full interchange lighting indicator (1 = present; 0 = otherwise)	0.170	0.078	2.19	0.029
Partial interchange lighting indicator (1 = present; 0 = otherwise)	0.121	0.073	1.65	0.100
Continuous interchange lighting indicator (1 = present; 0 = otherwise)	0.378	0.096	3.93	<0.001
Posted speed limit on major road (mph)	-0.003	0.003	-1.12	0.261
Indicator for full-access control on major road (1 = full-access control; 0 = otherwise)	0.614	0.069	8.88	<0.001
Indicator for partial-access control on major road (1 = partial access control; 0 = otherwise)	0.132	0.091	1.44	0.149
Indicator for median barrier presence on major road (1 = median barrier present; 0 = no barrier present)	0.136	0.048	2.86	0.004
Pavement surface indicator (1 = concrete pavement; 0 = asphalt pavement)	-0.045	0.042	-1.09	0.278
Lane width indicator for major road (1 = lane width $\geq$ 13-feet; 0 = otherwise)	-0.064	0.066	-0.957	0.339
Number of lanes on major road indicator (1 = Five or more lanes; 0 = otherwise)	0.278	0.049	5.69	<0.001
Dispersion parameter ( $\alpha$ )	0.499	0.024	20.78	<0.001
Number of observations = 2,021 Log-likelihood (constant only) = -5559.251 Log-likelihood (full model) = -5086.2512 Pseudo R <sup>2</sup> = 0.0851				

The night-day ratio linear regression models for lighting presence and lighting type were estimated and the model results are shown in Tables 22 and 23. From the lighting presence model, the lighting presence parameter estimate is -0.006 which indicates that the presence of fixed roadway lighting decreases the natural logarithm of the night-day crash ratio by -0.6 percent. From the lighting type log-linear model results shown in Table 21, the full and partial interchange lighting presence dummies are -0.033 and 0.010, respectively. This suggests that full interchange lighting decreases the natural logarithm of the night-day crash ratio by 3.3 percent. The presence of partial interchange lighting increases the natural logarithm of the night-day crash ratio by 1.0 percent when compared to no lighting. In both log-linear models, the lighting indicator variables are not statistically significant. Data attrition appears to be significant as the number of observations is 1,679 – nearly 17 percent of the available data were not used to estimate the log-linear model.

**Table 22 Log-linear Night-Day Ratio Crash Estimation Results for Minnesota Interchanges (Lighting Presence)**

Variable	Parameter Estimate	Standard Error	t-statistic	p-value
Constant	0.029	0.239	0.123	0.902
Log total entering vehicles (vehicles/day)	-0.076	0.017	-4.366	<0.001
Percent heavy vehicles on major road	0.020	0.005	4.328	<0.001
Area type indicator (1 = urban/suburban; 0 = rural)	-0.209	0.054	-3.865	<0.001
Interchange form indicator (1 = diamond; 0 = non-diamond)	-0.191	0.053	-3.599	<0.001
Lighting indicator (1 = present; 0 = not present)	-0.006	0.060	-0.106	0.915
Posted speed limit on major road (mph)	0.004	0.002	1.541	0.123
Indicator for full-access control on major road (1 = full-access control; 0 = otherwise)	-0.076	0.059	-1.301	0.193
Indicator for partial-access control on major road (1 = partial access control; 0 = otherwise)	-0.074	0.077	-0.961	0.337
Indicator for median barrier presence on major road (1 = median barrier present; 0 = no barrier present)	0.004	0.042	0.093	0.926
Pavement surface indicator (1 = concrete pavement; 0 = asphalt pavement)	-0.082	0.036	-2.288	0.022
Lane width indicator for major road (1 = lane width $\geq$ 13-feet; 0 = otherwise)	0.121	0.056	2.179	0.029
Number of lanes on major road indicator (1 = Five or more lanes; 0 = otherwise)	0.002	0.043	0.047	0.963
Number of observations = 1,679 $R^2 = 0.1496$ Adjusted $R^2 = 0.1434$ Root MSE = 0.6874				

**Table 23 Log-linear Night-Day Ratio Crash Estimation Results for Minnesota Interchanges (Lighting Type)**

Variable	Parameter Estimate	Standard Error	t-statistic	p-value
Constant	0.036	0.2239	0.152	0.879
Log total entering vehicles (vehicles/day)	-0.076	0.017	-4.375	<0.001
Percent heavy vehicles on major road	0.021	0.005	4.467	<0.001
Area type indicator (1 = urban/suburban; 0 = rural)	-0.200	0.055	-3.629	<0.001
Interchange form indicator (1 = diamond; 0 = non-diamond)	-0.197	0.053	-3.706	<0.001
Full interchange lighting indicator (1 = present; 0 = otherwise)	-0.033	0.065	-0.503	0.615
Partial interchange lighting indicator (1 = present; 0 = otherwise)	0.010	0.062	0.169	0.866
Continuous interchange lighting indicator (1 = present; 0 = otherwise)	0.038	0.083	0.456	0.648
Posted speed limit on major road (mph)	0.004	0.002	1.491	0.136
Indicator for full-access control on major road (1 = full-access control; 0 = otherwise)	-0.078	0.059	-1.327	0.185
Indicator for partial-access control on major road (1 = partial access control; 0 = otherwise)	-0.074	0.077	-0.962	0.336
Indicator for median barrier presence on major road (1 = median barrier present; 0 = no barrier present)	0.002	0.043	0.035	0.972
Pavement surface indicator (1 = concrete pavement; 0 = asphalt pavement)	-0.087	0.036	-2.405	0.016
Lane width indicator for major road (1 = lane width $\geq$ 13-feet; 0 = otherwise)	0.125	0.056	2.246	0.025
Number of lanes on major road indicator (1 = Five or more lanes; 0 = otherwise)	-0.001	0.043	-0.018	0.985
Number of observations = 1,679 R <sup>2</sup> = 0.1505 Adjusted R <sup>2</sup> = 0.1434 Root MSE = 0.68746				

The third approach to evaluate the safety effects of roadway lighting at Minnesota interchanges is to use the observed data and compute the night-day ratio. To compute the percent difference between the lighted and unlighted intersections, equation (1) was used. From all of the observed data, the night-day crash ratio at interchanges with lighting was 0.4242 (10,304 night crashes and 24,293 day crashes) while the night-day crash ratio at interchanges without lighting was 0.6488 (763 night crashes and 1,176 day crashes). As such the percent difference per equation (1) is -34.6 percent. Alternatively stated, the night-day crash ratio is 34.6 percent lower with fixed roadway lighting at interchanges in Minnesota when compared to interchanges without lighting. When comparing this measure to those obtained in the regression model estimations described previously, it is clear that using the night-day ratio as a measure of safety overestimates the effects of roadway lighting at interchanges in Minnesota. One possible explanation for this overestimation is the lack of control given to the geometric features present at the intersections.

Using equation (4), the percent difference in the night-day crash ratio with and without full interchange lighting is -7.1 percent. The percent difference in the night-day crash ratio with and without partial interchange lighting is 0.8 percent.

Rather than show all of the negative binomial, log-linear regression, and descriptive statistics analysis results in this section, a summary of these results is provided in Table 24. All of the statistical modeling results is shown in Appendix C.

**Table 24 Summary of Minnesota Interchange Analysis Results**

Facility Type	Negative Binomial Model		N/D Ratio Linear Model		Descriptive Statistics
	Model	Sample Size	Model	Sample Size	
All Interchanges	-7.77%	2021	-0.64%	1679	-34.59%
Diamond	-12.80%	1615	-3.25%	1315	-38.80%
Non-diamond	19.60%	406	10.86%	364	11.90%
Rural Interchanges	-1.79%	776	12.24%	540	-26.25%
Urban Interchanges	7.89%	1245	-23.07%	1139	5.39%
Rural - Diamond	-8.81%	644	8.18%	441	-33.19%
Rural - Nondiamond	36.83%	132	30.94%	99	13.52%
Urban - Diamond	11.12%	971	-22.51%	874	4.34%
Urban - Nondiamond	-29.05%	274	-37.23%	265	-3.93%

From the data summary shown in Table 24, the negative binomial regression model and descriptive statistics produce lighting safety effect estimates that have the same sign but are different in magnitude. This was expected as the negative binomial regression models control for many geometric variables and traffic volumes while the descriptive statistics do not control for any explanatory variables. It can generally be concluded that interchanges with fixed roadway lighting have a lower night-day crash ratio than interchanges without fixed roadway lighting. Likewise, the night-day crash ratio for diamond interchange is lower with fixed roadway lighting than without lighting.

#### 4.1.3 Freeway Segments

##### 4.1.3.1 Washington

For the Washington freeway segments, negative binomial regression models were estimated for both nighttime and daytime crashes. The results of these models are shown in Tables 25 and 26 below. The continuous lighting parameter estimate in the nighttime crash frequency model is 0.221 while the nighttime parameter estimate is 0.179. Using equation (4) above, the percent difference in the night-day crash ratio for segments with and without lighting is 4.29 percent. This indicates that freeway segments in Washington have a higher mean crash frequency with lighting than without lighting. Using the standard error of the nighttime and daytime crash frequency parameter estimates suggests that the confidence interval around the mean value ranges from -1.69 to 10.63 percent.

Using equation (1) above, the percent difference in the night-day crash ratios along roadway segments with and without roadway was computed. The night-day crash at segments with lighting was 0.331 (5080 night crashes and 16,333 day crashes) while the night-day crash ratio at segments without lighting was 0.391 (11,528 day crashes and

29,469 night crashes). As such, the percent difference in the night-day crash ratio was -15.35 percent. This indicates that using only the descriptive statistics, without controlling for traffic volume and geometric design variables, overestimates the safety effects of fixed roadway lighting on freeway segments in Washington.

**Table 25 Daytime Crash Frequency Model for Washington Freeway Segments**

Variable	Coefficient	Standard Error	t-statistic
Constant	-10.847	0.403	-26.944
Northwest region indicator* (1 if segment is located in the northwest region; 0 otherwise)	-0.245	0.148	-1.650
Olympic region indicator (1 if segment is located in the olympic region; 0 otherwise)	-0.487	0.147	-3.304
Southwest region indicator (1 if segment is located in the southwest region; 0 otherwise)	-0.664	0.142	-4.675
Eastern region indicator (1 if segment is located in the eastern region; 0 otherwise)	-0.431	0.145	-2.981
South central region indicator (1 if segment is located in the south central region; 0 otherwise)	-0.252	0.141	-1.783
Logarithm of segment length (miles)	0.890	0.013	69.719
Direction indicator (1 if increasing milepost of travel; 0 otherwise)	0.133	0.045	2.929
Rural segment indicator (1 if segment was in rural location; 0 otherwise)	-0.170	0.052	-3.247
Point lighting indicator (1 if segment had point lighting; 0 otherwise)	0.108	0.055	1.970
Continuous lighting indicator (1 if segment had continuous lighting; 0 otherwise)	0.179	0.028	6.411
Number of interchanges in segment	-0.094	0.019	-4.828
Number of overpasses in segment	0.056	0.011	5.135
Logarithm of average annual daily traffic	1.310	0.041	31.604
Number of vertical curves in segment	-0.003	0.004	-0.780
Number of horizontal curves in segment	0.023	0.004	5.098
Number of lanes in segment	-0.013	0.021	-0.592
Left shoulder width in feet	-0.043	0.006	-7.563
Right shoulder width in feet	-0.030	0.005	-6.392
Overdispersion parameter	0.450	0.015	30.508
Log-likelihood at convergence	-12,537.76		
Log-likelihood at zero	-17,806.96		
Number of observations	5,475		
Adjusted $\rho^2$	0.29		

\* North central region is the base region, and set to zero. Region effects in the table should be interpreted using the north central region as a baseline. Since all region effects have a negative sign, north central region segments are expected to have higher crash counts.

**Table 26 Nighttime Crash Frequency Model for Washington Freeway Segments**

Variable	Coefficient	Standard Error	t-statistic
Constant	-11.452	0.433	-26.450
Northwest region indicator* (1 if segment is located in the northwest region; 0 otherwise)	-0.143	0.148	-0.963
Olympic region indicator (1 if segment is located in the Olympic region; 0 otherwise)	-0.379	0.147	-2.572
Southwest region indicator (1 if segment is located in the southwest region; 0 otherwise)	-0.317	0.141	-2.248
Eastern region indicator (1 if segment is located in the eastern region; 0 otherwise)	-0.170	0.143	-1.189
South central region indicator (1 if segment is located in the south central region; 0 otherwise)	-0.040	0.139	-0.289
Logarithm of segment length (miles)	0.885	0.014	62.240
Direction indicator (1 if increasing milepost of travel; 0 otherwise)	0.052	0.048	1.082
Rural segment indicator (1 if segment was in rural location; 0 otherwise)	0.188	0.0520	3.616
Point lighting indicator (1 if segment had point lighting; 0 otherwise)	0.170	0.076	2.229
Continuous lighting indicator ( 1 if segment had continuous lighting; 0 otherwise)	0.221	0.031	7.149
Number of interchanges in segment	-0.048	0.018	-2.654
Number of overpasses in segment	0.025	0.010	2.417
Logarithm of average annual daily traffic	1.205	0.045	26.830
Number of vertical curves in segment	0.003	0.003	0.756
Number of horizontal curves in segment	0.016	0.004	4.058
Number of lanes in segment	0.111	0.023	4.844
Left shoulder width in feet	-0.038	0.006	-6.380
Right shoulder width in feet	-0.023	0.005	-4.416
Overdispersion parameter	0.266	0.015	17.346
Log-likelihood at convergence	-8,349.58		
Log-likelihood at zero	-8,968.72		
Number of observations	5,475		
Adjusted $p^2$	0.067		
* North central region is the base region, and set to zero. Region effects in the table should be interpreted using the north central region as a baseline. Since all region effects have a negative sign, north central region segments are expected to have higher crash counts.			

The findings from the negative binomial models for daytime and nighttime crash occurrence indicate that lighting variables such as the presence of point lighting and continuous lighting are associated with increases in nighttime crashes. When controlling for geometric and traffic volume factors, as well as segment length, lighting presence appears to indicate a greater than expected number of crashes compared to no lighting. In particular, the presence of continuous lighting is associated with a stronger positive effect compared to point lighting. This might suggest that the lighting effect occurs in two possible ways – where non-interchange/non-decision points are lighted, drivers are afforded greater visibility resulting in behavior conducive to increased crash occurrence. For example, more frequent lane changing can be expected to occur in lighted segments. At decision points, especially at interchanges, merge-weave effects contribute to

increased crash likelihoods. While this counter-productive finding may argue for removal of roadway lighting, one should view the finding in a broader context – the tradeoff between decision related conflict points and resulting severities from absence of lighting versus energy gains from removal of lighting.

In terms of other significant findings from Tables 23 and 24, geometric effects with the exception of vertical curves in the roadway segment were found to be significant. The greater the number of interchanges in a segment, the fewer daytime and nighttime crashes were expected to be. This can be attributed to the fact that increased interchange density creates the effect of cautious driving to the extent that it offsets the merge-weave effect that occurs in an isolated manner at interchange areas. On the contrary, as the number of overpasses increase, crash frequency is expected to increase both during the day and night. This might be attributed to the potential visibility and roadside encroachment issues arising from increasing overpass density. Shoulder widths are expected to decrease crash occurrence. With wider roadway lane cross sections, nighttime crashes are expected to increase, while daytime crashes are expected to remain unchanged from a significance standpoint. The magnitude of the variable is marginally negative for daytime effects, and marginally positive for nighttime effects. Horizontal curve frequency in a segment is expected to increase crash occurrence during both daytime and nighttime periods. Vertical curve frequency is expected to have an insignificant impact. Furthermore, the magnitude of vertical curve frequency is less than horizontal curve frequency for both daytime and nighttime periods.

Urban Interstate segments were expected to increase crash occurrence during daytime periods and decrease frequency during nighttime periods, compared to rural locations. The overdispersion parameter is of lesser magnitude for nighttime crash occurrence, while remaining significant in both periods. As expected, traffic volume and segment length (both in logarithm form) contribute the greatest to the variance explained by the models and increase crash frequency during both daytime and nighttime periods.

#### 4.1.3.2 Supplemental Washington Freeway Segments

Several variations of the models shown in Tables 25 and 26 were specified to determine if excluding point lighting only, excluding interchange and overpass locations, or stratifying the sample into urban and rural segments produced different results from the full Washington Interstate segment models described in the previous section. For brevity, the statistical output is not provided in this section of the report. Only the overall assessment of the safety effects of lighting are provided in summary tables below.

As Tables 27a, 27b and 27c show, a total of 4,495 observations were used in the estimation of the combined urban-rural models to estimate the safety effects of continuous roadway lighting, excluding point lighting locations. Continuous lighting was differentiated in terms of whether the location was on the median side only, on the right side only, or on both sides of the freeway. The baseline lighting scenario included segments without any lighting installation. Table 27a shows the mean parameter estimates from the model estimations, while tables 27b and 27c show the estimated changes due to lighting type with associated confidence intervals of one standard error.



Combined Urban and Rural Segments Excluding Point Lighting (with Interchange and Overpasses)

When interchanges and overpasses are included in the assessment, all 4,495 observations remained in the analysis. It is estimated that the presence of median-only continuous lighting is associated with a 10.36 percent reduction in night-day ratios of crash frequencies with respect to the no-lighting baseline. Comparatively, the observed change in night-day ratios was significantly higher, a decrease of 32.58 percent. A right-side only lighting installation was estimated to be associated with a marginal 0.32 percent increase in night-day ratios, while the observed change was a decrease of 40.15 percent. Lighting installations on both sides of a freeway are estimated to be associated with a 15.07 percent decrease in night-day ratios while the observed change was a decrease of 56.82 percent.

Combined Urban and Rural Segments Excluding Point Lighting, Interchanges and Overpasses

When interchanges and overpasses are excluded from the analysis, 495 observations remained in the data analysis file. This indicates that eliminating interchange and overpass locations from the freeway segment database resulted in the exclusion of nearly 90 percent of the sample. As such, continuous freeway lighting is nearly always present in locations that include interchange and overpass locations. The presence of median-only continuous lighting is associated with a 9.69 percent reduction in night-day ratios of crash frequencies with respect to the no-lighting baseline. Comparatively, the observed change in night-day ratios for this scenario was an increase of 17.74 percent. A right-side only lighting installation was associated with a 9.95 percent decrease in night-day ratios, while the observed change was a decrease of 45.16 percent. Lighting installations on both sides of the freeway were associated with a 40.57 percent increase in night-day ratios while the observed change was a decrease of 29.03 percent.

**Table 27a Comparisons of Predicted versus Observed Change in Night-Day Ratios for all Interstate Segments for Median-Side Only, Right-Side Only, and Both-Sides Continuous Lighting**

Overall Model Summary				
Lighting Location	With interchanges and overpasses		Without interchanges and overpasses	
	4,495 observations		495 observations	
	Observed Change <sup>1</sup>	Predicted Change <sup>2</sup>	Observed Change <sup>1</sup>	Predicted Change <sup>2</sup>
Median only	-32.58%	-10.36%	17.74%	-9.69%
Right only	-40.15%	0.32%	-45.16%	-9.95%
Both	-56.82%	-15.07%	-29.03%	40.57%

<sup>1</sup> Values computed based on equation (1)  
<sup>2</sup> Values computed based on equation (4)

**Table 27b Comparisons of Predicted versus Observed Change in Night-Day Ratios for all Interstate Segments with Interchanges and Overpasses for Median-side only, Right-side only, and Both-sides continuous lighting**

Continuous Lighting type (count, %)	Model			Descriptive data: change in night/day ratio
	Change in night/day ratio with lighting (based on $\pm 1$ standard error)	Change in day crashes with lighting ( $\pm 1$ standard error)	Change in night crashes with lighting ( $\pm 1$ standard error)	
Median Only (n=1030, 22.91%)	-10.36% (-1.21% to -16.97%)	+16.05% (+11.33% to +20.78%)	+5.11% (+0.07% to +10.16%)	-32.58%
Right Only (n=630, 14.02%)	+0.32% (-15.89% to 18.89%)	-33.10% (-39.06% to -27.15%)	-32.79% (-39.36% to -26.21%)	-40.15%
Both (n=55, 1.22%)	-15.07% (-34.69% to 15.03%)	+22.26% (+5.63% to +38.88%)	+5.92% (-11.96% to +23.81%)	-56.82%

**Table 27c Comparisons of Predicted versus Observed Change in Night-Day Ratios for all Interstate Segments without Interchanges and Overpasses for Median-side only, Right-side only, and Both-sides Continuous Lighting**

Continuous Lighting type (count, %)	Model			Descriptive data: change in night/day ratio
	Change in night/day ratio with lighting (based on $\pm 1$ standard error)	Change in day crashes with lighting ( $\pm 1$ standard error)	Change in night crashes with lighting ( $\pm 1$ standard error)	
Median Only (n=75, 15.15%)	-9.69% (-20.15% to 11.96%)	+85.41% (+71.14% to +99.68%)	+75.22% (+57.64% to +92.80%)	17.74%
Right Only (n=145, 29.29%)	-9.95% (-31.68% to 19.36%)	+8.50% (-4.66% to +21.66%)	-1.98% (-19.56% to +15.61%)	-45.16%
Both (n=15, 3.03%)	+40.57% (-11.22% to 78.07%)	+32.27% (+6.03% to +58.52%)	+66.33% (+36.05% to +96.60%)	-29.03%

Urban Segments

As tables 28a, 28b and 28c show, a total of 3,720 observations were used in the estimation of urban-only models with interchange and overpass locations present. When excluding interchange and overpass locations from the analysis, 405 observations were included in the safety assessment. Table 28a shows the mean parameter effects, while Tables 28b and 28c show the estimated day, night, and night-day ratio relative effects of continuous roadway lighting. Confidence intervals, computed using the standard error of the parameter estimate, are also shown.

Urban Segments Excluding Point Lighting (with Interchanges and Overpasses)

When interchanges and overpasses are included in the assessment, all 3,720 observations remained in the analysis. It is estimated that the presence of median-only continuous lighting is associated with a 5.45 percent reduction in night-day ratios of crash frequencies when compared to the no-lighting baseline. Comparatively, the observed change in night-day ratios was a marginal increase of 0.99 percent. A right-side only lighting installation was estimated to be associated with a 4.47 percent increase in night-

day ratios, while the observed change was a decrease of 28.60 percent. Lighting installations on both sides were estimated to be associated with an 8.57 percent decrease in night-day ratios while the observed change was a decrease of 7.50 percent.

Urban Segments Excluding Point Lighting, Interchanges, and Overpasses

When interchanges and overpasses are excluded from the assessment, 405 observations remained in the analysis data file. It is estimated that the presence of median-only continuous lighting is associated with a 5.87 percent reduction in night-day ratios of crash frequencies when compared to the no-lighting baseline. Comparatively, the observed change in the night-day ratio was a decrease of 6.12 percent. A right-side only lighting installation was associated with a 1.92 percent increase in the night-day ratio, while the observed change was a decrease of 2.04 percent. Lighting installations on both sides were estimated to be associated with a 40.18 percent increase in night-day ratios while the observed change was a decrease of 10.20 percent.

**Table 28a Comparisons of Predicted versus Observed Change in Night-Day Ratios for Urban Interstate Segments for Median-side only, Right-side only, and Both-sides Continuous Lighting**

Urban Model Summary				
Lighting Location	With interchanges and overpasses		Without interchanging and overpasses	
	3,675 observations		405 observations	
	Observed Change <sup>1</sup>	Predicted Change <sup>2</sup>	Observed Change <sup>1</sup>	Predicted Change <sup>2</sup>
Median only	0.99%	-5.10	-6.12%	-5.87%
Right only	-28.60%	4.47%	-2.04%	1.92%
Both	-7.50%	-8.57%	-10.20%	40.18%
<sup>1</sup> Values computed based on equation (1)				
<sup>2</sup> Values computed based on equation (4)				

**Table 28b Comparisons of Predicted versus Observed Change in Night-day Ratios for Urban Interstate Segments with Interchanges and Overpasses for Median-side only, Right-side only, and Both-sides Continuous Lighting**

Continuous Lighting type (count, %)	Model			Descriptive data: change in night/day ratio
	Change in night/day ratio with lighting (based on ±1 standard error)	Change in day crashes with lighting (±1 standard error)	Change in night crashes with lighting (±1 standard error)	
Median Only (n=995, 26.75%)	-5.10% (-10.77% to 3.05%)	+37.10% (+32.39% to +41.80%)	+31.50% (+26.43% to +36.56%)	0.99%
Right Only (n=500, 13.44%)	+4.47% (-7.13% to 16.88%)	+4.48% (-1.87% to +10.08%)	+8.85% (+1.75% to +15.96%)	-28.60%
Both (n=55, 1.48%)	-8.57% (-26.21% to 18.53%)	+39.20% (+23.00% to +55.39%)	+30.24% (+12.66% to +47.82%)	-7.50%

**Table 28c Comparisons of Predicted versus Observed Change in Night-day Ratios for Urban Interstate Segments without Interchanges and Overpasses for Median-side only, Right-side only, and Both-sides Continuous Lighting**

Continuous Lighting type (count, %)	Model			Descriptive data: change in night/day ratio
	Change in night/day ratio with lighting (based on $\pm 1$ standard error)	Change in day crashes with lighting ( $\pm 1$ standard error)	Change in night crashes with lighting ( $\pm 1$ standard error)	
Median Only (n=70, 16.41%)	-5.87% (-17.88% to 14.22%)	+88.96% (+74.80% to +103.12%)	+82.91% (+65.00% to +100.83%)	-6.12%
Right Only (n=100, 24.10%)	+1.92% (-23.73% to +35.66%)	+12.27% (-1.70% to +28.27%)	+14.17% (-5.04% to +33.38%)	-2.04%
Both (n=15, 3.15%)	+40.18% (-10.77% to 73.33%)	+38.98% (+13.24% to +64.72%)	+72.75% (+42.36% to +103.14%)	-10.20%

Rural Segments

As Tables 29a, 29b and 29c shows, a total of 775 observations were used in the model estimation of rural-only models with interchange and overpass locations present. When excluding interchange and overpass locations, 80 observations were used in the analysis. Table 29a shows the mean effects from the regression models, while tables 29b and 29c show the estimated day, night, and night-day ratio changes due to continuous roadway lighting. The confidence intervals for each mean estimate are also provided.

Rural Segments Excluding Point Lighting (with Interchanges and Overpasses)

When interchanges and overpasses are included in the assessment, all 775 observations remained in the analysis. It is estimated that the presence of median-only continuous lighting is associated with a 16.71 percent reduction in night-day ratios of crash frequencies when compared to the no-lighting baseline. Comparatively, the observed change in the night-day ratios was a decrease of 85.16 percent. A right-side only lighting installation was associated with a 22.16 percent increase in the night-day ratios, while the observed change was a decrease of 50.97 percent. Lighting installations on both sides of a rural freeway were not observed.

Rural Segments Excluding Point Lighting, Interchanges, and Overpasses

When interchanges and overpasses were excluded from the assessment, only 80 observations remained. It is estimated that the presence of median-only continuous lighting is estimated to be associated with a 100 percent reduction in night-day ratios of crash frequencies when compared to the no-lighting baseline. Comparatively, the observed change in night-day ratios was a decrease of 100 percent. A right-side only lighting installation was estimated to be associated with a 17.86 percent decrease in night-day ratios, while the observed change was a decrease of 54.55 percent. Lighting installations on both sides were not observed. Due to small sample sizes in the rural only database the results of the analysis excluding point lighting, interchanges, and overpasses should be interpreted with caution.

**Table 29a Comparisons of Predicted versus Observed Change in Night-day Ratios for Rural Interstate Segments for Median-side only, Right-side only, and Both-sides Continuous Lighting**

Rural Model Summary				
Lighting Location	With interchanges and overpasses		Without interchanging and overpasses	
	775 observations		80 observations	
	Observed Change <sup>1</sup>	Predicted Change <sup>2</sup>	Observed Change <sup>1</sup>	Predicted Change <sup>2</sup>
Median only	-85.16%	-16.71%	-100%	-100.00%
Right only	-50.97%	22.16%	-54.55%	-17.86%
Both	No data	No data	No data	No data
<sup>1</sup> Values computed based on equation (1)				
<sup>2</sup> Values computed based on equation (4)				

**Table 29b Comparisons of Predicted versus Observed Change in Night-day Ratios for Rural Interstate Segments with Interchanges and Overpasses for Median-side only, Right-side only, and Both-sides Continuous Lighting**

Continuous Lighting type (count, %)	Model			Descriptive data: change in night/day ratio
	Change in night/day ratio with lighting (based on ±1 standard error)	Change in day crashes with lighting (±1 standard error)	Change in night crashes with lighting (±1 standard error)	
Median Only (n=35, 4.52%)	-16.71% (-37% to 0%)	-72.84% (-98.84% to -46.83%)	-91.12% (-100% to -55.57%)	-85.16%
Right Only (n=130, 16.77%)	+22.16% (-30% to +30%)	-100% (-100% to -89.80%)	-80.65% (-92.71% to -68.59%)	-50.97%
Both (n=0, 0%)	No data	No data	No data	No data

**Table 29c Comparisons of Predicted versus Observed Change in Night-day Ratios for Rural Interstate Segments without Interchanges and Overpasses for Median-side only, Right-side only, and Both-sides Continuous Lighting**

Continuous Lighting type (count, %)	Model			Descriptive data: change in night/day ratio
	Change in night/day ratio with lighting (based on ±1 standard error)	Change in day crashes with lighting (±1 standard error)	Change in night crashes with lighting (±1 standard error)	
Median Only (n=5, 6.25%)	N/A (Very high s.e.)	-40.45% (-148.37% to +68.46%)	-100% (very high s.e.)	-100.0%
Right Only (n=45, 56.25%)	-17.86% (-67% to 77%)	+18.98% (-16.20% to +54.16%)	-0.70% (-49.35% to +47.96%)	-54.55%
Both (n=0,0%)	No data	No data	No data	No data

#### 4.1.3.2 Oregon Segments

For the Oregon freeway segments, negative binomial regression models were estimated for both nighttime and daytime crashes. The results of these models are shown in Tables 30 and 31 below. The lighting parameter estimate in the daytime crash frequency model is 0.740 while the nighttime parameter estimate is 0.670 in the nighttime crash frequency model. The mean percent difference in the night-day crash ratio for segments with and without lighting is - 6.76 percent. This indicates that freeway segments in Oregon have a lower night-day crash ratio with continuous lighting when compared to segments without continuous lighting. When using the standard error of the mean estimate for daytime and nighttime crashes, the range of the night-day crash ratio is -34.4 to +32.6 percent. Using the descriptive statistics, the night-day crash ratio along freeway segments with lighting was 0.278 (1972 night crashes and 7101 day crashes) while the night-day crash ratio at segments without lighting was 0.468 (1808 day crashes and 3867 night crashes). As such, the percent difference in the night-day crash ratio was -18.98 percent. This indicates that using only the descriptive statistics, without controlling for traffic volume and geometric design variables, the safety effects of roadway lighting on freeway segments in Oregon might be overestimated. Table 32 shows a summary of the safety analysis results.

The findings from the negative binomial models for daytime and nighttime crash occurrence indicate that lighting has a slight positive effect (i.e., lower crash frequency). When controlling for geometric and traffic volume factors, as well as segment length, lighting presence appears to indicate a greater than expected number of crashes when compared to no lighting.

In terms of other significant findings from Tables 30 and 31, an urban area does not have a statistically significant effect on either daytime or nighttime crash occurrence when compared to the baseline of a rural area. A wider paved right shoulder increases the expected daytime crash frequency, but the right paved shoulder width is not statistically significant in the nighttime crash frequency model. The paved left shoulder width was not statistically significant in either the daytime or nighttime crash frequency models. Higher ADTs tend to increase both daytime and nighttime crash occurrence. Freeway segments with two through lanes in each direction are associated with fewer expected daytime and nighttime crashes when compared to freeways with more than two through lanes in each direction. The presence of a median barrier increases daytime crash occurrence, while it has no statistically significant effect on nighttime crash frequency. More horizontal curves along the road segment tend to increase both daytime and nighttime crash occurrence, while the effects of vertical curves are not statistically significant. More interchanges along a road segment tend to increase the expected crash frequencies.

**Table 30 Daytime Crash Frequency Model for Oregon Freeway Segments**

Variable	Coefficient	Standard Error	z	P> z	95% Conf. Interval	
					Lower	Higher
Constant	-8.313	1.181	-7.04	<0.001	-10.627	-5.999
Urban indicator	-0.032	0.147	-0.22	0.830	-0.320	0.257
Left shoulder pavement width (feet)	0.002	0.019	0.09	0.928	-0.035	0.038
Right shoulder pavement width (feet)	0.057	0.023	2.45	0.014	0.011	0.102
Logarithm of average daytime daily traffic (veh/day)	0.998	0.098	10.15	<0.001	0.806	1.191
Presence of lighting indicator	0.740	0.184	4.03	<0.001	0.380	1.100
Two-lanes per direction indicator	-0.444	0.169	-2.62	0.009	-0.776	-0.112
Logarithm of segment length (miles)	0.842	0.059	14.16	<0.001	0.725	0.958
Median barrier presence indicator	0.271	0.141	1.92	0.054	-0.005	0.548
Number of horizontal curves in segment	0.016	0.011	1.46	0.143	-0.006	0.038
Number of vertical curves in segment	-0.001	0.008	-0.19	0.853	-0.016	0.014
Number of interchanges in segment	0.056	0.037	1.52	0.128	-0.016	0.129
Median width (feet)	0.0009	0.002	0.43	0.666	-0.003	0.005
Overdispersion parameter	0.257	0.040			0.190	0.347
Number of observations = 179						
Log likelihood at convergence = -599.45457						
Pseudo R <sup>2</sup> =0.2598						

**Table 31 Nighttime Crash Frequency Model for Oregon Freeway Segments**

Variable	Coefficient	Standard Error	z	P> z	95% Conf. Interval	
					Lower	Higher
Constant	-4.888	1.005	-4.86	<0.001	-6.859	-2.918
Urban indicator	-0.036	0.147	-0.25	0.805	-0.324	0.251
Left shoulder pavement width (feet)	-0.003	0.017	-0.19	0.847	-0.036	0.030
Right shoulder pavement width (feet)	0.032	0.022	1.43	0.153	-0.012	0.075
Logarithm of average nighttime daily traffic (veh/day)	0.709	0.093	7.66	<0.001	0.528	0.890
Lighting presence indicator	0.670	0.168	3.98	<0.001	0.340	1.000
Two-lanes per direction indicator	-0.321	0.163	-1.97	0.049	-0.640	-0.002
Logarithm of segment length (miles)	0.859	0.058	14.7	<0.001	0.745	0.974
Median barrier presence indicator	0.140	0.135	1.04	0.300	-0.125	0.404
Number of horizontal curves in segment	0.013	0.008	1.51	0.130	-0.004	0.029
Number of vertical curves in segment	-0.002	0.006	-0.36	0.722	-0.015	0.010
Number of interchanges in segment	0.043	0.031	1.39	0.165	-0.018	0.103
Median width (feet)	-0.0004	0.002	-0.18	0.859	-0.004	0.004
Overdispersion parameter	0.158	0.032			0.107	0.2347
Number of observations = 179						
Log likelihood at convergence = -474.549						
Pseudo R <sup>2</sup> =0.2861						

**Table 32 Summary of statistical modeling and descriptive statistics for N/D crash ratios, nighttime crashes, and daytime crashes associated with lighting for OR highway segments**

Number of segments with lighting	Model			Descriptive data: change in night/day ratio
	Change in night/day ratio with lighting	Change in day crashes with lighting	Change in night crashes with lighting	
19 (10.6%)	-6.76%	+109.6%	+95.4%	-18.98%

4.1.3.3 Virginia Segments

For the Virginia freeway segments, negative binomial regression models were estimated for both nighttime and daytime crashes. The results of these models are shown in Tables 33 and 34 below. The overdispersion parameter was statistically significant in both models. The lighting parameter estimate in the daytime crash frequency model is -0.027, but is not statistically significant. The nighttime parameter estimate is -0.095. The percent difference in the night-day crash ratio for segments with and without lighting is -



6.64 percent. Using the standard error of this estimate, the range in the night-day crash ratio is +6.29 to -17.5 percent. Using the observed crash count data, the night-day crash on segments with lighting was 0.390 (4966 night crashes and 12,730 day crashes) while the night-day crash ratio on segments without lighting was 0.446 (1173 day crashes and 2632 night crashes). As such, the percent difference in the night-day crash ratio was -5.6 percent. This indicates that using only the observed crash count data, without controlling for traffic volume and geometric design variables, the safety effects of roadway lighting on freeway segments in Virginia may be slightly underestimated. Table 35 shows a summary of the statistical modeling and descriptive statistics analysis for night-day crash ratios, nighttime crashes, and daytime crashes associated with continuous freeway lighting on Virginia freeway segments.

Other findings from the statistical models for daytime and nighttime crashes shown in Tables 33 and 34 are as follows:

- A unit increase in the right shoulder width is associated with an increase in the expected daytime and nighttime crash frequencies.
- The left shoulder width has no statistically significant association with daytime crash frequencies, while a unit increase in the left shoulder width is associated with a decrease in the expected nighttime crash frequency.
- The median width has no statistically significant effect on daytime crashes, but a unit increase in the median width is associated with an increase in the expected number of nighttime crashes.
- Higher truck traffic percentages is associated with an increase in the expected number of daytime crashes, but the effect of truck traffic percentage on nighttime crash occurrence is not statistically significant.
- Increased traffic volumes are associated with an increase in the expected number of daytime and nighttime crashes.
- Two through travel lanes per direction are associated with an increase in the expected number of daytime crashes when compared to the baseline of four or more through travel lanes per direction. However, the opposite effect was found in the nighttime crash frequency model. Three through travel lanes per direction are associated with an increase in the expected number of daytime and nighttime crashes when compared to the baseline of four or more through travel lanes per direction.
- The presence of a median barrier increases the expected nighttime crash frequency, while it has no statistically significant effect on daytime crash frequency.
- The presence of interchanges along a road segment tends to increase both daytime and nighttime crash frequencies, but the effect on daytime crash frequency is not statistically significant.

**Table 33 Daytime Crash Frequency Model for Virginia Freeway Segments**

Variable	Coefficient	Standard Error	z	P> z	95% Conf. Interval	
					Lower	Higher
Constant	-7.334	0.775	-9.460	<0.001	-8.854	-5.815
Lighting presence indicator	-0.027	0.059	-0.450	0.652	-0.143	0.089
Number of interchanges in segment	0.076	0.055	1.380	0.168	-0.032	0.185
Two-lanes per direction indicator	0.238	0.076	3.150	0.002	0.090	0.386
Three-lanes per direction indicator	0.431	0.049	8.810	<0.001	0.335	0.527
Right shoulder width (feet)	0.024	0.007	3.620	<0.001	0.011	0.036
Left shoulder width (feet)	0.001	0.006	0.240	0.814	-0.010	0.012
Percentage of truck traffic	0.016	0.009	1.840	0.066	-0.001	0.033
Median width (feet)	0.00006	0.001	0.120	0.906	-0.001	0.001
Logarithm of segment length (miles)	0.570	0.020	27.880	<0.001	0.530	0.610
Logarithm of average daily traffic (veh/day)	0.838	0.067	12.440	<0.001	0.706	0.970
Median Barrier presence indicator	0.045	0.046	0.980	0.326	-0.045	0.136
Overdispersion parameter	0.627	0.027			0.575	0.683
Number of observations = 2276						
Log likelihood at convergence = -5990.355						
Pseudo R <sup>2</sup> =0.0892						

**Table 34 Nighttime Crash Frequency Model for Virginia Freeway Segments**

Variable	Coefficient	Standard Error	z	P> z	95% Conf. Interval	
					Lower	Higher
Constant	-6.750	0.863	-7.820	<0.001	-8.441	-5.059
Lighting presence indicator	-0.095	0.065	-1.470	0.143	-0.223	0.032
Number of interchanges in segment	0.157	0.057	2.740	0.006	0.045	0.269
Two-lanes per direction indicator	-0.125	0.085	-1.480	0.139	-0.291	0.041
Three-lanes per direction indicator	0.111	0.053	2.090	0.037	0.007	0.215
Right shoulder width (feet)	0.042	0.008	5.530	<0.001	0.027	0.057
Left shoulder width (feet)	-0.022	0.006	-3.660	<0.001	-0.033	-0.010
Percentage of truck traffic	0.004	0.009	0.470	0.637	-0.014	0.023
Median width (feet)	0.002	0.001	3.270	0.001	0.001	0.003
Logarithm of segment length (miles)	0.594	0.023	25.380	<0.001	0.548	0.640
Logarithm of average daily traffic (veh/day)	0.701	0.075	9.320	<0.001	0.554	0.849
Median Barrier presence indicator	0.217	0.051	4.240	<0.001	0.117	0.318
Overdispersion parameter	0.485	0.033			0.426	0.553
Number of observations = 2276						
Log likelihood at convergence = -4201.6594						
Pseudo R <sup>2</sup> =0.1103						

**Table 35 Summary of statistical modeling and descriptive statistics for N/D crash ratios, nighttime crashes, and daytime crashes associated with lighting for VA highway segments**

Number of segments with lighting	Model			Descriptive data: change in night/day ratio
	Change in night/day ratio with lighting	Change in day crashes with lighting	Change in night crashes with lighting	
1968 (79%)	-6.64%	-2.6%	-9.1%	-5.6%

## 4.2 Crash Severity Results

This section contains crash severity distributions for the California and Minnesota intersection databases, Minnesota interchange database, and Washington freeway segment database. The severity distributions are based on the KABCO scale as described previously. Additionally, the crash severity distributions are stratified by sections with and without lighting, and during daytime and nighttime conditions.

### 4.2.1 Intersections

#### 4.2.1.1 Minnesota

Table 36 shows the fatal crash frequency and proportion of total crashes for Minnesota intersections. Table 37 shows the incapacitating crash frequency and proportion of total crashes for Minnesota intersections. Table 38 shows the non-incapacitating crash frequency and proportion of total crashes for Minnesota intersections. Table 39 shows the possible injury crash frequency and proportion of total crashes for Minnesota intersections. Table 40 shows the property-damage only crash frequency and proportion of total crashes for Minnesota intersections. Table 41 shows the unknown crash frequency and proportion of total crashes for Minnesota intersections. When considering all intersection forms, the crash severity distribution is as follows, irrespective of time of day and with or without lighting:

- Fataals: 0.77 percent
- Incapacitating injury: 2.35 percent
- Non-incapacitating injury: 12.45 percent
- Possible injury: 21.82 percent
- Property-damage only: 14.78 percent
- Unknown injury severity: 47.82 percent

When considering nighttime crashes with and without fixed roadway lighting, the proportion of the fatal crashes is higher without lighting than with lighting; the proportion of incapacity injury crashes is higher without lighting than with lighting; the proportion of non-incapacitating injury crashes without lighting is higher than with lighting; the proportion of possible injury crashes without lighting is lower than with lighting; and, the proportion of property-damage only crashes is lower without lighting than with lighting. As such, the severity distribution suggests that the nighttime crash severity is generally lower at intersections with lighting than at those without lighting. Similar changes in the crash severity distribution were also observed during the daytime at intersections with and without fixed roadway lighting, which may indicate that other roadway and traffic control factors that are often associated with lighting are also influencing crash severity. Furthermore, it is worth noting that nearly 50 percent of Minnesota intersection crashes were recorded as unknown injury severity. As such, a conclusion related to the effect of roadway lighting on crash severity is difficult to quantify.

**Table 36 Minnesota Intersection Fatal Crash Severity**

Intersection Type	# fatal					% fatal				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
All intersections	93	44	115	47	299	0.45%	0.72%	1.41%	1.41%	0.77%
All signalized	48	26	1	1	76	0.34%	0.63%	0.34%	1.22%	0.41%
All unsignalized	45	18	114	46	223	0.65%	0.92%	1.45%	1.41%	1.11%
Cross	63	22	71	23	179	0.45%	0.55%	1.96%	1.69%	0.77%
Skew	14	9	12	9	44	0.39%	0.81%	0.95%	1.78%	0.67%
Tee	16	13	32	15	76	0.48%	1.27%	0.98%	1.02%	0.82%
All urban	63	33	9	6	111	0.34%	0.64%	0.54%	1.11%	0.43%
Urban signalized	37	21	1	1	60	0.29%	0.56%	0.45%	1.75%	0.36%
Urban unsignalized	26	12	8	5	51	0.46%	0.82%	0.56%	1.03%	0.56%
Urban signalized cross	26	12	0	0	43	0.46%	0.82%	0.00%	0.00%	0.34%
Urban signalized skew	6	3	1	1	11	0.25%	0.41%	1.89%	12.50%	0.34%
Urban signalized tee	3	3	0	0	6	0.47%	1.49%	0.00%	0.00%	0.68%
Urban unsignalized cross	17	3	3	1	24	0.59%	0.42%	0.62%	0.88%	0.56%
Urban unsignalized skew	3	2	2	1	8	0.43%	0.90%	1.74%	2.50%	0.74%
Urban unsignalized tee	6	7	3	3	19	0.30%	1.34%	0.36%	0.91%	0.51%
All rural	30	11	106	41	188	1.17%	1.19%	1.63%	1.46%	1.45%
Rural signalized	11	5	0	0	16	0.83%	1.14%	0.00%	0.00%	0.85%
Rural unsignalized	19	6	106	41	172	1.52%	1.24%	1.65%	1.48%	1.55%
Rural signalized cross	10	4	0	0	14	1.00%	1.22%	0.00%	0.00%	0.97%
Rural signalized skew	1	1	0	0	2	0.64%	1.89%	0.00%	0.00%	0.93%
Rural signalized tee	0	0	0	0	0	0.00%	0.00%	#DIV/0!	#DIV/0!	0.00%
Rural unsignalized cross	8	0	68	22	98	1.98%	0.00%	2.32%	1.87%	2.09%
Rural unsignalized skew	4	3	9	7	23	1.16%	2.59%	0.82%	1.54%	1.14%
Rural unsignalized tee	7	3	29	12	51	1.40%	1.23%	1.20%	1.05%	1.17%

**Table 37 Minnesota Intersection Incapacitating Injury Crash Severity**

Intersection Type	#incapacitating injury( severe injury)					% incapacitating injury( severe injury)				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
All intersections	376	139	279	106	916	1.80%	2.27%	3.42%	3.17%	2.35%
All signalized	245	89	6	3	352	1.75%	2.14%	2.05%	3.66%	1.88%
All unsignalized	131	50	273	103	564	1.91%	2.56%	3.47%	3.16%	2.80%
Cross	266	92	158	50	575	1.91%	2.32%	4.35%	3.67%	2.48%
Skew	55	23	46	18	143	1.54%	2.06%	3.63%	3.56%	2.19%
Tee	55	24	75	38	198	1.64%	2.34%	2.30%	2.58%	2.15%
All urban	323	117	31	13	493	1.77%	2.25%	1.88%	2.40%	1.90%
Urban signalized	229	81	4	3	324	1.81%	2.18%	1.81%	5.26%	1.92%
Urban unsignalized	94	36	27	10	169	1.67%	2.45%	1.89%	2.06%	1.85%
Urban signalized cross	94	36	2	2	261	1.67%	2.45%	1.32%	4.26%	2.04%
Urban signalized skew	30	16	2	1	50	1.26%	2.21%	3.77%	12.50%	1.56%
Urban signalized tee	6	5	0	0	13	0.93%	2.49%	0.00%	0.00%	1.48%
Urban unsignalized cross	42	22	14	1	81	1.45%	3.05%	2.87%	0.88%	1.90%
Urban unsignalized skew	13	7	1	2	23	1.86%	3.14%	0.87%	5.00%	2.12%
Urban unsignalized tee	39	7	12	7	65	1.92%	1.34%	1.45%	2.11%	1.73%
All rural	53	22	248	93	423	2.06%	2.39%	3.81%	3.32%	3.27%
Rural signalized	16	8	2	0	28	1.21%	1.83%	2.82%	0.00%	1.49%
Rural unsignalized	37	14	246	93	395	2.96%	2.89%	3.82%	3.35%	3.57%
Rural signalized cross	15	7	2	0	26	1.51%	2.14%	3.03%	0.00%	1.81%
Rural signalized skew	1	0	0	0	1	0.64%	0.00%	0.00%	0.00%	0.46%
Rural signalized tee	0	1	0	0	1	0.00%	1.75%	#DIV/0!	#DIV/0!	0.44%
Rural unsignalized cross	16	3	140	47	207	3.95%	2.40%	4.79%	3.99%	4.41%
Rural unsignalized skew	11	0	43	15	69	3.20%	0.00%	3.93%	3.29%	3.41%
Rural unsignalized tee	10	11	63	31	119	2.00%	4.53%	2.61%	2.72%	2.74%

**Table 38 Minnesota Intersection Non-Incapacitating Injury Crash Severity**

Intersection Type	# non-incapacitating injury (visible injury)					% non-incapacitating injury (visible injury)				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
All intersections	2344	736	1270	433	4847	11.25%	12.05%	15.57%	12.96%	12.45%
All signalized	1547	498	52	11	2138	11.08%	11.98%	17.81%	13.41%	11.40%
All unsignalized	797	238	1218	422	2709	11.59%	12.19%	15.49%	12.95%	13.43%
Cross	1576	502	608	188	2914	11.32%	12.64%	16.75%	13.79%	12.57%
Skew	398	121	199	58	781	11.13%	10.84%	15.71%	11.46%	11.97%
Tee	370	113	463	187	1152	11.06%	11.04%	14.20%	12.70%	12.50%
All urban	1999	605	238	51	2934	10.94%	11.66%	14.41%	9.41%	11.29%
Urban signalized	1398	428	41	7	1901	11.06%	11.50%	18.55%	12.28%	11.27%
Urban unsignalized	601	177	197	44	1033	10.68%	12.06%	13.77%	9.07%	11.34%
Urban signalized cross	601	177	21	5	1450	10.68%	12.06%	13.91%	10.64%	11.34%
Urban signalized skew	257	78	14	1	352	10.81%	10.77%	26.42%	12.50%	11.01%
Urban signalized tee	70	21	6	1	99	10.89%	10.45%	35.29%	50.00%	11.24%
Urban unsignalized cross	312	94	71	8	490	10.77%	13.02%	14.58%	7.02%	11.48%
Urban unsignalized skew	73	22	14	3	115	10.44%	9.87%	12.17%	7.50%	10.59%
Urban unsignalized tee	216	61	112	33	428	10.64%	11.66%	13.51%	9.97%	11.39%
All rural	345	131	1032	382	1913	13.41%	14.22%	15.87%	13.65%	14.78%
Rural signalized	149	70	11	4	237	11.26%	16.02%	15.49%	16.00%	12.59%
Rural unsignalized	196	61	1021	378	1676	15.69%	12.60%	15.87%	13.63%	15.15%
Rural signalized cross	116	58	11	3	191	11.65%	17.74%	16.67%	13.04%	13.29%
Rural signalized skew	19	9	0	1	28	12.18%	16.98%	0.00%	50.00%	12.96%
Rural signalized tee	14	4	0	0	18	8.19%	7.02%	#DIV/0!	#DIV/0!	7.86%
Rural unsignalized cross	77	21	505	172	783	19.01%	16.80%	17.26%	14.59%	16.70%
Rural unsignalized skew	49	13	171	53	286	14.24%	11.21%	15.63%	11.62%	14.12%
Rural unsignalized tee	70	27	345	153	607	14.00%	11.11%	14.29%	13.43%	13.95%

**Table 39 Minnesota Intersection Possible Injury Crash Severity**

Intersection Type	# possible injury (pain/complaint)					% possible injury (pain/complaint)				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
All intersections	4701	1248	1867	593	8495	22.56%	20.43%	22.89%	17.75%	21.82%
All signalized	3263	882	75	20	4292	23.37%	21.21%	25.68%	24.39%	22.89%
All unsignalized	1438	366	1792	573	4203	20.91%	18.75%	22.79%	17.58%	20.83%
Cross	3121	815	810	241	5043	22.42%	20.53%	22.32%	17.68%	21.75%
Skew	855	242	310	95	1512	23.91%	21.68%	24.47%	18.77%	23.18%
Tee	725	191	747	257	1940	21.68%	18.65%	22.91%	17.46%	21.05%
All urban	4111	1086	395	107	5765	22.50%	20.93%	23.91%	19.74%	22.19%
Urban signalized	2968	794	56	17	3884	23.48%	21.34%	25.34%	29.82%	23.02%
Urban unsignalized	1143	292	339	90	1881	20.31%	19.89%	23.69%	18.56%	20.65%
Urban signalized cross	1143	292	40	15	2906	20.31%	19.89%	26.49%	31.91%	22.72%
Urban signalized skew	587	165	13	2	773	24.69%	22.79%	24.53%	25.00%	24.18%
Urban signalized tee	164	35	3	0	205	25.51%	17.41%	17.65%	0.00%	23.27%
Urban unsignalized cross	590	137	109	23	865	20.36%	18.98%	22.38%	20.18%	20.27%
Urban unsignalized skew	150	44	29	6	230	21.46%	19.73%	25.22%	15.00%	21.18%
Urban unsignalized tee	403	111	201	61	786	19.85%	21.22%	24.25%	18.43%	20.92%
All rural	590	162	1472	486	2730	22.94%	17.59%	22.63%	17.36%	21.09%
Rural signalized	295	88	19	3	408	22.30%	20.14%	26.76%	12.00%	21.68%
Rural unsignalized	295	74	1453	483	2322	23.62%	15.29%	22.59%	17.41%	20.99%
Rural signalized cross	225	66	17	3	313	22.59%	20.18%	25.76%	13.04%	21.78%
Rural signalized skew	35	10	2	0	47	22.44%	18.87%	40.00%	0.00%	21.76%
Rural signalized tee	35	12	0	0	48	20.47%	21.05%	#DIV/0!	#DIV/0!	20.96%
Rural unsignalized cross	89	18	644	200	959	21.98%	14.40%	22.02%	16.96%	20.45%
Rural unsignalized skew	83	23	266	87	462	24.13%	19.83%	24.31%	19.08%	22.81%
Rural unsignalized tee	123	33	543	196	901	24.60%	13.58%	22.49%	17.21%	20.71%



**Table 40 Minnesota Intersection Property-damage Only Crash Severity**

Intersection Type	# pdo					% pdo				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
All intersections	3219	904	1005	479	5754	15.45%	14.80%	12.32%	14.34%	14.78%
All signalized	2134	605	39	18	2884	15.28%	14.55%	13.36%	21.95%	15.38%
All unsignalized	1085	299	966	461	2870	15.78%	15.32%	12.28%	14.15%	14.22%
Cross	2190	613	429	203	3531	15.73%	15.44%	11.82%	14.89%	15.23%
Skew	517	143	144	59	886	14.46%	12.81%	11.37%	11.66%	13.58%
Tee	512	148	432	217	1337	15.31%	14.45%	13.25%	14.74%	14.50%
All urban	2890	770	220	76	4065	15.82%	14.84%	13.32%	14.02%	15.65%
Urban signalized	1963	549	28	9	2630	15.53%	14.75%	12.67%	15.79%	15.59%
Urban unsignalized	927	221	192	67	1435	16.47%	15.05%	13.42%	13.81%	15.75%
Urban signalized cross	927	221	20	8	2026	16.47%	15.05%	13.25%	17.02%	15.84%
Urban signalized skew	359	96	7	1	478	15.10%	13.26%	13.21%	12.50%	14.95%
Urban signalized tee	92	27	1	0	126	14.31%	13.43%	5.88%	0.00%	14.30%
Urban unsignalized cross	500	121	76	22	733	17.25%	16.76%	15.61%	19.30%	17.17%
Urban unsignalized skew	100	27	14	5	150	14.31%	12.11%	12.17%	12.50%	13.81%
Urban unsignalized tee	327	73	102	40	552	16.11%	13.96%	12.30%	12.08%	14.69%
All rural	329	134	785	403	1689	12.79%	14.55%	12.07%	14.40%	13.05%
Rural signalized	171	56	11	9	254	12.93%	12.81%	15.49%	36.00%	13.50%
Rural unsignalized	158	78	774	394	1435	12.65%	16.12%	12.03%	14.20%	12.97%
Rural signalized cross	126	42	11	8	194	12.65%	12.84%	16.67%	34.78%	13.50%
Rural signalized skew	20	5	0	1	26	12.82%	9.43%	0.00%	50.00%	12.04%
Rural signalized tee	25	9	0	0	34	14.62%	15.79%	#DIV/0!	#DIV/0!	14.85%
Rural unsignalized cross	52	24	322	165	578	12.84%	19.20%	11.01%	13.99%	12.33%
Rural unsignalized skew	38	15	123	52	232	11.05%	12.93%	11.24%	11.40%	11.46%
Rural unsignalized tee	68	39	329	177	625	13.60%	16.05%	13.63%	15.54%	14.36%

**Table 41 Minnesota Intersection Unknown Injury Crash Severity**

Intersection Type	# severity unknown					% severity unknown				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
All intersections	10107	3039	3620	1683	18616	48.50%	49.74%	44.38%	50.37%	47.82%
All signalized	6727	2058	119	29	9009	48.17%	49.49%	40.75%	35.37%	48.05%
All unsignalized	3380	981	3501	1654	9607	49.16%	50.26%	44.52%	50.75%	47.62%
Cross	6704	1926	1553	658	10943	48.16%	48.51%	42.79%	48.28%	47.20%
Skew	1737	578	556	267	3158	48.57%	51.79%	43.88%	52.77%	48.41%
Tee	1666	535	1511	758	4515	49.82%	52.25%	46.35%	51.49%	48.98%
All urban	8882	2578	759	289	12612	48.62%	49.68%	45.94%	53.32%	48.54%
Urban signalized	6046	1848	91	20	8070	47.83%	49.66%	41.18%	35.09%	47.84%
Urban unsignalized	2836	730	668	269	4542	50.40%	49.73%	46.68%	55.46%	49.85%
Urban signalized cross	2836	730	68	17	6105	50.40%	49.73%	45.03%	36.17%	47.73%
Urban signalized skew	1138	366	16	2	1533	47.88%	50.55%	30.19%	25.00%	47.95%
Urban signalized tee	308	110	7	1	432	47.90%	54.73%	41.18%	50.00%	49.04%
Urban unsignalized cross	1437	345	214	59	2075	49.59%	47.78%	43.94%	51.75%	48.62%
Urban unsignalized skew	360	121	55	23	560	51.50%	54.26%	47.83%	57.50%	51.57%
Urban unsignalized tee	1039	264	399	187	1907	51.18%	50.48%	48.13%	56.50%	50.76%
All rural	1225	461	2861	1394	6004	47.63%	50.05%	43.99%	49.80%	46.37%
Rural signalized	681	210	28	9	939	51.47%	48.05%	39.44%	36.00%	49.89%
Rural unsignalized	544	251	2833	1385	5065	43.56%	51.86%	44.04%	49.93%	45.77%
Rural signalized cross	504	150	25	9	699	50.60%	45.87%	37.88%	39.13%	48.64%
Rural signalized skew	80	29	3	0	112	51.28%	54.72%	60.00%	0.00%	51.85%
Rural signalized tee	97	31	0	0	128	56.73%	54.39%	#DIV/0!	#DIV/0!	55.90%
Rural unsignalized cross	163	59	1246	573	2064	40.25%	47.20%	42.60%	48.60%	44.02%
Rural unsignalized skew	159	62	482	242	953	46.22%	53.45%	44.06%	53.07%	47.06%
Rural unsignalized tee	222	130	1105	570	2048	44.40%	53.50%	45.77%	50.04%	47.07%

#### 4.2.1.2 California

Table 42 shows the fatal crash frequency and proportion of total crashes for California intersections. Table 43 shows the incapacitating crash frequency and proportion of total crashes for California intersections. Table 44 shows the non-incapacitating crash frequency and proportion of total crashes for California intersections. Table 45 shows the possible injury crash frequency and proportion of total crashes for California intersections. Table 46 shows the property-damage only crash frequency and proportion of total crashes for California intersections. When considering all intersection forms, the crash severity distribution is as follows, irrespective of time of day and with or without lighting:

- Fataals: 0.85 percent
- Incapacitating injury: 2.47 percent
- Non-incapacitating injury: 14.33 percent
- Possible injury: 25.46 percent
- Property-damage only: 56.69 percent

When considering nighttime crashes with and without fixed roadway lighting, the proportion of the fatal crashes is higher without lighting than with lighting; the proportion of incapacity injury crashes is higher without lighting than with lighting; the proportion of non-incapacitating injury crashes without lighting is higher than with lighting; the proportion of possible injury crashes without lighting is lower than with lighting; and, the proportion of property-damage only crashes is lower without lighting than with lighting. As such, the severity distribution suggests that the nighttime crash severity is generally lower at California intersections with lighting than at those without lighting. Similar trends were observed in the daytime crash severity data, which suggests that others roadway and traffic control features, in addition to lighting, are influencing the crash severity at California intersections.

**Table 42 California Intersection Fatal Crash Severity**

Intersections	# fatal					% fatal				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
all	120	84	132	58	395	0.43%	0.91%	1.90%	2.44%	0.85%
all 4leg	66	57	84	39	246	0.35%	0.86%	2.84%	3.87%	0.83%
all T	46	19	39	10	115	0.64%	0.87%	1.14%	0.85%	0.82%
all stop	83	50	131	58	323	0.66%	1.50%	1.91%	2.48%	1.28%
all signal	37	34	1	0	72	0.24%	0.58%	1.30%	0.00%	0.34%
all Y/offset	8	8	9	9	34	0.48%	1.72%	1.57%	4.79%	1.17%
signal 4leg	31	32	1	0	631	0.24%	0.64%	1.54%	0.00%	3.49%
stop 4leg	35	25	83	39	182	0.57%	1.59%	2.87%	4.00%	1.57%
signal T	6	1	0	0	7	0.31%	0.14%	0.00%	0.00%	0.26%
stop T	40	18	39	10	108	0.77%	1.25%	1.15%	0.85%	0.96%
signal Y/offset	0	1	0	0	1	0.00%	0.74%	#DIV/0!	#DIV/0!	0.19%
stop Y/offset	8	7	9	9	33	0.62%	2.13%	1.57%	4.79%	1.38%

**Table 43 California Intersection Incapacitating Injury Crash Severity**

Intersections	# severe injury					% severe injury				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
all	464	252	286	148	1151	1.66%	2.73%	4.12%	6.24%	2.47%
all 4leg	283	171	135	81	671	1.48%	2.59%	4.57%	8.04%	2.26%
all T	141	74	128	53	396	1.98%	3.40%	3.75%	4.50%	2.83%
all stop	255	114	283	148	800	2.03%	3.41%	4.12%	6.33%	3.17%
all signal	209	138	3	0	351	1.36%	2.34%	3.90%	0.00%	1.64%
all Y/offset	40	7	23	14	84	2.40%	1.51%	4.02%	7.45%	2.88%
signal 4leg	164	113	2	0	1364	1.26%	2.25%	3.08%	0.00%	7.54%
stop 4leg	119	58	133	81	391	1.95%	3.68%	4.61%	8.30%	3.38%
signal T	35	23	1	0	59	1.79%	3.12%	8.33%	0.00%	2.17%
stop T	106	51	127	53	337	2.05%	3.55%	3.73%	4.51%	2.99%
signal Y/offset	10	2	0	0	12	2.62%	1.48%	#DIV/0!	#DIV/0!	2.31%
stop Y/offset	30	5	23	14	72	2.33%	1.52%	4.02%	7.45%	3.01%

**Table 44 California Intersection Non-incapacitating Crash Severity**

Intersections	# visible injury					% visible injury				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
all	3600	1326	1314	433	6677	12.91%	14.36%	18.94%	18.25%	14.33%
all 4leg	2453	916	633	213	4216	12.86%	13.89%	21.44%	21.15%	14.19%
all T	946	350	584	187	2070	13.26%	16.09%	17.11%	15.87%	14.82%
all stop	1752	541	1298	427	4021	13.95%	16.18%	18.92%	18.26%	15.95%
all signal	1848	785	16	6	2656	12.06%	13.33%	20.78%	17.14%	12.43%
all Y/offset	201	60	97	33	391	12.05%	12.93%	16.96%	17.55%	13.42%
signal 4leg	1600	651	13	5	4250	12.33%	12.97%	20.00%	16.13%	23.50%
stop 4leg	853	265	620	208	1946	14.00%	16.80%	21.47%	21.31%	16.83%
signal T	211	113	3	1	328	10.78%	15.33%	25.00%	25.00%	12.08%
stop T	735	237	581	186	1742	14.19%	16.48%	17.08%	15.84%	15.48%
signal Y/offset	37	21	0	0	58	9.69%	15.56%	#DIV/0!	#DIV/0!	11.15%
stop Y/offset	164	39	97	33	333	12.75%	11.85%	16.96%	17.55%	13.91%

**Table 45 California Intersection Possible Injury Crash Severity**

Intersections	# pain/complaint					% pain/complaint				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
all	7478	2424	1490	452	11862	26.82%	26.25%	21.48%	19.05%	25.46%
all 4leg	5229	1822	625	180	7862	27.41%	27.62%	21.16%	17.87%	26.47%
all T	1834	488	730	235	3299	25.70%	22.44%	21.39%	19.95%	23.62%
all stop	3173	743	1473	447	5849	25.27%	22.22%	21.47%	19.12%	23.20%
all signal	4305	1681	17	5	6013	28.10%	28.53%	22.08%	14.29%	28.13%
all Y/offset	415	114	135	37	701	24.88%	24.57%	23.60%	19.68%	24.06%
signal 4leg	3662	1470	14	5	7133	28.21%	29.29%	21.54%	16.13%	39.44%
stop 4leg	1567	352	611	175	2706	25.71%	22.32%	21.16%	17.93%	23.40%
signal T	540	179	3	0	722	27.59%	24.29%	25.00%	0.00%	26.58%
stop T	1294	309	727	235	2577	24.99%	21.49%	21.38%	20.02%	22.90%
signal Y/offset	103	32	0	0	135	26.96%	23.70%	#DIV/0!	#DIV/0!	25.96%
stop Y/offset	312	82	135	37	566	24.26%	24.92%	23.60%	19.68%	23.64%

**Table 46 California Intersection Property Damage Only Crash Severity**

Intersections	# pdo					% pdo				
	with lighting day	with lighting night	without lighting day	without lighting night	total	with lighting day	with lighting night	without lighting day	without lighting night	total
all	16159	5130	3705	1277	26409	57.96%	55.55%	53.40%	53.81%	56.69%
all 4leg	11005	3618	1475	491	16653	57.69%	54.85%	49.95%	48.76%	56.06%
all T	4156	1237	1925	692	8062	58.25%	56.87%	56.40%	58.74%	57.71%
all stop	7268	1890	3665	1253	14169	57.88%	56.52%	53.42%	53.59%	56.20%
all signal	8891	3240	40	24	12240	58.04%	55.00%	51.95%	68.57%	57.26%
all Y/offset	998	275	305	94	1694	59.83%	59.27%	53.32%	50.00%	58.13%
signal 4leg	7497	2743	35	21	12575	57.75%	54.65%	53.85%	67.74%	69.52%
stop 4leg	3508	875	1440	470	6321	57.56%	55.49%	49.86%	48.16%	54.66%
signal T	1162	418	5	3	1594	59.38%	56.72%	41.67%	75.00%	58.69%
stop T	2994	819	1920	689	6468	57.82%	56.95%	56.45%	58.69%	57.48%
signal Y/offset	232	79	0	0	314	60.73%	58.52%	#DIV/0!	#DIV/0!	60.38%
stop Y/offset	766	196	305	94	1380	59.56%	59.57%	53.32%	50.00%	57.64%

#### 4.2.2 *Minnesota Interchanges*

Table 47 shows severity distributions for Minnesota interchanges. When considering all interchange forms, the crash severity distribution is as follows, irrespective of time of day and with or without lighting:

- Fatafs: 0.42 percent
- Incapacitating injury: 0.81 percent
- Non-incapacitating injury: 6.95 percent
- Possible injury: 18.78 percent
- Property-damage only: 21.40 percent
- Unknown severity: 52.09 percent

When considering nighttime crashes with and without fixed roadway lighting, the proportion of the fatal crashes is higher without lighting than with lighting; the proportion of incapacitating injury crashes is higher without lighting than with lighting; the proportion of non-incapacitating injury crashes without lighting is higher than with lighting; the proportion of possible injury crashes without lighting is lower than with lighting; and, the proportion of property-damage only crashes is higher without lighting than with lighting. As such, the severity distribution suggests that the nighttime crash severity is generally lower at Minnesota interchanges with lighting than at those without lighting. Again, similar trends were observed in the daytime crash frequency data, suggesting that other roadway and traffic control features, in addition to lighting, may be influencing the crash severity distribution.

**Table 47 Minnesota Interchange Fatal Crash Severity**

All Interchange Data												
Crash Severity	With Lighting					Without Lighting					Percent	Total
	Day	Percent	Night	Percent	Total	Day	Percent	Night	Percent	Total		
Total Crashes	24293	70.22%	10304	29.78%	34597	1176	60.65%	763	39.35%	1939	100.00%	36536
PDO	5253	21.62%	2136	20.73%	7389	248	21.09%	183	23.98%	431	21.40%	7820
Severity Unknown	12652	52.08%	5299	51.43%	17951	539	45.83%	380	49.80%	919	51.66%	18870
Possible Injury	4688	19.30%	1853	17.98%	6541	213	18.11%	107	14.02%	320	18.78%	6861
Minor Injury	1469	6.05%	848	8.23%	2317	143	12.16%	78	10.22%	221	6.95%	2538
Major Injury	162	0.67%	103	1.00%	265	20	1.70%	10	1.31%	30	0.81%	295
Fatal	69	0.28%	65	0.63%	134	13	1.11%	5	0.66%	18	0.42%	152
Urban Interchanges												
Crash Severity	With Lighting					Without Lighting					Percent	Total
	Day	Percent	Night	Percent	Total	Day	Percent	Night	Percent	Total		
Total Crashes	21872	70.11%	9060	29.04%	31292	189	0.61%	74	0.24%	265	100.00%	31195
PDO	4775	21.83%	1898	20.95%	6794	43	22.75%	17	22.97%	61	21.97%	6733
Severity Unknown	11399	52.12%	4621	51.00%	16161	83	43.92%	33	44.59%	116	52.18%	16277
Possible Injury	4247	19.42%	1662	18.34%	5937	37	19.58%	11	14.86%	49	19.30%	5957
Minor Injury	1260	5.76%	735	8.11%	2022	19	10.05%	12	16.22%	31	6.58%	2026
Major Injury	134	0.61%	94	1.04%	234	5	2.65%	1	1.35%	6	0.77%	234
Fatal	57	0.26%	50	0.55%	108	2	1.06%	0	0.00%	2	0.35%	109
Rural Interchanges												
Crash Severity	With Lighting					Without Lighting					Percent	Total
	Day	Percent	Night	Percent	Total	Day	Percent	Night	Percent	Total		
Total Crashes	2421	44.88%	1244	23.06%	3699	987	18.30%	689	12.77%	1695	100.00%	5394
PDO	478	19.74%	238	19.13%	728	205	20.77%	166	24.09%	378	20.50%	1106
Severity Unknown	1253	51.76%	678	54.50%	1942	456	46.20%	347	50.36%	812	51.06%	2754
Possible Injury	441	18.22%	191	15.35%	638	176	17.83%	96	13.93%	275	16.93%	913
Minor Injury	209	8.63%	113	9.08%	325	124	12.56%	66	9.58%	190	9.55%	515
Major Injury	28	1.16%	9	0.72%	39	15	1.52%	9	1.31%	24	1.17%	63
Fatal	12	0.50%	15	1.21%	27	11	1.11%	5	0.73%	16	0.80%	43
All Diamond Interchanges												
Crash Severity	With Lighting					Without Lighting					Percent	Total
	Day	Percent	Night	Percent	Total	Day	Percent	Night	Percent	Total		
Total Crashes	18190	66.46%	7537	27.54%	25727	979	3.58%	662	2.42%	1641	100.00%	27368
PDO	3891	21.39%	1590	21.10%	5481	210	21.45%	165	24.92%	375	21.40%	5856
Severity Unknown	9528	52.38%	3861	51.23%	13389	453	46.27%	325	49.09%	778	51.76%	14167
Possible Injury	3492	19.20%	1352	17.94%	4844	169	17.26%	94	14.20%	263	18.66%	5107
Minor Injury	1106	6.08%	614	8.15%	1720	119	12.16%	67	10.12%	186	6.96%	1906
Major Injury	123	0.68%	72	0.96%	195	18	1.84%	8	1.21%	26	0.81%	221
Fatal	50	0.27%	48	0.64%	98	10	1.02%	3	0.45%	13	0.41%	111
All Non-diamond Interchanges												
Crash Severity	With Lighting					Without Lighting					Percent	Total
	Day	Percent	Night	Percent	Total	Day	Percent	Night	Percent	Total		
Total Crashes	6103	66.55%	2767	30.17%	8870	199	2.17%	101	1.10%	300	100.00%	9170
PDO	1362	22.32%	546	19.73%	1908	38	19.10%	18	17.82%	56	21.42%	1964
Severity Unknown	3124	51.19%	1438	51.97%	4562	88	44.22%	55	54.46%	143	51.31%	4705
Possible Injury	1196	19.60%	501	18.11%	1697	44	22.11%	13	12.87%	57	19.13%	1754
Minor Injury	363	5.95%	234	8.46%	597	24	12.06%	11	10.89%	35	6.89%	632
Major Injury	39	0.64%	31	1.12%	70	2	1.01%	2	1.98%	4	0.81%	74
Fatal	19	0.31%	17	0.61%	36	3	1.51%	2	1.98%	5	0.45%	41

4.2.3 Freeway Segments

4.2.3.1 Washington

Table 48 shows severity distribution for Washington roadway segments with and without continuous freeway lighting. The crash severity distribution indicates the following:

- The proportion of fatal crashes is higher along roadway sections without lighting when compared to roadway sections with lighting, both during the day and at night;
- The proportion of disabling injury crashes is higher along roadway sections without lighting when compared to roadway sections with lighting, both during the day and at night;
- The proportion of evident injury crashes is higher along roadway sections without lighting when compared to roadway sections with lighting, both during the day and at night;



- The proportion of possible injury crashes is lower along roadway sections without lighting when compared to roadway sections with lighting, both during the day and at night;
- The proportion of property damage only (PDO) crashes is lower along roadway sections without lighting when compared to roadway sections with lighting, both during the day and at night.

**Table 48 Severity Distribution for Washington Freeway Segments**

Day/Night	Total Length (miles)	Lighting Indicator	Severity Level	COUNTS	Mean Count Per Mile Per Year	Severity Proportion
Day	760.93	With Lighting	PDO	10430	2.74	63.86%
			Possible injury	4816	1.27	29.49%
			Evident injury	954	0.25	5.84%
			Disabling injury	112	0.03	0.69%
			Fatal	21	0.01	0.13%
			Total Crashes	16333	4.29	100.00%
	767.92	Without Lighting	PDO	18689	4.87	63.42%
			Possible injury	7685	2.00	26.08%
			Evident injury	2666	0.69	9.05%
			Disabling injury	325	0.08	1.10%
			Fatal	104	0.03	0.35%
			Total Crashes	29469	7.68	100.00%
Night	760.93	With Lighting	PDO	3193	0.84	62.85%
			Possible injury	1341	0.35	26.40%
			Evident injury	466	0.12	9.17%
			Disabling injury	59	0.02	1.16%
			Fatal	21	0.01	0.41%
			Total Crashes	5080	1.34	100.00%
	767.92	Without Lighting	PDO	7506	1.95	65.11%
			Possible injury	2414	0.63	20.94%
			Evident injury	1308	0.34	11.35%
			Disabling injury	203	0.05	1.76%
			Fatal	97	0.03	0.84%
			Total Crashes	11528	3.00	100.00%

#### 4.2.3.2 Oregon and Virginia Freeway Segments

The database acquired from Monsere and Grile (2002) contained only crash frequency data, so a severity distribution for freeway segments with and without lighting in Oregon was not developed for the present study. The freeway segment crash data from Virginia contained severity information at three levels: fatal, injury, and PDO. The severity distributions for locations with and without continuous freeway lighting, stratified by daytime and nighttime periods, are shown in Table 49.

**Table 49 Crash Severity Distribution for Virginia Freeway Segments**

Lighting Presence	Fatal Crashes (%)		Injury Crashes (%)		PDO Crashes (%)	
	Daytime	Nighttime	Daytime	Nighttime	Daytime	Nighttime
Without Lighting	0.1	0.1	23.3	11.0	45.8	19.8
With Lighting	0.1	0.2	24.4	9.6	47.2	18.5

Based on the results provided in Table 49, it appears that locations with lighting experience fewer nighttime injury and PDO crashes than segments without lighting, but the proportion of fatal crashes is higher at night with lighting than without lighting. During the day, locations with continuous freeway lighting experience more PDO and injury crashes than locations without lighting; the proportion of fatal crashes with and without lighting is equal during the daytime.

## 5. SUMMARY AND CONCLUSIONS

The results of the negative binomial regression models indicate that the presence of fixed roadway lighting appears to be associated with a safety benefit at intersections included in the present analysis. Using the nighttime and daytime negative binomial crash frequency models for all intersections in California, the difference in the night-day ratios between intersections with lighting and those without lighting is a 22.51 percent lower expected total crash frequency (range is 18 to 26 percent reduction based on 95<sup>th</sup>-percentile confidence interval). This suggests that the presence of lighting is associated with a net safety benefit. At nearly all levels of the analysis taxonomy for California intersections, the difference in the night-day crash ratios between lighted and unlighted intersections, computed using the negative binomial regression models, indicated a mean 20 to 30 percent reduction in the night-day crash ratio with lighting. The only exceptions were at signalized tee-intersections and signalized wye- or offset-intersections. The log-linear night-day ratio models, and the night-day descriptive statistics, both produced results that showed a less favorable safety benefit attributed to roadway lighting at intersections. As noted earlier in this report, computing night-day ratios using only crash data does not control for differences in the roadway geometry or traffic control features across intersections. Use of the night-day ratio log-linear models resulted in a significant reduction in the sample size used to estimate the safety effects of roadway lighting. As such, results obtained from the negative binomial regression models appear most suitable in the present study.

For Minnesota intersections, an expected 11.9 percent reduction (5 to 18 percent reduction based on 95<sup>th</sup>-percentile confidence interval) in the night-day total crash ratio was computed using the negative binomial regression models for all intersections. At most levels of the analysis taxonomy, the models predict a reduction in the night-day total crash ratio of between 5 and 26 percent. For urban signalized skew intersections, urban signalized t-intersections, urban unsignalized cross-intersections, rural signalized intersections, and rural unsignalized t-intersections, the change in the night-day crash ratio was positive, indicating that the presence of roadway lighting is associated with a crash increase. At most levels of the analysis taxonomy, the night-day ratios computed using only the crash data showed a more favorable safety benefit from the presence of roadway lighting when compared to the negative binomial regression models. The log-linear models exhibited inconsistent results when compared to the negative binomial regression models. Again, the sample size used to estimate the log-linear models was significantly lower than the sample used to estimate the negative binomial models. As such, results from the negative binomial regression models appear more suitable to compute the change in the night-day ratios for Minnesota intersections with and without lighting.

At Minnesota interchange locations, a mean 7.77 percent decrease (6 percent increase to 20 percent reduction based on 95<sup>th</sup>-percentile confidence interval) in the night-day ratio at locations with lighting was computed using the negative binomial regression parameter estimates. Similar results were obtained when considering the effects of full or partial interchange lighting. At lower levels of the analysis taxonomy, the safety effects of lighting interchange areas were inconsistent. Computing the night-day ratios using only the crash data showed more favorable safety effects attributed to

roadway lighting when compared to the negative binomial regression models, but do not control for the various roadway features present at the analysis locations. As such, the safety effects from roadway lighting at interchange locations that were computed using the negative binomial regression models appear more suitable in the present analysis. Based on the confidence interval around the point estimate of the night-day ratio computed from the negative binomial regression model, the presence of interchange lighting does not appear to have a significant benefit on total crashes.

The freeway segment analysis in Washington indicated that continuous freeway lighting was associated with an expected 4.3 percent increase (2 percent reduction to 11 percent increase based on 95<sup>th</sup>-percentile confidence interval) in the night-day total crash ratio along segments with lighting when compared to segments without lighting. This result was obtained when accounting for interchange and overpass locations, as well as segments with only point lighting. When excluding point lighting locations from the analysis, the models were used to predict an expected 10.4 percent decrease in the night-day ratio for continuous lighting in the median only. If lighting was located only on the right-side of the freeway segment, the models predicted an expected 0.3 percent increase in the night-day ratio on segments with lighting relative to segments without lighting. If continuous lighting was located along both sides of the freeway segment, the negative binomial models predicted an expected 15.0 percent decrease in the night-day crash ratio when comparing lighted segments to those that were not lighted. Similar trends were observed when stratifying the sample into urban and rural segments, where an expected safety benefit was computed for segments with lighting on the median- or on both sides, but an expected increase in the night-day ratio was computed when lighting was present only on the right-side of the freeway segment. When excluding freeway segments with point lighting, interchanges, and overpasses, the sample size was reduced by nearly 90 percent, resulting in large standard errors for the lighting presence parameter estimates. The night-day ratios computed using the crash data generally showed a significant safety benefit for fixed roadway lighting; however, these ratios do not account for the roadway geometrics present along roadway segments.

The freeway segment analyses using data from Oregon and Virginia produced consistent results. In Oregon, a mean 6.7 percent decrease (34.4 percent decrease to 32.6 increase based on 95<sup>th</sup>-percentile confidence interval) in the night-day ratio was computed from the negative binomial regression models, indicating a net safety benefit on roadway segments with continuous freeway lighting. Similarly, the negative binomial regression models estimated using data from Virginia indicated a mean 6.6 percent decrease (5.6 percent increase to 17.5 reduction based on 95<sup>th</sup>-percentile confidence interval) in the night-day ratio for segments with continuous lighting relative to segments without lighting. The night-day ratios computed using only the crash data from Oregon and Virginia indicated that the night-day ratios were lower on segments with continuous lighting when compared to segments without lighting by 19.0 and 5.6 percent, respectively. Based on the continuous freeway lighting analysis using data from Oregon, Virginia, and Washington, the confidence intervals around the mean safety estimates do not suggest that continuous freeway lighting reduces total crash frequency.

In the present analysis, it was assumed that fixed roadway lighting would not be associated with daytime crash frequencies. In many of the models, however, the expected number of daytime crashes was higher at locations with lighting when

compared to locations without lighting. This suggests that there are other factors associated with the presence of lighting that were not included in the statistical models. Separate nighttime crash frequency models were estimated to address this issue, assuming that these same unobserved factors would be captured in the lighting presence indicator. The night-day crash ratios were then computed as the metric to determine the association with lighting presence and safety. Future research should attempt to include additional factors in statistical models that may be associated with roadway lighting to address the issue of daytime crash frequencies being associated with the presence of fixed roadway lighting.

The severity distributions computed for intersections, interchanges, and freeway segments generally indicated that the presence of lighting reduced the proportion of the most severe crashes at night; however, this effect was offset by similar reductions at the same locations during the daytime. As such, future research is recommended to determine the change in the severity distributions at locations with and without lighting. This may include estimation of statistical models that not only include the presence of lighting, but also include driver-related factors as well as various geometric and traffic control features present at locations with and without lighting.

As shown in the literature review for NCHRP Project 5-19 (Rea et al. [2009]), past research appears to agree that the presence of roadway lighting is a safety benefit. Generally, published research appears to converge on a 20 to 30 percent reduction in nighttime crashes. This nighttime crash reduction was confirmed by Elvik (1995) in a meta-analysis on the safety effects of roadway lighting. Based on 37 published studies, conducted over a 40-year period, in 11 different countries, the author found that total nighttime crashes are reduced by approximately 23 percent on roadways with lighting. The safety benefits of roadway lighting appeared to be more favorable at junctions (30 percent reduction in nighttime crashes) than on motorways (23 percent reduction in nighttime crashes). The same trends were found in the present study where the safety benefits of lighting presence was greater at intersections than at interchanges or along freeway segments.

Harwood et al. (2007) developed an accident modification factor (AMF) for total crashes using the meta-analysis by Elvik (1995). The AMF is proposed for inclusion in the first edition of the Highway Safety Manual to predict the expected crash frequency along roadway segments, and at-grade intersections, on urban and suburban arterials. Using combined data from Michigan and Minnesota as an example, and adjusting for the proportion of crashes that occur at night, Harwood et al. (2007) illustrated that an appropriate AMF for total crashes on roadway segments with lighting would be approximately 0.96 (i.e., 4 percent reduction in total crashes after installing roadway lighting). Similarly, an AMF for at-grade intersections was estimated using combined data from Minnesota and North Carolina. A 4 percent reduction in total crashes was shown to be an appropriate safety effect estimate for intersection lighting (AMF = 0.96). Assuming that approximately 25 percent of the average daily traffic travels during nighttime periods (which is consistent with Hallmark et al. [2004] and Box [1970]), similar safety effects for roadway lighting at intersections would be obtained from the present study; however, the association between continuous lighting presence and safety on freeway segments is not as apparent in the present study.

In addition to estimating statistical models to determine the effects of lighting on crash severity, additional research is recommended based on the results of the present study. These include:

- Only one state transportation agency was identified that maintained lighting presence data in electronic roadway inventory files for interchanges. Future research should consider estimating statistical models of crash frequency to evaluate the safety effects of full and partial interchange lighting.
- The statistical analyses in the present study considered the presence of roadway lighting. Lighting design parameters (e.g., illuminance, uniformity, and spacing) were either not included in state transportation agency roadway inventory files or were not linkable to electronic roadway data. As such, future research should consider the effects of lighting design on safety. The visibility analyses included in a separate report for NCHRP Project 5-19 addressed the effects of lighting design using relative visual performance (see Bullough et al. [2009]).
- Consider an observational before-after study to determine the effects of roadway lighting presence and lighting-quality at intersections, interchanges, and along roadway segments.

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## **APPENDIX A**

### **CALIFORNIA INTERSECTION MODELING RESULTS**

Table A.1 Nighttime Crash Frequency at Signalized Intersections

```

Negative binomial regression
Dispersion = mean
Log likelihood = -9418.158
Number of obs = 8494
LR chi2(11) = 694.26
Prob > chi2 = 0.0000
Pseudo R2 = 0.0355
    
```

	total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
fourleg		.6554975	.0992076	6.61	0.000	.4610541	.8499408
tee		.1436888	.1063655	1.35	0.177	-.0647837	.3521614
lght_typ		-.1613575	.2036699	-0.79	0.428	-.5605432	.2378281
mlltncha		-.0742938	.060697	-1.22	0.221	-.1932577	.0446701
ml_right		.1335361	.0369311	3.62	0.000	.0611524	.2059197
ltres		-.3252026	.1159291	-2.81	0.005	-.5524194	-.0979857
mllan34		-.0474021	.0573136	-0.83	0.408	-.1597347	.0649304
mllan56		.0724366	.0695266	1.04	0.297	-.0638331	.2087062
med_ind		.1412432	.0474102	2.98	0.003	.0483209	.2341655
lnmladt		-.0010204	.0150798	-0.07	0.946	-.0305764	.0285355
lnxsadt		.2631832	.0147547	17.84	0.000	.2342646	.2921019
_cons		-3.007431	.2833551	-10.61	0.000	-3.562797	-2.452066
-----							
/lnalpha		-.3339442	.0551903			-.4421153	-.2257731
-----							
alpha		.7160937	.0395215			.6426755	.7978991
-----							

Likelihood-ratio test of alpha=0: chibar2(01) = 754.16 Prob>=chibar2 = 0.000

Table A.2 Daytime Crash Frequency at Signalized Intersections

```

Negative binomial regression
Dispersion = mean
Log likelihood = -15030.774
Number of obs = 8494
LR chi2(11) = 947.80
Prob > chi2 = 0.0000
Pseudo R2 = 0.0306
    
```

	total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
fourleg		.5981006	.0668191	8.95	0.000	.4671376	.7290636
tee		.0803543	.0716736	1.12	0.262	-.0601235	.220832
lght_typ		.1201818	.1502131	0.80	0.424	-.1742305	.4145941
mlltncha		-.1416663	.0430823	-3.29	0.001	-.226106	-.0572266
ml_right		.1198676	.026973	4.44	0.000	.0670014	.1727338
ltres		-.3284141	.0816943	-4.02	0.000	-.488532	-.1682963
mllan34		.0946837	.0410342	2.31	0.021	.0142581	.1751093
mllan56		.1987008	.0501077	3.97	0.000	.1004916	.29691
med_ind		.0238777	.0336804	0.71	0.478	-.0421347	.0898901
lnmladt		.0001506	.0109886	0.01	0.989	-.0213868	.0216879
lnxsadt		.1903048	.0101652	18.72	0.000	.1703814	.2102282
_cons		-1.62843	.2043929	-7.97	0.000	-2.029033	-1.227827
-----							
/lnalpha		-.5327527	.0343557			-.6000886	-.4654167
-----							
alpha		.586987	.0201664			.548763	.6278734
-----							

Likelihood-ratio test of alpha=0: chibar2(01) = 2514.64 Prob>=chibar2 = 0.000

Table A.3 Nighttime Crash Frequency at Stop-controlled Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -16816.184
Number of obs   = 53533
LR chi2(11)    = 3277.66
Prob > chi2    = 0.0000
Pseudo R2     = 0.0888
    
```

total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
fourleg	.401659	.0547377	7.34	0.000	.294375	.5089429
tee	-.1550745	.0539808	-2.87	0.004	-.2608748	-.0492741
lght_typ	-.1621588	.0350366	-4.63	0.000	-.2308292	-.0934883
mlltncha	.3992548	.0390965	10.21	0.000	.3226272	.4758825
ml_right	.3322819	.0488217	6.81	0.000	.2365931	.4279707
ltres	-.6373171	.1022618	-6.23	0.000	-.8377466	-.4368876
mllan34	.1005901	.0443774	2.27	0.023	.013612	.1875682
mllan56	.2214548	.0799682	2.77	0.006	.06472	.3781897
med_ind	-.0704971	.0476471	-1.48	0.139	-.1638836	.0228894
lnmladt	.1412268	.0129257	10.93	0.000	.1158928	.1665607
lnxsadt	.4181169	.0121408	34.44	0.000	.3943214	.4419123
_cons	-6.105697	.1313854	-46.47	0.000	-6.363207	-5.848186
/lnalpha	.4618308	.0552108			.3536196	.5700419
alpha	1.586977	.0876182			1.424213	1.768341

Likelihood-ratio test of alpha=0: chibar2(01) = 788.24 Prob>=chibar2 = 0.000

Table A.4 Daytime Crash Frequency at Stop-controlled Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -36501.459
Number of obs   = 53533
LR chi2(11)    = 8902.22
Prob > chi2    = 0.0000
Pseudo R2     = 0.1087
    
```

total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
fourleg	.3894287	.0341533	11.40	0.000	.3224895	.4563679
tee	-.2067008	.0333834	-6.19	0.000	-.2721312	-.1412705
lght_typ	.1011913	.0220822	4.58	0.000	.0579111	.1444716
mlltncha	.3799336	.0246128	15.44	0.000	.3316935	.4281738
ml_right	.2539307	.033018	7.69	0.000	.1892165	.3186448
ltres	-.6805289	.0621382	-10.95	0.000	-.8023174	-.5587403
mllan34	.1448535	.027588	5.25	0.000	.0907821	.198925
mllan56	.1285369	.0516046	2.49	0.013	.0273937	.2296801
med_ind	-.1485493	.0300572	-4.94	0.000	-.2074604	-.0896382
lnmladt	.1540217	.0080697	19.09	0.000	.1382054	.169838
lnxsadt	.433753	.0077028	56.31	0.000	.4186557	.4488502
_cons	-5.17563	.0827528	-62.54	0.000	-5.337823	-5.013438
/lnalpha	.2834054	.0250182			.2343707	.3324402
alpha	1.327643	.0332153			1.264113	1.394367

Likelihood-ratio test of alpha=0: chibar2(01) = 5099.01 Prob>=chibar2 = 0.000

Table A.5 Nighttime Crash Frequency at Four-leg Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -14350.041
Number of obs   = 20510
LR chi2(10)    = 3704.42
Prob > chi2    = 0.0000
Pseudo R2     = 0.1143
    
```

total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
sig_cntl	.5288767	.0415668	12.72	0.000	.4474074	.6103461
lght_typ	-.1138911	.0470836	-2.42	0.016	-.2061733	-.021609
mlltncha	.3125752	.0419108	7.46	0.000	.2304316	.3947188
ml_right	.1111264	.0357633	3.11	0.002	.0410317	.1812211
ltres	-.7742412	.1415403	-5.47	0.000	-1.051655	-.4968274
mllan34	-.0234593	.0439194	-0.53	0.593	-.1095398	.0626212
mllan56	.0221758	.06187	0.36	0.720	-.099087	.1434387
med_ind	.0508374	.0414549	1.23	0.220	-.0304127	.1320874
lnmladt	.05566	.0126223	4.41	0.000	.0309207	.0803992
lnxsadt	.3325413	.0123962	26.83	0.000	.3082452	.3568374
_cons	-4.341071	.1248567	-34.77	0.000	-4.585786	-4.096357
/lnalpha	-.1734326	.0489634			-.2693991	-.0774661
alpha	.8407738	.0411671			.7638384	.9254584

Likelihood-ratio test of alpha=0: chibar2(01) = 984.73 Prob>=chibar2 = 0.000

Table A.6 Daytime Crash Frequency at Four-leg Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -26249.872
Number of obs   = 20510
LR chi2(10)    = 5799.96
Prob > chi2    = 0.0000
Pseudo R2     = 0.0995
    
```

total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
sig_cntl	.187809	.027907	6.73	0.000	.1331123	.2425057
lght_typ	.1752955	.030076	5.83	0.000	.1163476	.2342434
mlltncha	.2491665	.0274265	9.08	0.000	.1954115	.3029215
ml_right	.0633353	.0265985	2.38	0.017	.0112033	.1154674
ltres	-.897536	.095591	-9.39	0.000	-1.084891	-.7101811
mllan34	.0417367	.029421	1.42	0.156	-.0159273	.0994007
mllan56	.0143057	.0444446	0.32	0.748	-.0728042	.1014156
med_ind	-.0430422	.0289342	-1.49	0.137	-.0997523	.0136679
lnmladt	.0704389	.0087204	8.08	0.000	.0533472	.0875306
lnxsadt	.3380876	.0084302	40.10	0.000	.3215647	.3546106
_cons	-3.393503	.0857402	-39.58	0.000	-3.56155	-3.225455
/lnalpha	-.2179179	.0264014			-.2696637	-.1661722
alpha	.8041915	.0212318			.7636363	.8469004

Likelihood-ratio test of alpha=0: chibar2(01) = 4661.13 Prob>=chibar2 = 0.000

Table A.7 Nighttime Crash Frequency at Tee Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -10073.871
Number of obs   = 35804
LR chi2(10)    = 2316.20
Prob > chi2     = 0.0000
Pseudo R2      = 0.1031
    
```

total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
sig_cntl	.3146287	.0629599	5.00	0.000	.1912295	.4380279
lght_typ	-.1239344	.0484833	-2.56	0.011	-.2189598	-.028909
mlltncha	.3382613	.0538702	6.28	0.000	.2326776	.4438449
ml_right	.3461815	.0590751	5.86	0.000	.2303963	.4619666
ltres	-.3495211	.1027186	-3.40	0.001	-.5508458	-.1481964
mllan34	.147679	.0615274	2.40	0.016	.0270876	.2682704
mllan56	.3503216	.0903172	3.88	0.000	.1733031	.5273401
med_ind	-.0832786	.0640409	-1.30	0.193	-.2087964	.0422393
lnmladt	.128157	.0168282	7.62	0.000	.0951743	.1611397
lnxsadt	.4266044	.0155883	27.37	0.000	.3960519	.4571569
_cons	-6.216904	.1571157	-39.57	0.000	-6.524845	-5.908963
/lnalpha	.3882756	.0755745			.2401523	.5363989
alpha	1.474436	.1114298			1.271443	1.709838

Likelihood-ratio test of alpha=0: chibar2(01) = 429.94 Prob>=chibar2 = 0.000

Table A.8 Daytime Crash Frequency at Tee Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -21476.462
Number of obs   = 35804
LR chi2(10)    = 5277.13
Prob > chi2     = 0.0000
Pseudo R2      = 0.1094
    
```

total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
sig_cntl	.0781033	.0443835	1.76	0.078	-.0088868	.1650934
lght_typ	.0995101	.030219	3.29	0.001	.040282	.1587382
mlltncha	.3949195	.0337583	11.70	0.000	.3287545	.4610844
ml_right	.3122609	.0406806	7.68	0.000	.2325284	.3919934
ltres	-.3895633	.0645438	-6.04	0.000	-.5160667	-.2630598
mllan34	.2855989	.0383835	7.44	0.000	.2103687	.3608291
mllan56	.4102358	.0591423	6.94	0.000	.294319	.5261525
med_ind	-.1923247	.0403944	-4.76	0.000	-.2714963	-.113153
lnmladt	.1484817	.0106329	13.96	0.000	.1276416	.1693219
lnxsadt	.4055048	.0099145	40.90	0.000	.3860727	.4249369
_cons	-5.244946	.0998629	-52.52	0.000	-5.440673	-5.049218
/lnalpha	.2721221	.0355222			.2024999	.3417443
alpha	1.312747	.0466316			1.22446	1.4074

Likelihood-ratio test of alpha=0: chibar2(01) = 2347.15 Prob>=chibar2 = 0.000

Table A.9 Nighttime Crash Frequency at Wye/Offset Intersections

Negative binomial regression		Number of obs	=	5713
		LR chi2(10)	=	375.84
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -1889.0062	Pseudo R2	=	0.0905

total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
sig_cntl	.1382316	.1394519	0.99	0.322	-.135089	.4115523
lght_typ	-.0387059	.1186723	-0.33	0.744	-.2712994	.1938876
mlltncha	.1813172	.1363355	1.33	0.184	-.0858954	.4485298
ml_right	.4834917	.1485161	3.26	0.001	.1924056	.7745778
ltres	-.5252292	.2335949	-2.25	0.025	-.9830669	-.0673916
mllan34	.3755989	.1329871	2.82	0.005	.1149489	.6362489
mllan56	.3966216	.2023704	1.96	0.050	-.0000171	.7932603
med_ind	.174923	.1479011	1.18	0.237	-.1149579	.4648039
lnmladt	.172588	.0395285	4.37	0.000	.0951135	.2500625
lnxsadt	.294424	.0375335	7.84	0.000	.2208597	.3679883
_cons	-5.841688	.3679982	-15.87	0.000	-6.562952	-5.120425
/lnalpha	.4034995	.1643047			.0814681	.7255308
alpha	1.497054	.2459731			1.084879	2.065827

Likelihood-ratio test of alpha=0: chibar2(01) = 87.04 Prob>=chibar2 = 0.000

Table A.10 Daytime Crash Frequency at Wye/Offset Intersections

Negative binomial regression		Number of obs	=	5713
		LR chi2(10)	=	925.92
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -4115.6751	Pseudo R2	=	0.1011

total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
sig_cntl	-.099207	.0998925	-0.99	0.321	-.2949927	.0965787
lght_typ	.3263588	.0738495	4.42	0.000	.1816164	.4711012
mlltncha	.4383632	.0864683	5.07	0.000	.2688885	.6078379
ml_right	.278881	.1033665	2.70	0.007	.0762864	.4814756
ltres	-.4981119	.162377	-3.07	0.002	-.8163649	-.1798589
mllan34	.0165101	.0812287	0.20	0.839	-.1426953	.1757156
mllan56	-.11168	.1399532	-0.80	0.425	-.3859832	.1626231
med_ind	-.1365893	.0967888	-1.41	0.158	-.3262918	.0531132
lnmladt	.1927221	.0249097	7.74	0.000	.1438999	.2415442
lnxsadt	.3699301	.0239308	15.46	0.000	.3230265	.4168337
_cons	-5.24207	.2358371	-22.23	0.000	-5.704303	-4.779838
/lnalpha	.4031829	.0688749			.2681905	.5381752
alpha	1.496581	.1030768			1.307596	1.712878

Likelihood-ratio test of alpha=0: chibar2(01) = 706.78 Prob>=chibar2 = 0.000

Table A.11 Nighttime Crash Frequency at Signalized, Four-leg Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -7633.9591
Number of obs   =      6290
LR chi2(9)      =      306.47
Prob > chi2     =      0.0000
Pseudo R2      =      0.0197
    
```

total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	-.5049901	.2375554	-2.13	0.034	-.9705902	-.03939
mlltncha	-.068523	.0671141	-1.02	0.307	-.2000641	.0630181
ml_right	.1262114	.0403309	3.13	0.002	.0471644	.2052585
ltres	-.7417399	.1628686	-4.55	0.000	-1.060956	-.4225234
mllan34	-.0763841	.0639554	-1.19	0.232	-.2017344	.0489662
mllan56	.0109408	.0780011	0.14	0.888	-.1419385	.1638201
med_ind	.1434854	.0517888	2.77	0.006	.0419813	.2449896
lnmladt	-.0005751	.0165033	-0.03	0.972	-.0329209	.0317707
lnxsadt	.2475643	.0164267	15.07	0.000	.2153685	.2797601
_cons	-1.846162	.3090309	-5.97	0.000	-2.451852	-1.240473
/lnalpha	-.3641492	.0595617			-.4808881	-.2474104
alpha	.6947875	.0413827			.6182341	.7808202

Likelihood-ratio test of alpha=0: chibar2(01) = 647.24 Prob>=chibar2 = 0.000

Table A.12 Daytime Crash Frequency at Signalized, Four-leg Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -11927.461
Number of obs   =      6290
LR chi2(9)      =      356.05
Prob > chi2     =      0.0000
Pseudo R2      =      0.0147
    
```

total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	-.2513577	.1855702	-1.35	0.176	-.6150686	.1123532
mlltncha	-.1666395	.0478218	-3.48	0.000	-.2603685	-.0729104
ml_right	.1150011	.0295832	3.89	0.000	.0570191	.1729831
ltres	-.8812696	.1164033	-7.57	0.000	-1.109416	-.6531234
mllan34	.0569525	.0460816	1.24	0.216	-.0333657	.1472708
mllan56	.1069438	.0565362	1.89	0.059	-.0038651	.2177527
med_ind	.0679526	.0370869	1.83	0.067	-.0047364	.1406416
lnmladt	-.0086112	.0120889	-0.71	0.476	-.032305	.0150827
lnxsadt	.1803001	.011464	15.73	0.000	.1578311	.2027691
_cons	-.4489477	.2341807	-1.92	0.055	-.9079335	.0100381
/lnalpha	-.5839137	.037697			-.6577984	-.5100289
alpha	.5577114	.021024			.5179905	.6004782

Likelihood-ratio test of alpha=0: chibar2(01) = 2105.80 Prob>=chibar2 = 0.000

Table A.13 Nighttime Crash Frequency at Signalized, Tee Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -1473.8499
Number of obs   =      1830
LR chi2(9)     =      135.54
Prob > chi2    =      0.0000
Pseudo R2     =      0.0440
    
```

total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	.7275625	.5351088	1.36	0.174	-.3212315	1.776357
mlltncha	-.2259463	.1682567	-1.34	0.179	-.5557234	.1038308
ml_right	.2266572	.0979418	2.31	0.021	.0346948	.4186197
ltres	-.0823061	.2198585	-0.37	0.708	-.5132208	.3486085
mllan34	.1397559	.1488895	0.94	0.348	-.1520623	.431574
mllan56	.5019131	.1713783	2.93	0.003	.1660179	.8378084
med_ind	.0082778	.1386999	0.06	0.952	-.2635691	.2801246
lnmladt	.0068662	.0409892	0.17	0.867	-.0734711	.0872035
lnxsadt	.3242814	.0363365	8.92	0.000	.2530632	.3954996
_cons	-4.341065	.7015611	-6.19	0.000	-5.7161	-2.966031
/lnalpha	-.1355293	.1567485			-.4427508	.1716922
alpha	.8732536	.1368812			.6422673	1.187312

Likelihood-ratio test of alpha=0: chibar2(01) = 93.32 Prob>=chibar2 = 0.000

Table A.14 Daytime Crash Frequency at Signalized, Tee Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -2517.4135
Number of obs   =      1830
LR chi2(9)     =      223.74
Prob > chi2    =      0.0000
Pseudo R2     =      0.0425
    
```

total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	.7394551	.3236864	2.28	0.022	.1050415	1.373869
mlltncha	-.0270067	.1182443	-0.23	0.819	-.2587613	.2047479
ml_right	.2046344	.0660745	3.10	0.002	.0751308	.3341381
ltres	.1452398	.1524908	0.95	0.341	-.1536367	.4441163
mllan34	.3306574	.1011209	3.27	0.001	.1324641	.5288508
mllan56	.7193201	.1175442	6.12	0.000	.4889377	.9497024
med_ind	-.2202703	.0898425	-2.45	0.014	-.3963583	-.0441824
lnmladt	.0427851	.0278128	1.54	0.124	-.0117269	.0972972
lnxsadt	.2560985	.0231037	11.08	0.000	.2108161	.301381
_cons	-3.33104	.445962	-7.47	0.000	-4.205109	-2.456971
/lnalpha	-.5270193	.10119			-.7253481	-.3286906
alpha	.590362	.0597387			.484156	.7198657

Likelihood-ratio test of alpha=0: chibar2(01) = 235.80 Prob>=chibar2 = 0.000



Table A.15 Nighttime Crash Frequency at Signalized, Wye/Offset Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood = -285.40374
Number of obs   =      374
LR chi2(9)      =      14.41
Prob > chi2     =      0.1086
Pseudo R2      =      0.0246
    
```

total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	13.81879	1925.948	0.01	0.994	-3760.969	3788.607
mlltncha	.2204247	.2880579	0.77	0.444	-.3441585	.7850079
ml_right	-.1203247	.2831407	-0.42	0.671	-.6752701	.4346208
ltres	.3096953	.4256384	0.73	0.467	-.5245407	1.143931
mllan34	-.1751865	.3149083	-0.56	0.578	-.7923954	.4420224
mllan56	-.2313904	.389041	-0.59	0.552	-.9938968	.5311159
med_ind	.2738449	.2408188	1.14	0.255	-.1981514	.7458411
lnmladt	.0195551	.0863385	0.23	0.821	-.1496653	.1887755
lnxsadt	.3350836	.1196279	2.80	0.005	.1006173	.5695499
_cons	-17.96947	1925.948	-0.01	0.993	-3792.757	3756.818
/lnalpha	-1.229114	.7676671			-2.733714	.2754857
alpha	.2925516	.2245822			.0649775	1.31717

Likelihood-ratio test of alpha=0: chibar2(01) = 2.40 Prob>=chibar2 = 0.061

Table A.16 Daytime Crash Frequency at Signalized, Wye/Offset Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood = -519.1899
Number of obs   =      374
LR chi2(9)      =      9.57
Prob > chi2     =      0.3864
Pseudo R2      =      0.0091
    
```

total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	17.2033	2137.189	0.01	0.994	-4171.61	4206.016
mlltncha	-.172803	.2113692	-0.82	0.414	-.5870791	.241473
ml_right	.086472	.2292985	0.38	0.706	-.3629449	.5358888
ltres	.0585445	.3208794	0.18	0.855	-.5703676	.6874565
mllan34	-.1181909	.2312985	-0.51	0.609	-.5715276	.3351458
mllan56	-.082538	.2929073	-0.28	0.778	-.6566257	.4915497
med_ind	-.1603016	.1900674	-0.84	0.399	-.5328269	.2122237
lnmladt	.0325573	.0693752	0.47	0.639	-.1034155	.1685301
lnxsadt	-.0512632	.0845659	-0.61	0.544	-.2170093	.114483
_cons	-16.75143	2137.189	-0.01	0.994	-4205.564	4172.062
/lnalpha	-.0692543	.1818956			-.4257631	.2872545
alpha	.9330894	.1697248			.6532711	1.332763

Likelihood-ratio test of alpha=0: chibar2(01) = 89.10 Prob>=chibar2 = 0.000

Table A.17 Nighttime Crash Frequency at Stop-controlled, Four-leg Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -6627.6334
Number of obs   = 14220
LR chi2(9)     = 945.76
Prob > chi2    = 0.0000
Pseudo R2      = 0.0666
    
```

total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	-.2105725	.0531903	-3.96	0.000	-.3148236	-.1063214
mlltncha	.4510264	.0564552	7.99	0.000	.3403763	.5616765
ml_right	.1918961	.0721481	2.66	0.008	.0504885	.3333037
ltres	-1.592226	.3506561	-4.54	0.000	-2.2795	-.904953
mllan34	-.004084	.0635918	-0.06	0.949	-.1287216	.1205537
mllan56	-.0161918	.1362645	-0.12	0.905	-.2832654	.2508817
med_ind	-.0720557	.068174	-1.06	0.291	-.2056743	.0615628
lnmladt	.1135378	.0198063	5.73	0.000	.0747183	.1523574
lnxsadt	.4223719	.0191829	22.02	0.000	.3847742	.4599696
_cons	-5.409494	.1926972	-28.07	0.000	-5.787174	-5.031814
/lnalpha	.2864056	.0810798			.1274921	.4453192
alpha	1.331632	.1079686			1.135976	1.560988

Likelihood-ratio test of alpha=0: chibar2(01) = 348.32 Prob>=chibar2 = 0.000

Table A.18 Daytime Crash Frequency at Stop-controlled, Four-leg Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -14012.257
Number of obs   = 14220
LR chi2(9)     = 2477.00
Prob > chi2    = 0.0000
Pseudo R2      = 0.0812
    
```

total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	.0698004	.0342752	2.04	0.042	.0026222	.1369785
mlltncha	.3410019	.0360695	9.45	0.000	.270307	.4116968
ml_right	.1145468	.0489348	2.34	0.019	.0186364	.2104572
ltres	-1.348291	.1756806	-7.67	0.000	-1.692619	-1.003963
mllan34	.0178318	.0403769	0.44	0.659	-.0613054	.0969691
mllan56	-.0964315	.0897491	-1.07	0.283	-.2723364	.0794734
med_ind	-.1423488	.0439456	-3.24	0.001	-.2284805	-.056217
lnmladt	.12549	.0125462	10.00	0.000	.1008999	.1500802
lnxsadt	.4551796	.0123439	36.87	0.000	.430986	.4793732
_cons	-4.555415	.1233449	-36.93	0.000	-4.797166	-4.313663
/lnalpha	.1264685	.0365949			.0547438	.1981933
alpha	1.134814	.0415284			1.05627	1.219198

Likelihood-ratio test of alpha=0: chibar2(01) = 2416.02 Prob>=chibar2 = 0.000

Table A.19 Nighttime Crash Frequency at Stop-controlled, Tee Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -8561.7788
Number of obs   = 33974
LR chi2(9)     = 1452.15
Prob > chi2    = 0.0000
Pseudo R2      = 0.0782
    
```

total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	-.1379249	.0500687	-2.75	0.006	-.2360577	-.039792
mlltncha	.3628024	.0577889	6.28	0.000	.2495382	.4760667
ml_right	.437131	.0714038	6.12	0.000	.2971822	.5770797
ltres	-.5735366	.1237676	-4.63	0.000	-.8161167	-.3309566
mllan34	.1529334	.0675056	2.27	0.023	.0206248	.2852419
mllan56	.308699	.109907	2.81	0.005	.0932851	.5241128
med_ind	-.0969483	.0714655	-1.36	0.175	-.2370182	.0431215
lnmladt	.1479407	.0185004	8.00	0.000	.1116807	.1842008
lnxsadt	.4333521	.0171742	25.23	0.000	.3996912	.467013
_cons	-6.433075	.1719839	-37.41	0.000	-6.770157	-6.095993
/lnalpha	.5629813	.0863542			.3937301	.7322325
alpha	1.7559	.1516294			1.4825	2.079718

Likelihood-ratio test of alpha=0: chibar2(01) = 326.49 Prob>=chibar2 = 0.000

Table A.20 Daytime Crash Frequency at Stop-controlled, Tee Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -18845.79
Number of obs   = 33974
LR chi2(9)     = 3929.44
Prob > chi2    = 0.0000
Pseudo R2      = 0.0944
    
```

total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	.0917047	.031311	2.93	0.003	.0303362	.1530733
mlltncha	.3992568	.0359823	11.10	0.000	.3287328	.4697807
ml_right	.3762739	.0481978	7.81	0.000	.2818079	.4707399
ltres	-.5917986	.0746105	-7.93	0.000	-.7380325	-.4455648
mllan34	.2881039	.0414825	6.95	0.000	.2067996	.3694082
mllan56	.3185721	.0694732	4.59	0.000	.1824072	.4547371
med_ind	-.1829326	.0444345	-4.12	0.000	-.2700226	-.0958425
lnmladt	.1615991	.0114958	14.06	0.000	.1390677	.1841304
lnxsadt	.4189914	.0108194	38.73	0.000	.3977857	.4401971
_cons	-5.434232	.1078528	-50.39	0.000	-5.645619	-5.222844
/lnalpha	.4060604	.0381587			.3312707	.48085
alpha	1.500893	.0572721			1.392737	1.617449

Likelihood-ratio test of alpha=0: chibar2(01) = 2049.71 Prob>=chibar2 = 0.000

Table A.21 Nighttime Crash Frequency at Stop-controlled, Wye/Offset Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -1588.087
Number of obs   =      5339
LR chi2(9)     =      263.29
Prob > chi2    =      0.0000
Pseudo R2      =      0.0765
    
```

total_n	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	-.0660367	.1240162	-0.53	0.594	-.3091041	.1770307
mlltncha	.1481959	.1601022	0.93	0.355	-.1655986	.4619904
ml_right	.6147544	.1734669	3.54	0.000	.2747656	.9547433
ltres	-.80907	.2823511	-2.87	0.004	-1.362468	-.2556721
mllan34	.41918	.1498961	2.80	0.005	.1253889	.712971
mllan56	.5454333	.2449523	2.23	0.026	.0653357	1.025531
med_ind	.1716879	.1827129	0.94	0.347	-.1864228	.5297986
lnmladt	.202322	.04431	4.57	0.000	.115476	.2891679
lnxsadt	.2969429	.0409108	7.26	0.000	.2167592	.3771267
_cons	-6.120546	.4100147	-14.93	0.000	-6.92416	-5.316932
/lnalpha	.7480604	.1660624			.422584	1.073537
alpha	2.112898	.3508729			1.525899	2.925709

Likelihood-ratio test of alpha=0: chibar2(01) = 96.66 Prob>=chibar2 = 0.000

Table A.22 Daytime Crash Frequency at Stop-controlled, Wye/Offset Intersections

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -52663.208
Number of obs   =      62027
LR chi2(9)     =     16139.25
Prob > chi2    =      0.0000
Pseudo R2      =      0.1329
    
```

total_d	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
lght_typ	.2132609	.0202835	10.51	0.000	.1735059	.2530159
mlltncha	.3462093	.0207068	16.72	0.000	.3056247	.3867939
ml_right	.1835214	.0225001	8.16	0.000	.1394219	.2276208
ltres	-.6691504	.0479764	-13.95	0.000	-.7631824	-.5751184
mllan34	.1862352	.0224141	8.31	0.000	.1423042	.2301661
mllan56	.2010967	.0345704	5.82	0.000	.13334	.2688534
med_ind	-.1212837	.0232834	-5.21	0.000	-.1669183	-.0756491
lnmladt	.1087546	.0065631	16.57	0.000	.0958912	.1216181
lnxsadt	.4369189	.0056419	77.44	0.000	.425861	.4479769
_cons	-4.793478	.0609838	-78.60	0.000	-4.913004	-4.673952
/lnalpha	.0841143	.0196956			.0455116	.122717
alpha	1.087753	.021424			1.046563	1.130564

Likelihood-ratio test of alpha=0: chibar2(01) = 8767.45 Prob>=chibar2 = 0.000

..

Table A.23 Log-linear Regression Model for Signalized Intersections

Source	SS	df	MS	Number of obs = 2862		
Model	16.9726993	11	1.54297267	F( 11, 2850)	=	2.89
Residual	1521.87591	2850	.533991546	Prob > F	=	0.0009
				R-squared	=	0.0110
				Adj R-squared	=	0.0072
Total	1538.84861	2861	.537870886	Root MSE	=	.73075

lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
fourleg	-.0248632	.091186	-0.27	0.785	-.2036603	.1539339
tee	.1184383	.097799	1.21	0.226	-.0733258	.3102023
lght_typ	-.1692033	.1838822	-0.92	0.358	-.529759	.1913523
mlltncha	.1376608	.050519	2.72	0.006	.0386032	.2367183
ml_right	-.0338712	.0308321	-1.10	0.272	-.0943267	.0265843
ltres	.1856594	.0973058	1.91	0.056	-.0051375	.3764563
mllan34	-.0288585	.0489818	-0.59	0.556	-.1249018	.0671848
mllan56	-.1192405	.0596474	-2.00	0.046	-.2361969	-.0022841
med_ind	.0038051	.0398946	0.10	0.924	-.0744202	.0820303
lnmladt	.0168799	.0128388	1.31	0.189	-.0082943	.0420542
lnxsadt	-.0068811	.0120363	-0.57	0.568	-.0304818	.0167197
_cons	-.5153513	.2541477	-2.03	0.043	-1.013683	-.0170193

Table A.24 Log-linear Regression Model for Stop-controlled Intersections

Source	SS	df	MS	Number of obs = 2434		
Model	47.1188764	11	4.28353422	F( 11, 2422)	=	10.92
Residual	949.96769	2422	.39222448	Prob > F	=	0.0000
				R-squared	=	0.0473
				Adj R-squared	=	0.0429
Total	997.086566	2433	.409817742	Root MSE	=	.62628

lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
fourleg	-.027735	.0482123	-0.58	0.565	-.1222767	.0668067
tee	.1366073	.0491061	2.78	0.005	.0403131	.2329015
lght_typ	-.0397144	.0286861	-1.38	0.166	-.0959662	.0165374
mlltncha	-.1036154	.0310491	-3.34	0.001	-.164501	-.0427299
ml_right	-.1113747	.0376771	-2.96	0.003	-.1852572	-.0374921
ltres	-.099561	.1031391	-0.97	0.334	-.3018111	.1026891
mllan34	-.0198821	.0366091	-0.54	0.587	-.0916704	.0519062
mllan56	.0658324	.0618016	1.07	0.287	-.0553572	.1870219
med_ind	.0824447	.0383825	2.15	0.032	.0071787	.1577106
lnmladt	-.0080601	.0109749	-0.73	0.463	-.0295812	.013461
lnxsadt	-.053084	.0105822	-5.02	0.000	-.073835	-.032333
_cons	.0593277	.1233526	0.48	0.631	-.1825598	.3012152

Table A.25 Log-linear Regression Model for Four-leg Intersections

Source	SS	df	MS	Number of obs = 3685		
Model	18.0103642	10	1.80103642	F( 10, 3674)	=	3.49
Residual	1897.54582	3674	.516479537	Prob > F	=	0.0001
				R-squared	=	0.0094
				Adj R-squared	=	0.0067
Total	1915.55618	3684	.519966391	Root MSE	=	.71867

lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
sig_cntl	.0160636	.0348445	0.46	0.645	-.0522529	.0843801
lght_typ	-.1013809	.0437119	-2.32	0.020	-.1870829	-.0156788
mlltncha	.0025133	.035542	0.07	0.944	-.0671707	.0721972
ml_right	-.0272455	.028883	-0.94	0.346	-.0838739	.0293829
ltres	.3896218	.1230157	3.17	0.002	.1484359	.6308076
mllan34	.0047167	.0376054	0.13	0.900	-.0690129	.0784462
mllan56	-.0680349	.0515628	-1.32	0.187	-.1691295	.0330596
med_ind	.0419774	.0343829	1.22	0.222	-.0254341	.1093888
lnmladt	.0083342	.0107623	0.77	0.439	-.0127665	.029435
lnxsadt	-.0266843	.0105334	-2.53	0.011	-.0473361	-.0060325
_cons	-.3179901	.1179695	-2.70	0.007	-.5492823	-.0866979

Table A.26 Log-linear Regression Model for Tee Intersections

Source	SS	df	MS	Number of obs = 1346		
Model	15.1518978	10	1.51518978	F( 10, 1335)	=	4.34
Residual	465.623755	1335	.348781839	Prob > F	=	0.0000
				R-squared	=	0.0315
				Adj R-squared	=	0.0243
Total	480.775653	1345	.357454017	Root MSE	=	.59058

lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
sig_cntl	.0330864	.0453837	0.73	0.466	-.0559447	.1221175
lght_typ	.0121986	.0408293	0.30	0.765	-.067898	.0922952
mlltncha	-.0966428	.0436406	-2.21	0.027	-.1822544	-.0110312
ml_right	-.1039917	.0423755	-2.45	0.014	-.1871216	-.0208619
ltres	-.226885	.0830885	-2.73	0.006	-.3898833	-.0638867
mllan34	-.0629741	.0502112	-1.25	0.210	-.1614756	.0355274
mllan56	-.0428029	.068051	-0.63	0.529	-.1763013	.0906956
med_ind	.0358372	.0502453	0.71	0.476	-.0627311	.1344054
lnmladt	-.0081721	.0142625	-0.57	0.567	-.0361515	.0198073
lnxsadt	-.0356675	.0125423	-2.84	0.005	-.0602723	-.0110627
_cons	.1036945	.1401085	0.74	0.459	-.1711624	.3785513

Table A.27 Log-linear Regression Model for Wye/Offset Intersections

Source	SS	df	MS	Number of obs = 265		
Model	8.89087976	10	.889087976	F( 10, 254)	=	2.04
Residual	110.569707	254	.435313807	Prob > F	=	0.0297
				R-squared	=	0.0744
				Adj R-squared	=	0.0380
Total	119.460587	264	.452502222	Root MSE	=	.65978

lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
sig_cntl	.0149772	.1204366	0.12	0.901	-.2222044	.2521588
lght_typ	-.1013449	.1068806	-0.95	0.344	-.31183	.1091402
mlltncha	-.136959	.1197977	-1.14	0.254	-.3728822	.0989642
ml_right	-.2157577	.1238242	-1.74	0.083	-.4596107	.0280952
ltres	-.1788878	.2434754	-0.73	0.463	-.6583756	.3005999
mllan34	.0616837	.1160478	0.53	0.596	-.1668548	.2902222
mllan56	-.0092139	.1765997	-0.05	0.958	-.357	.3385723
med_ind	.244236	.1304688	1.87	0.062	-.0127024	.5011743
lnmladt	.0321734	.0379101	0.85	0.397	-.0424847	.1068316
lnxsadt	-.0597779	.038963	-1.53	0.126	-.1365095	.0169537
_cons	-.3012334	.3977018	-0.76	0.449	-1.084447	.4819797

Table A.28 Log-linear Regression Model for Signalized, Four-leg Intersections

Source	SS	df	MS	Number of obs = 2440		
Model	12.9393148	9	1.43770164	F( 9, 2430)	=	2.60
Residual	1343.28828	2430	.552793531	Prob > F	=	0.0055
				R-squared	=	0.0095
				Adj R-squared	=	0.0059
Total	1356.22759	2439	.556058874	Root MSE	=	.7435

lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
lght_typ	-.1632917	.1933548	-0.84	0.398	-.542449	.2158657
mlltncha	.1362408	.0562272	2.42	0.015	.0259826	.2464991
ml_right	-.0295993	.033879	-0.87	0.382	-.0960341	.0368354
ltres	.5124301	.1363291	3.76	0.000	.2450968	.7797633
mllan34	-.0082609	.0547896	-0.15	0.880	-.1157001	.0991782
mllan56	-.0881594	.0674173	-1.31	0.191	-.2203607	.0440418
med_ind	.0032415	.0441165	0.07	0.941	-.0832684	.0897514
lnmladt	.0217055	.0141249	1.54	0.124	-.0059925	.0494035
lnxsadt	-.0083862	.0132726	-0.63	0.528	-.0344129	.0176406
_cons	-.6043408	.2553279	-2.37	0.018	-1.105024	-.1036579

Table A.29 Log-linear Regression Model for Signalized, Tee Intersections

Source	SS	df	MS	Number of obs = 355		
Model	6.52279844	9	.724755382	F( 9, 345)	=	1.80
Residual	138.65555	345	.401900145	Prob > F	=	0.0665
				R-squared	=	0.0449
				Adj R-squared	=	0.0200
Total	145.178349	354	.410108329	Root MSE	=	.63396

lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
lght_typ	-.330324	.6368789	-0.52	0.604	-1.582978	.9223301
mlltncha	.1668343	.1256287	1.33	0.185	-.0802603	.4139289
ml_right	-.1061384	.0749063	-1.42	0.157	-.253469	.0411921
ltres	-.0682121	.1617449	-0.42	0.673	-.3863424	.2499182
mllan34	-.1408728	.1124026	-1.25	0.211	-.3619535	.0802078
mllan56	-.29711	.1288979	-2.31	0.022	-.5506347	-.0435853
med_ind	.0191749	.1010198	0.19	0.850	-.1795174	.2178671
lnmladt	-.0392368	.0320805	-1.22	0.222	-.1023347	.0238612
lnxsadt	.0014542	.0288016	0.05	0.960	-.0551946	.0581029
_cons	.3647468	.7485085	0.49	0.626	-1.107468	1.836961

Table A.30 Log-linear Regression Model for Signalized, Wye/Offset Intersections

Source	SS	df	MS	Number of obs = 67		
Model	2.91249828	8	.364062285	F( 8, 58)	=	0.76
Residual	27.6489861	58	.476706657	Prob > F	=	0.6357
				R-squared	=	0.0953
				Adj R-squared	=	-0.0295
Total	30.5614844	66	.463052794	Root MSE	=	.69044

lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
lght_typ	(dropped)					
mlltncha	.1265767	.27745	0.46	0.650	-.4287999	.6819532
ml_right	.226762	.2897694	0.78	0.437	-.3532745	.8067986
ltres	-.2447303	.3586895	-0.68	0.498	-.9627253	.4732647
mllan34	.0720703	.3760762	0.19	0.849	-.6807279	.8248685
mllan56	-.3251513	.4459435	-0.73	0.469	-1.217804	.5675015
med_ind	.1595017	.2480575	0.64	0.523	-.3370393	.6560426
lnmladt	.1029183	.0882738	1.17	0.248	-.073781	.2796176
lnxsadt	-.1066517	.1158036	-0.92	0.361	-.3384577	.1251544
_cons	-.8388531	1.178598	-0.71	0.479	-3.198074	1.520368



Table A.31 Log-linear Regression Model for Stop-controlled, Four-leg Intersections

Source	SS	df	MS	Number of obs = 1245		
Model	13.7265927	9	1.52517697	F( 9, 1235)	=	3.47
Residual	542.943217	1235	.439630135	Prob > F	=	0.0003
				R-squared	=	0.0247
				Adj R-squared	=	0.0176
Total	556.66981	1244	.44748377	Root MSE	=	.66305

lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
lght_typ	-.0685009	.0433443	-1.58	0.114	-.1535375	.0165357
mlltncha	-.0899448	.0443243	-2.03	0.043	-.1769041	-.0029856
ml_right	-.0561153	.0582001	-0.96	0.335	-.1702973	.0580668
_ltres	.0594111	.3906558	0.15	0.879	-.7070114	.8258335
mllan34	.0074574	.0520551	0.14	0.886	-.0946689	.1095837
mllan56	-.0475031	.1006917	-0.47	0.637	-.2450489	.1500427
med_ind	.1042379	.0544429	1.91	0.056	-.0025728	.2110487
lnmladt	-.01566	.0161861	-0.97	0.333	-.0474152	.0160953
lnxsadt	-.0647212	.0173652	-3.73	0.000	-.0987898	-.0306526
_cons	.1652048	.1815345	0.91	0.363	-.1909453	.5213549

Table A.32 Log-linear Regression Model for Stop-controlled, Tee Intersections

Source	SS	df	MS	Number of obs = 991		
Model	15.4030131	9	1.7114459	F( 9, 981)	=	5.28
Residual	318.180234	981	.324342746	Prob > F	=	0.0000
				R-squared	=	0.0462
				Adj R-squared	=	0.0374
Total	333.583247	990	.336952774	Root MSE	=	.56951

lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
lght_typ	.0012878	.040256	0.03	0.974	-.07771	.0802856
mlltncha	-.1333039	.0459362	-2.90	0.004	-.2234485	-.0431593
ml_right	-.118027	.0521548	-2.26	0.024	-.2203748	-.0156791
_ltres	-.1492342	.1054754	-1.41	0.157	-.3562175	.0577492
mllan34	-.0643944	.0564923	-1.14	0.255	-.1752541	.0464653
mllan56	.1170564	.0836932	1.40	0.162	-.047182	.2812947
med_ind	.0363149	.0576537	0.63	0.529	-.0768238	.1494537
lnmladt	-.0039525	.0157358	-0.25	0.802	-.0348321	.0269271
lnxsadt	-.0410495	.0137836	-2.98	0.003	-.0680982	-.0140008
_cons	.1160649	.1526169	0.76	0.447	-.1834281	.415558

Table A.33 Log-linear Regression Model for Stop-controlled, Wye/Offset Intersections

Source	SS	df	MS	Number of obs = 198		
Model	9.45788023	9	1.05087558	F( 9, 188)	=	2.49
Residual	79.2371569	188	.421474239	Prob > F	=	0.0103
-----				R-squared	=	0.1066
-----				Adj R-squared	=	0.0639
Total	88.6950371	197	.450228615	Root MSE	=	.64921
-----						
lnntday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
lght_typ	-.1011074	.1060858	-0.95	0.342	-.3103789	.108164
mlltncha	-.128923	.137109	-0.94	0.348	-.3993928	.1415468
ml_right	-.3186755	.1428198	-2.23	0.027	-.6004109	-.0369402
ltres	.203484	.3901212	0.52	0.603	-.5660935	.9730616
mllan34	.0705385	.127736	0.55	0.581	-.1814415	.3225184
mllan56	.1699066	.2074821	0.82	0.414	-.2393855	.5791987
med_ind	.1914675	.1625482	1.18	0.240	-.1291853	.5121204
lnmladt	.0176642	.0421658	0.42	0.676	-.0655148	.1008431
lnxsadt	-.0545003	.0411127	-1.33	0.187	-.1356018	.0266012
_cons	-.1899423	.4336625	-0.44	0.662	-1.045412	.6655275
-----						

## **APPENDIX B**

### **MINNESOTA INTERSECTION MODELING RESULTS**

Table B1. Day Crash Frequency Model for All Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:10:04AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                22058   |
| Iterations completed                  20     |
| Log likelihood function                -27087.49 |
| Restricted log likelihood              -30979.15 |
| Chi squared                           7783.324 |
| Degrees of freedom                    1      |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.53264106  .15084148  -43.308  .0000
LNADTMAJ  .60061020   .01546967  38.825   .0000   8.52246180
LNADTMN   .16030383   .00735881  21.784   .0000   6.98494400
LIGHTING  .04758165   .03059577   1.555    .1199   .45752108
SKEW      .48770956   .03066339  15.905   .0000   .11342823
URBSUB    -.09952432   .02931312  -3.395   .0007   .48077795
SIGNALIZ  .64559033   .03058379  21.109   .0000   .14629613
HIGHSP50  -.15982583   .02174191  -7.351   .0000   .67014235
PER       -.00926586   .00278935  -3.322   .0009   8.59552611
DEPRESS   .08544284   .03359337   2.543    .0110   .12911415
NOACCON   -.04216732   .03818598  -1.104   .2695   .93634962
LSHPAV    -.11804647   .04224130  -2.795   .0052   .46559072
RSHPAV    .08085443   .04143621   1.951    .0510   .51287515
Dispersion parameter for count data model
Alpha     .94974485   .02361081  40.225   .0000

```

Table B2. Night Crash Frequency Model for All Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:10:47AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                22058  |
| Iterations completed                 18     |
| Log likelihood function               -15168.45 |
| Restricted log likelihood             -15887.89 |
| Chi squared                          1438.897 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.88625456  .20593927  -33.438  .0000
LNADTMAJ  .57217224   .02138705   26.753   .0000   8.52246180
LNADTMN   .12658194   .01027589   12.318   .0000   6.98494400
LIGHTING  -.07917456   .04244971   -1.865   .0622   .45752108
SKEW      .48549137   .03980885   12.196   .0000   .11342823
URBSUB    -.42133795   .04005058   -10.520  .0000   .48077795
SIGNALIZ  .71287769   .04140312   17.218   .0000   .14629613
HIGHSP50  -.11296275   .02915918   -3.874   .0001   .67014235
PER       -.01699813   .00385689   -4.407   .0000   8.59552611
DEPRESS   .17152343   .04295123   3.993    .0001   .12911415
NOACCON   -.01600660   .04711328   -.340    .7340   .93634962
LSHPAV    -.29194832   .05344464   -5.463   .0000   .46559072
RSHPAV    .21655019   .05242544   4.131    .0000   .51287515
Dispersion parameter for count data model
Alpha     .89631324   .04077399   21.982   .0000

```

Table B3. Day Crash Frequency Model for All Signalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:14:42AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                3227   |
| Iterations completed                 17     |
| Log likelihood function               -7420.663 |
| Restricted log likelihood             -8202.862 |
| Chi squared                          1564.398 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.74859828  .30509550  -22.120  .0000
LNADTMAJ  .67589263   .03217919  21.004   .0000   9.70895835
LNADTMN   .16882637   .01929906   8.748    .0000   9.02913538
LIGHTING  -.00314848   .08748358   -.036    .9713   .96870158
SKEW      .22739053   .03958161   5.745    .0000   .17415556
URBSUB    .04366528   .04690217   .931     .3519   .89092036
HIGHSP50  -.03657944   .02842000   -1.287   .1981   .61140378
PER       -.00449086   .00465688   -.964    .3349   5.55126106
DEPRESS   .10611267   .04337423   2.446    .0144   .26216300
NOACCON   -.12100355   .03829957   -3.159   .0016   .83885962
LSHPAV    -.08452831   .04831751   -1.749   .0802   .39727301
RSHPAV    .00404509   .04111404   .098     .9216   .54942671
Alpha     Dispersion parameter for count data model
          .32707037   .01558563   20.985   .0000

```

Table B4. Night Crash Frequency Model for All Signalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:15:09AM. |
| Dependent variable                    TOTAL_N |
| Weighting variable                    None    |
| Number of observations                 3227   |
| Iterations completed                   17     |
| Log likelihood function                -4459.628 |
| Restricted log likelihood              -4578.791 |
| Chi squared                           238.3262 |
| Degrees of freedom                     1      |
| Prob[ChiSqd > value] =                 .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -8.93674705  .44658154  -20.011  .0000
LNADTMAJ  .72543708   .04801223  15.109   .0000   9.70895835
LNADTMN   .23698629   .03131641   7.567    .0000   9.02913538
LIGHTING  -.05647396   .13346751   -.423    .6722   .96870158
SKEW      .33593750   .05731117   5.862    .0000   .17415556
URBSUB    -.10493485   .06597372   -1.591   .1117   .89092036
HIGHSP50  -.03639427   .04071996   -.894    .3714   .61140378
PER       -.02507615   .00698033   -3.592   .0003   5.55126106
DEPRESS   .00822407   .06067522   .136     .8922   .26216300
NOACCON   -.08038171   .05271473   -1.525   .1273   .83885962
LSHPAV    -.08380479   .06779798   -1.236   .2164   .39727301
RSHPAV    .15855726   .05798045   2.735    .0062   .54942671
Dispersion parameter for count data model
Alpha     .33765043   .03166679   10.663   .0000

```

Table B5. Day Crash Frequency Model for All Unsignalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:15:52AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                18831  |
| Iterations completed                 17     |
| Log likelihood function               -19163.23 |
| Restricted log likelihood             -22656.42 |
| Chi squared                          6986.380 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.45883774  .18977032  -34.035  .0000
LNADTMAJ  .58971787   .01897214  31.083   .0000   8.31913620
LNADTMN   .15788576   .00854233  18.483   .0000   6.63463836
LIGHTING  .06392618   .03746466   1.706    .0880   .36992194
SKEW      .59747159   .04198203  14.232   .0000   .10302161
URBSUB    -.12247154   .03739590  -3.275    .0011   .41049334
HIGHSP50  -.21469146   .02916637  -7.361    .0000   .68020817
PER       -.00950971   .00344301  -2.762    .0057   9.11721074
DEPRESS   .09720011   .04849047   2.005    .0450   .10631406
NOACCON   .00935651   .06182603   .151     .8797   .95305613
LSHPAV    -.18944322   .06808325  -2.783    .0054   .47729807
RSHPAV    .17108417   .06876060   2.488    .0128   .50661144
          Dispersion parameter for count data model
Alpha     1.58900005   .04289051  37.048    .0000

```



Table B6. Night Crash Frequency Model for All Unsignalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:16:18AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                18831  |
| Iterations completed                 18     |
| Log likelihood function              -10515.34 |
| Restricted log likelihood             -11208.37 |
| Chi squared                          1386.060 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =              .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.49687303  .25532202  -25.446  .0000
LNADTMAJ  .53760734   .02598646  20.688   .0000   8.31913620
LNADTMN   .10851344   .01158771  9.365    .0000   6.63463836
LIGHTING  -.01348695   .05076050  -.266    .7905   .36992194
SKEW      .60107219   .05464859  10.999   .0000   .10302161
URBSUB    -.49207514   .05099836  -9.649   .0000   .41049334
HIGHSP50  -.15329308   .03954312  -3.877   .0001   .68020817
PER       -.01402336   .00466530  -3.006   .0026   9.11721074
DEPRESS   .22888717   .06250214  3.662    .0003   .10631406
NOACCON   .01821295   .07827623  .233     .8160   .95305613
LSHPAV    -.34988871   .08885618  -3.938   .0001   .47729807
RSHPAV    .24753759   .09032665  2.740    .0061   .50661144
          Dispersion parameter for count data model
Alpha     1.68204391   .08420331  19.976   .0000

```

Table B7. Day Crash Frequency Model for All Cross Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:18:09AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                10593  |
| Iterations completed                 18     |
| Log likelihood function               -14147.74 |
| Restricted log likelihood             -15753.35 |
| Chi squared                          3211.219 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.84660749  .19295887  -35.482  .0000
LNADTMAJ  .16994546   .05403770   3.145   .0017   8.48707935
LNADTMN   .65880736   .05706381  11.545   .0000   8.00819948
LIGHTING  -.02453100   .04419007   -.555   .5788   .53129425
URBSUB    -.06277456   .04123673   -1.522   .1279   .53856320
SIGNALIZ  .61660836   .03559440  17.323   .0000   .22713112
HIGHSP50  -.09131889   .02733207   -3.341   .0008   .68129897
PER       -.00675841   .00353626   -1.911   .0560   8.81875288
DEPRESS   -.01364508   .04266265   -.320   .7491   .12640423
NOACCON   -.09042185   .04643478   -1.947   .0515   .94043236
LSHPAV    .03645914   .05189697   .703    .4823   .37609742
RSHPAV    -.03532071   .04839407   -.730   .4655   .42934013
          Dispersion parameter for count data model
Alpha     .64669086   .02360382   27.398   .0000

```

Table B8. Night Crash Frequency Model for All Cross Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:18:29AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                10593  |
| Iterations completed                 18     |
| Log likelihood function               -7703.160 |
| Restricted log likelihood             -7985.448 |
| Chi squared                          564.5753 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -7.24568341  .27843559  -26.023  .0000
LNADTMAJ  .11395738   .07582519   1.503   .1329   8.48707935
LNADTMN   .65289618   .07966015   8.196   .0000   8.00819948
LIGHTING  -.18302131   .06449057   -2.838   .0045   .53129425
URBSUB    -.34594228   .05809517   -5.955   .0000   .53856320
SIGNALIZ  .71005197   .05252644   13.518   .0000   .22713112
HIGHSP50  -.08502325   .03846411   -2.210   .0271   .68129897
PER       -.02113041   .00521960   -4.048   .0001   8.81875288
DEPRESS   .09992351   .05737490   1.742   .0816   .12640423
NOACCON   -.02821129   .05978772   -.472   .6370   .94043236
LSHPAV    -.17006592   .06867861   -2.476   .0133   .37609742
RSHPAV    .19918602   .06338407   3.143   .0017   .42934013
          Dispersion parameter for count data model
Alpha     .62873297   .04340109   14.487   .0000

```

Table B9. Day Crash Frequency Model for All Skew Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:19:02AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                2502   |
| Iterations completed                 17     |
| Log likelihood function              -3816.239 |
| Restricted log likelihood             -4562.848 |
| Chi squared                          1493.219 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =              .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.83649774  .45373582  -15.067  .0000
LNADTMAJ  .62852968   .04620484  13.603   .0000   8.63901733
LNADTMN   .25091759   .02794492   8.979    .0000   6.52253795
LIGHTING  .33100045   .08240136   4.017    .0001   .47681855
URBSUB    -.36559402   .07955706   -4.595   .0000   .47042366
SIGNALIZ  .13335235   .08686258   1.535    .1247   .22462030
HIGHSP50  -.14109421   .05796415   -2.434   .0149   .69104716
PER       -.01621833   .00772590   -2.099   .0358   8.82625316
DEPRESS   .03971078   .08528086   .466     .6415   .16626699
NOACCON   .07057007   .09177739   .769     .4419   .90487610
LSHPAV    .04129539   .11311582   .365     .7151   .58193445
RSHPAV    -.06074305   .11482333   -.529    .5968   .62949640
          Dispersion parameter for count data model
Alpha     .91175073   .05517813   16.524   .0000

```

Table B10. Night Crash Frequency Model for All Skew Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:19:37AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                2502   |
| Iterations completed                  17     |
| Log likelihood function               -2260.145 |
| Restricted log likelihood             -2415.651 |
| Chi squared                           311.0136 |
| Degrees of freedom                    1      |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -8.64315652  .60046505  -14.394  .0000
LNADTMAJ  .72688505   .06082010  11.951   .0000  8.63901733
LNADTMN   .23867633   .03715944   6.423   .0000  6.52253795
LIGHTING  .21341119   .11152736   1.914   .0557  .47681855
URBSUB    -.53355608   .10646864   -5.011   .0000  .47042366
SIGNALIZ  .05182383   .11302149   .459    .6466  .22462030
HIGHSP50  -.09968322   .07443079   -1.339   .1805  .69104716
PER       -.255397D-04 .01023172   -.002    .9980  8.82625316
DEPRESS   .02583016   .10725705   .241    .8097  .16626699
NOACCON   .14425747   .11221534   1.286   .1986  .90487610
LSHPAV    -.01076510   .14291811   -.075    .9400  .58193445
RSHPAV    -.14177913   .14402146   -.984    .3249  .62949640
Dispersion parameter for count data model
Alpha     .89670311   .09199663   9.747   .0000

```

Table B11. Day Crash Frequency Model for All Tee Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:20:14AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                8963   |
| Iterations completed                 18     |
| Log likelihood function               -8856.289 |
| Restricted log likelihood             -10436.66 |
| Chi squared                          3160.736 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -5.89662928  .28233264  -20.885  .0000
LNADTMAJ  .57770886   .02790069  20.706   .0000   8.53174266
LNADTMN   .10433486   .01156675   9.020    .0000   5.90468010
LIGHTING  -.03399687   .05279564   -.644    .5196   .36494477
URBSUB    -.05615028   .05122836   -1.096   .2730   .41537432
SIGNALIZ  .69798419   .09886746   7.060    .0000   .02889657
HIGHSP50  -.27931572   .04241123   -6.586   .0000   .65112128
PER       -.01186188   .00547851   -2.165   .0304   8.26729669
DEPRESS   .20407093   .06828495   2.989    .0028   .12194578
NOACCON   -.09750650   .08260494   -1.180   .2378   .94031016
LSHPAV    -.33448715   .08634722   -3.874   .0001   .53888207
RSHPAV    .26191216   .08886684   2.947    .0032   .57904719
          Dispersion parameter for count data model
Alpha     1.67478497   .06718893   24.927   .0000

```

Table B12. Night Crash Frequency Model for All Tee Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:20:42AM. |
| Dependent variable                    TOTAL_N |
| Weighting variable                    None    |
| Number of observations                8963    |
| Iterations completed                  18      |
| Log likelihood function                -5100.943 |
| Restricted log likelihood              -5375.175 |
| Chi squared                           548.4651 |
| Degrees of freedom                    1       |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -5.87672215 | .36212310 | -16.229 | .0000 |
LNADTMAJ  .51108537  | .03622867 | 14.107 | .0000 | 8.53174266
LNADTMN   .08707337  | .01546013 | 5.632  | .0000 | 5.90468010
LIGHTING  -.12666815  | .06776424 | -1.869 | .0616 | .36494477
URBSUB    -.45192824  | .06585855 | -6.862 | .0000 | .41537432
SIGNALIZ  .72151034  | .11721069 | 6.156  | .0000 | .02889657
HIGHSP50  -.15950331  | .05446852 | -2.928 | .0034 | .65112128
PER       -.01490102  | .00695475 | -2.143 | .0321 | 8.26729669
DEPRESS   .24233719  | .08515263 | 2.846  | .0044 | .12194578
NOACCON   -.15893467  | .09954235 | -1.597 | .1103 | .94031016
LSHPAV    -.48266614  | .10584825 | -4.560 | .0000 | .53888207
RSHPAV    .29432170  | .11009581 | 2.673  | .0075 | .57904719
          Dispersion parameter for count data model
Alpha     1.49154430 | .11217198 | 13.297 | .0000 |

```

Table B13. Day Crash Frequency Model for All Urban Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:22:23AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                10605  |
| Iterations completed                  18     |
| Log likelihood function                -15723.07 |
| Restricted log likelihood              -17820.19 |
| Chi squared                           4194.242 |
| Degrees of freedom                    1     |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -7.39542636  .20758396  -35.626  .0000
LNADTMAJ  .69312728   .02056588  33.703   .0000   8.93925369
LNADTMN   .14325722   .00970060  14.768   .0000   7.61005548
LIGHTING  .06982479   .03982644   1.753    .0796   .81423857
SIGNALIZ  .66417158   .03270074  20.311   .0000   .27109854
SKEW      .37309117   .03769015   9.899    .0000   .11098538
HIGHSP50  -.13978397   .02581154   -5.416   .0000   .62083923
PER        .00102902   .00379190    .271    .7861   7.10717803
DEPRESS   .04740628   .04278226    1.108    .2678   .11824611
NOACCON   -.06493810   .04220183   -1.539    .1239   .92267798
LSHPAV    -.00317613   .04654401   -.068    .9456   .36115040
RSHPAV    -.05894422   .04258546   -1.384    .1663   .44045262
Dispersion parameter for count data model
Alpha     .70453938   .02319544   30.374   .0000

```



Table B14. Night Crash Frequency Model for All Urban Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:22:43AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                10605  |
| Iterations completed                 16     |
| Log likelihood function               -8209.186 |
| Restricted log likelihood             -8582.260 |
| Chi squared                          746.1476 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =              .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -8.23025802  .31133226  -26.436  .0000
LNADTMAJ  .67200159   .03128921  21.477   .0000   8.93925369
LNADTMN   .12630883   .01511418   8.357   .0000   7.61005548
LIGHTING  -.08536231   .06168714  -1.384   .1664   .81423857
SIGNALIZ  .73030069   .04831000  15.117   .0000   .27109854
SKEW      .42580674   .05194166   8.198   .0000   .11098538
HIGHSP50  -.13593034   .03703963  -3.670   .0002   .62083923
PER       -.01550855   .00578751  -2.680   .0074   7.10717803
DEPRESS   .11928686   .05881800   2.028   .0426   .11824611
NOACCON   -.03933892   .05523693  -.712    .4764   .92267798
LSHPAV    -.18731501   .06384067  -2.934   .0033   .36115040
RSHPAV    .16427662   .05734069   2.865   .0042   .44045262
          Dispersion parameter for count data model
Alpha     .73427708   .04541467  16.168   .0000

```

Table B15. Day Crash Frequency Model for Urban Signalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:23:31AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                2875   |
| Iterations completed                 16     |
| Log likelihood function               -6637.240 |
| Restricted log likelihood             -7379.624 |
| Chi squared                          1484.768 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.50267849  .32500633  -20.008  .0000
LNADTMAJ  .66106742   .03415663  19.354   .0000   9.70266139
LNADTMN   .16219915   .02048459   7.918   .0000   9.03185966
LIGHTING  .03379945   .09961396    .339   .7344   .97217391
SKEW      .21591982   .04142157    5.213   .0000   .17878261
HIGHSP50  -.04826888   .03018526   -1.599   .1098   .60104348
PER       -.00833491   .00516090   -1.615   .1063   5.44667753
DEPRESS   .06069128   .04793850    1.266   .2055   .23826087
NOACCON   -.13303869   .04093847   -3.250   .0012   .84069565
LSHPAV    -.02072160   .05242216    -.395   .6926   .34400000
RSHPAV    -.00431818   .04304374    -.100   .9201   .50365217
Alpha     Dispersion parameter for count data model
          .33835619   .01680866   20.130   .0000

```

Table B16. Night Crash Frequency Model for Urban Signalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:23:58AM. |
| Dependent variable                    TOTAL_N |
| Weighting variable                    None     |
| Number of observations                 2875    |
| Iterations completed                   16      |
| Log likelihood function                -3940.872 |
| Restricted log likelihood              -4045.988 |
| Chi squared                           210.2315 |
| Degrees of freedom                     1       |
| Prob[ChiSqd > value] =                 .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -9.18517422  .47852489  -19.195  .0000
LNADTMAJ  .73062436   .05092417  14.347   .0000   9.70266139
LNADTMN   .24845524   .03386847   7.336    .0000   9.03185966
LIGHTING  -.03356483   .15685097   -.214    .8306   .97217391
SKEW      .33931968   .05987103   5.668    .0000   .17878261
HIGHSP50  -.04208159   .04315055   -.975    .3294   .60104348
PER       -.02916415   .00775545   -3.760   .0002   5.44667753
DEPRESS   -.01416974   .06682751   -.212    .8321   .23826087
NOACCON   -.09266252   .05562517   -1.666   .0957   .84069565
LSHPAV    -.06965974   .07288797   -.956    .3392   .34400000
RSHPAV    .15157643   .05994703   2.529    .0115   .50365217
Alpha     Dispersion parameter for count data model
          .33672865   .03376810   9.972    .0000

```

Table B17. Day Crash Frequency Model for Urban Unsignalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:24:37AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None   |
| Number of observations                7730  |
| Iterations completed                 18    |
| Log likelihood function               -8800.517 |
| Restricted log likelihood             -10369.59 |
| Chi squared                          3138.137 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -7.71145461  .30158210  -25.570  .0000
LNADTMAJ  .72162967   .02859220  25.239   .0000   8.65532133
LNADTMN   .13717364   .01226967  11.180   .0000   7.08124733
LIGHTING  .05263560   .04942478  1.065    .2869   .75549806
SKEW      .57186186   .06630215  8.625    .0000   .08576973
HIGHSP50  -.22195787  .04153669  -5.344   .0000   .62820181
PER        .00934229   .00546058  1.711    .0871   7.72476393
DEPRESS   .04552367   .07979708  .570     .5683   .07360931
NOACCON   .03800811   .08814559  .431     .6663   .95316947
LSHPAV    .02326850   .08715170  .267     .7895   .36752911
RSHPAV    -.10580662   .08527286  -1.241   .2147   .41694696
Alpha     Dispersion parameter for count data model
          1.42086894   .05607419  25.339   .0000

```

Table B18. Night Crash Frequency Model for Urban Unsignalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:25:02AM. |
| Dependent variable                    TOTAL_N |
| Weighting variable                    None    |
| Number of observations                 7730   |
| Iterations completed                   17     |
| Log likelihood function                -4109.605 |
| Restricted log likelihood              -4470.158 |
| Chi squared                            721.1056 |
| Degrees of freedom                     1      |
| Prob[ChiSqd > value] =                 .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -7.54554919  .46635251  -16.180  .0000
LNADTMAJ  .62725022   .04512582   13.900   .0000   8.65532133
LNADTMN   .08367199   .01873851    4.465   .0000   7.08124733
LIGHTING  -.08978536   .07624689   -1.178   .2390   .75549806
SKEW      .71642034   .09834180    7.285   .0000   .08576973
HIGHSP50  -.26603315   .06449416   -4.125   .0000   .62820181
PER       .00075714   .00862544    .088    .9301   7.72476393
DEPRESS   .25341418   .11807388    2.146   .0319   .07360931
NOACCON   -.02830633   .12920289   -.219   .8266   .95316947
LSHPAV    -.23635619   .13088295   -1.806   .0709   .36752911
RSHPAV    .08886383   .12786671    .695    .4871   .41694696
Alpha     2.19140748   .16254618   13.482   .0000
Dispersion parameter for count data model

```

Table B19. Day Crash Frequency Model for Urban Signalized Cross Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:26:12AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                 2158   |
| Iterations completed                   16     |
| Log likelihood function                -4960.373 |
| Restricted log likelihood              -5507.643 |
| Chi squared                           1094.540 |
| Degrees of freedom                     1      |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.44969909  .38057610  -16.947  .0000
LNADTMAJ  .58062561   .06703993   8.661   .0000   9.67838374
LNADTMN   .25656355   .07041171   3.644   .0003   9.27893123
LIGHTING  -.04806528   .12355390   -.389   .6973   .97775718
HIGHSP50  -.04289559   .03470146   -1.236   .2164   .59592215
PER        -.00788670   .00570494   -1.382   .1668   5.51110903
DEPRESS   .00486484   .05966777   .082    .9350   .21362373
NOACCON   -.18624869   .04982562   -3.738   .0002   .87303058
LSHPAV    .02539302   .06439989   .394    .6934   .29101019
RSHPAV    -.03887524   .04963291   -.783   .4335   .45690454
Alpha     .32811667   .01887348   17.385   .0000
Dispersion parameter for count data model

```

Table B20. Night Crash Frequency Model for Urban Signalized Cross Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:26:35AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                2158   |
| Iterations completed                 16     |
| Log likelihood function              -2924.645 |
| Restricted log likelihood             -3014.327 |
| Chi squared                          179.3628 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =              .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -9.29486754  .57048626  -16.293  .0000
LNADTMAJ  .30626355   .09968152   3.072   .0021   9.67838374
LNADTMN   .74031602   .10598999   6.985   .0000   9.27893123
LIGHTING  -.35545333  .18123783  -1.961   .0498   .97775718
HIGHSP50  -.04755818  .05083089  -.936    .3495   .59592215
PER       -.03335134  .00882949  -3.777   .0002   5.51110903
DEPRESS   -.14103047  .08470581  -1.665   .0959   .21362373
NOACCON   -.10180859  .06914530  -1.472   .1409   .87303058
LSHPAV    .04354556  .09049061   .481    .6304   .29101019
RSHPAV    .13520413  .07014626   1.927   .0539   .45690454
Alpha     .35518044  .03954782   8.981   .0000
Dispersion parameter for count data model

```

Table B21. Day Crash Frequency Model for Urban Signalized Skew Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:27:06AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                514    |
| Iterations completed                 15     |
| Log likelihood function               -1224.874 |
| Restricted log likelihood             -1359.843 |
| Chi squared                          269.9394 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =              .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -7.18404375  .79828811  -8.999  .0000
LNADTMAJ  .71008733   .07781102  9.126   .0000   9.73023153
LNADTMN   .17317375   .03964990  4.368   .0000   8.41171648
LIGHTING  .14601602   .20497700  .712    .4762   .96108949
HIGHSP50  -.11968312  .07032882  -1.702  .0888   .60700389
PER       -.02332911  .01450267  -1.609  .1077   5.44478066
DEPRESS   .21303203   .09608516  2.217   .0266   .30350195
NOACCON   .09313155   .08503799  1.095   .2734   .73540856
LSHPAV    .01035587   .11078216  .093    .9255   .46303502
RSHPAV    .15207441   .10479715  1.451   .1467   .61478599
Alpha     Dispersion parameter for count data model
          .32817502   .03883258  8.451   .0000

```



Table B22. Night Crash Frequency Model for Urban Signalized Skew Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:27:31AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                514    |
| Iterations completed                 16     |
| Log likelihood function               -739.3866 |
| Restricted log likelihood             -747.3102 |
| Chi squared                          15.84714 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .6866965E-04 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -10.1534095  1.07882432    -9.412  .0000
LNADTMAJ   .75636468   .10152848     7.450  .0000  9.73023153
LNADTMN   .27250115   .05616434     4.852  .0000  8.41171648
LIGHTING  .64447459   .38080210     1.692  .0906  .96108949
HIGHSP50  -.07536585   .09155159     -.823  .4104  .60700389
PER       -.01755791   .01919180     -.915  .3603  5.44478066
DEPRESS   .22305835   .12419271     1.796  .0725  .30350195
NOACCON   .08583094   .10754402     .798  .4248  .73540856
LSHPAV   -.12621377   .14835948     -.851  .3949  .46303502
RSHPAV    .08986331   .13650432     .658  .5103  .61478599
Alpha     .19942882   .06325688     3.153  .0016
Dispersion parameter for count data model

```

Table B23. Day Crash Frequency Model for Urban Signalized Tee Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:28:05AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                203    |
| Iterations completed                 17     |
| Log likelihood function               -428.0800 |
| Restricted log likelihood             -453.0799 |
| Chi squared                          49.99974 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -7.25332434  1.30951275    -5.539  .0000
LNADTMAJ  .78387081   .12898612     6.077  .0000  9.89093783
LNADTMN   .06448167   .03335774     1.933  .0532  7.97556980
LIGHTING  .26040133   .34248326     .760   .4471  .94088670
HIGHSP50  .07023095   .13196672     .532   .5946  .64039409
PER       .01435673   .02341399     .613   .5398  4.76653865
DEPRESS  -.20700625   .15974400    -1.296  .1950  .33497537
NOACCON  -.16657606   .14786075    -1.127  .2599  .76354680
LSHPAV   -.01572775   .19226360    -.082   .9348  .60591133
RSHPAV   -.19631326   .20129528    -.975   .3294  .71921182
Alpha    Dispersion parameter for count data model
         .31798312   .07176408     4.431  .0000

```

Table B24. Night Crash Frequency Model for Urban Signalized Tee Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:28:23AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                203    |
| Iterations completed                 16     |
| Log likelihood function              -243.7161 |
| Restricted log likelihood             -245.5207 |
| Chi squared                          3.609148 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =              .5746256E-01 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -11.9205466  1.94157347    -6.140  .0000
LNADTMAJ  1.03301420  .18254639     5.659  .0000  9.89093783
LNADTMN   .08435517   .05018253     1.681  .0928  7.97556980
LIGHTING  1.03884190  .76349966     1.361  .1736  .94088670
HIGHSP50  -.20323702  .18297047     -1.111 .2667  .64039409
PER       .04831234   .03410108     1.417  .1566  4.76653865
DEPRESS   -.19810430  .21078902     -.940  .3473  .33497537
NOACCON   -.46271715  .19254630     -2.403 .0163  .76354680
LSHPAV    -.11070715  .26603310     -.416  .6773  .60591133
RSHPAV    .19031634   .29162080     .653   .5140  .71921182
Alpha     .20316904   .13106400     1.550  .1211
Dispersion parameter for count data model

```

Table B25. Day Crash Frequency Model for Urban Unsignalized Cross Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:28:55AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                 3547   |
| Iterations completed                   18     |
| Log likelihood function                -4181.529 |
| Restricted log likelihood               -4732.424 |
| Chi squared                            1101.790 |
| Degrees of freedom                     1      |
| Prob[ChiSqd > value] =                 .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -7.54302056  .40148894  -18.788  .0000
LNADTMAJ  -.06538544   .11802237   -.554   .5796   8.53089692
LNADTMN   .97978375   .12860594   7.618   .0000   8.05411635
LIGHTING  -.00698841   .07649024   -.091   .9272   .83281646
HIGHSP50  -.14389276   .05667146   -2.539   .0111   .64899915
PER       .00972247   .00721525    1.347   .1778   8.22710724
DEPRESS   -.15908581   .12081232   -1.317   .1879   .05497604
NOACCON   -.13255378   .12982661   -1.021   .3073   .96306738
LSHPAV    .15231216   .12930552    1.178   .2388   .26332112
RSHPAV    -.24822667   .12381024   -2.005   .0450   .30279109
Alpha     1.05153302   .06481192   16.224   .0000
Dispersion parameter for count data model

```

Table B26. Night Crash Frequency Model for Urban Unsignalized Cross Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:29:16AM. |
| Dependent variable                    TOTAL_N |
| Weighting variable                    None     |
| Number of observations                 3547    |
| Iterations completed                   16     |
| Log likelihood function                -1853.269 |
| Restricted log likelihood              -1998.719 |
| Chi squared                           290.9000 |
| Degrees of freedom                     1      |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -7.36088717  .66574812  -11.057  .0000
LNADTMAJ  -.04585723   .19548428  -.235    .8145    8.53089692
LNADTMN   .74772243   .21175257  3.531    .0004    8.05411635
LIGHTING  .11051074   .13249772  .834     .4042    .83281646
HIGHSP50  -.21996286  .09581461  -2.296   .0217    .64899915
PER       .00438711   .01228307  .357     .7210    8.22710724
DEPRESS   .36362566   .18742754  1.940    .0524    .05497604
NOACCON   -.00757681   .20373475  -.037    .9703    .96306738
LSHPAV    -.20142316   .21335464  -.944    .3451    .26332112
RSHPAV    .08414423   .20126214  .418     .6759    .30279109
Alpha     1.90329841   .22337783  8.521    .0000
Dispersion parameter for count data model

```

Table B27. Day Crash Frequency Model for Urban Unsignalized Skew Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:29:51AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                663    |
| Iterations completed                 16     |
| Log likelihood function              -887.8690 |
| Restricted log likelihood            -1141.163 |
| Chi squared                          506.5888 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =              .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -10.1976122  1.27004971   -8.029  .0000
LNADTMAJ   .88156889   .11597121    7.602   .0000   8.56885854
LNADTMN   .34056441   .08985278    3.790   .0002   6.63587915
LIGHTING  .19840180   .17093126    1.161   .2458   .76168929
HIGHSP50  -.32425031   .13607264   -2.383   .0172   .64404223
PER       .01875522   .01610747    1.164   .2443   8.30046711
DEPRESS   -.49740742   .26752603   -1.859   .0630   .09049774
NOACCON   .44268378   .31387008    1.410   .1584   .95173454
LSHPAV    .41714994   .36659641    1.138   .2552   .56862745
RSHPAV    -.77382708   .38043904   -2.034   .0419   .59577677
Alpha     1.56274287   .17265184    9.051   .0000
Dispersion parameter for count data model

```

Table B28. Night Crash Frequency Model for Urban Unsignalized Skew Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:30:13AM. |
| Dependent variable                    TOTAL_N |
| Weighting variable                    None    |
| Number of observations                 663    |
| Iterations completed                  15     |
| Log likelihood function                -469.4456 |
| Restricted log likelihood              -527.6173 |
| Chi squared                           116.3435 |
| Degrees of freedom                    1     |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -10.9697863  1.77523734    -6.179  .0000
LNADTMAJ   .91089107   .16795301     5.423  .0000  8.56885854
LNADTMN   .23781710   .12561139     1.893  .0583  6.63587915
LIGHTING  .18172103   .25222761     .720   .4712  .76168929
HIGHSP50  -.39783347   .19216212    -2.070  .0384  .64404223
PER        .00687253   .02447717     .281   .7789  8.30046711
DEPRESS   -.07993178   .36338252    -.220   .8259  .09049774
NOACCON   .57727975   .42857315     1.347  .1780  .95173454
LSHPAV    .16934022   .50863810     .333   .7392  .56862745
RSHPAV    -.51250937   .52846794    -.970   .3321  .59577677
Alpha     2.24503482   .42285363     5.309  .0000
Dispersion parameter for count data model

```

Table B29. Day Crash Frequency Model for Urban Unsignalized Tee Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:30:48AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                 3520   |
| Iterations completed                   16     |
| Log likelihood function                -3664.442 |
| Restricted log likelihood              -4394.254 |
| Chi squared                           1459.625 |
| Degrees of freedom                     1      |
| Prob[ChiSqd > value] =                 .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -8.11748929  .50811182  -15.976  .0000
LNADTMAJ  .77514647   .04737337  16.362   .0000   8.79698559
LNADTMN   .10351712   .01765468   5.863    .0000   6.18480207
LIGHTING  .00095101   .07297060   .013     .9896   .67642045
HIGHSP50  -.27458969  .06763977   -4.060   .0000   .60426136
PER       .00465754   .00974253   .478     .6326   7.11013241
DEPRESS   .18562348   .11812058   1.571    .1161   .08920455
NOACCON   .13333108   .13190690   1.011    .3121   .94346591
LSHPAV    -.04014493   .12732018   -.315    .7525   .43465909
RSHPAV    .03409080   .12636802   .270     .7873   .49829545
Alpha     1.77937114   .10651888   16.705   .0000
Dispersion parameter for count data model

```



Table B30. Night Crash Frequency Model for Urban Unsignalized Tee Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:31:09AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                3520   |
| Iterations completed                 16     |
| Log likelihood function               -1769.817 |
| Restricted log likelihood             -1917.070 |
| Chi squared                          294.5061 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -7.84980525  .73383303  -10.697  .0000
LNADTMAJ  .69396264   .06986064   9.934   .0000   8.79698559
LNADTMN   .06486353   .02619710   2.476   .0133   6.18480207
LIGHTING  -.29108155   .10476662   -2.778   .0055   .67642045
HIGHSP50  -.25693191   .09951956   -2.582   .0098   .60426136
PER       -.00288410   .01422343   -.203   .8393   7.11013241
DEPRESS   .19070119   .17078640   1.117   .2642   .08920455
NOACCON   -.10011623   .18251178   -.549   .5833   .94346591
LSHPAV    -.23209588   .17855342   -1.300   .1936   .43465909
RSHPAV    .07774294   .17832641   .436   .6629   .49829545
Alpha     2.34476706   .26664834   8.793   .0000
Dispersion parameter for count data model

```

Table B31. Day Crash Frequency Model for All Rural Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:32:21AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                11453  |
| Iterations completed                  18     |
| Log likelihood function               -11212.01 |
| Restricted log likelihood              -13069.52 |
| Chi squared                           3715.023 |
| Degrees of freedom                    1     |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.| P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -5.71938980  .24131593  -23.701  .0000
LNADTMAJ  .49003472   .02530969  19.362   .0000    8.13652991
LNADTMN   .17600631   .01163627  15.126   .0000    6.40611686
LIGHTING  .08099104   .05419972   1.494    .1351    .12721558
SIGNALIZ  .53061480   .08906274   5.958    .0000    .03073431
SKEW      .61374783   .05116125  11.996   .0000    .11569021
HIGHSP50  -.19233836  .03855016  -4.989   .0000    .71579499
PER       -.01857325  .00423725  -4.383   .0000    9.97367430
DEPRESS   .14677759   .05729583   2.562    .0104    .13917751
NOACCON   -.02866851  .07660452  -.374    .7082    .94900899
LSHPAV   -.40934445  .09520447  -4.300   .0000    .56229809
RSHPAV    .49221367   .09954111   4.945    .0000    .57993539
          Dispersion parameter for count data model
Alpha     1.48136036  .05469210  27.085   .0000

```

Table B32. Night Crash Frequency Model for All Rural Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:32:40AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                11453  |
| Iterations completed                 18     |
| Log likelihood function               -6923.386 |
| Restricted log likelihood             -7254.762 |
| Chi squared                          662.7519 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.38641240  .29777282  -21.447  .0000
LNADTMAJ  .49806004   .03155036  15.786   .0000   8.13652991
LNADTMN   .12874238   .01425443   9.032    .0000   6.40611686
LIGHTING  .06649521   .06478107   1.026    .3047   .12721558
SIGNALIZ  .40601802   .09869032   4.114    .0000   .03073431
SKEW      .52887716   .06144509   8.607    .0000   .11569021
HIGHSP50  -.07360354  .04721259   -1.559   .1190   .71579499
PER       -.01669873  .00523706   -3.189   .0014   9.97367430
DEPRESS   .23950317   .06720261   3.564    .0004   .13917751
NOACCON   .06424996   .08707751   .738     .4606   .94900899
LSHPAV    -.39116905  .11176443   -3.500   .0005   .56229809
RSHPAV    .31663153   .11772242   2.690    .0072   .57993539
          Dispersion parameter for count data model
Alpha     1.15272098  .07804117   14.771   .0000

```

Table B33. Day Crash Frequency Model for Rural Signalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:33:43AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                 352    |
| Iterations completed                  17      |
| Log likelihood function                -768.0485 |
| Restricted log likelihood              -801.0677 |
| Chi squared                           66.03830 |
| Degrees of freedom                    1      |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -8.01364708  .88961769      -9.008  .0000
LNADTMAJ  .82079675   .10272841      7.990   .0000   9.76038946
LNADTMN   .16113140   .05886343      2.737   .0062   9.00688449
LIGHTING  -.02269614   .17562526      -.129   .8972   .94034091
SKEW      .28676303   .13799980      2.078   .0377   .13636364
HIGHSP50  .07490567   .08469415      .884    .3765   .69602273
PER       .01198076   .01084772      1.104   .2694   6.40545893
DEPRESS   .28132899   .10810390      2.602   .0093   .45738636
NOACCON   -.02718821   .11576018      -.235   .8143   .82386364
LSHPAV    -.49147864   .12738042      -3.858  .0001   .83238636
RSHPAV    -.10409652   .16762387      -.621   .5346   .92329545
Alpha     Dispersion parameter for count data model
          .19579909   .03711637      5.275   .0000

```

Table B34. Night Crash Frequency Model for Rural Signalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:34:01AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                352    |
| Iterations completed                  16     |
| Log likelihood function               -513.0686 |
| Restricted log likelihood              -524.1446 |
| Chi squared                           22.15208 |
| Degrees of freedom                    1      |
| Prob[ChiSqd > value] =                .2518105E-05 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.63090007  1.33976587   -4.949  .0000
LNADTMAJ  .53890908   .15599110    3.455  .0006  9.76038946
LNADTMN   .12619884   .08976953    1.406  .1598  9.00688449
LIGHTING  -.01941672   .26114538    -.074  .9407  .94034091
SKEW      .16314281   .20968611    .778   .4365  .13636364
HIGHSP50  -.02086682   .12797851    -.163  .8705  .69602273
PER        .00760209   .01642101    .463   .6434  6.40545893
DEPRESS   .26574904   .16282422    1.632  .1027  .45738636
NOACCON   .21146771   .17993077    1.175  .2399  .82386364
LSHPAV    -.10275865   .20400244    -.504  .6145  .83238636
RSHPAV    .13496020   .28223091    .478   .6325  .92329545
Dispersion parameter for count data model
Alpha     .29894644   .08654760    3.454  .0006

```

Table B35. Day Crash Frequency Model for Rural Unsignalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:34:45AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                 11101  |
| Iterations completed                  16     |
| Log likelihood function                -10327.05 |
| Restricted log likelihood              -12204.60 |
| Chi squared                           3755.088 |
| Degrees of freedom                    1      |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -5.57755210  .25705642  -21.698  .0000
LNADTMAJ  .47733852   .02666446  17.902   .0000   8.08503918
LNADTMN   .17294355   .01211675  14.273   .0000   6.32364950
LIGHTING  .08562994   .05748770   1.490    .1363   .10143230
SKEW      .63150862   .05464261  11.557   .0000   .11503468
HIGHSP50  -.21231279  .04123193  -5.149   .0000   .71642194
PER       -.02023336  .00450066  -4.496   .0000  10.0868183
DEPRESS   .13608483   .06314549   2.155    .0312   .12908747
NOACCON   -.03301721  .08664957   -.381    .7032   .95297721
LSHPAV    -.44065252  .11083740  -3.976   .0001   .55373390
RSHPAV    .54823226   .11482370   4.775    .0000   .56904783
Alpha     Dispersion parameter for count data model
          1.72417976  .06428254  26.822   .0000

```

Table B36. Night Crash Frequency Model for Rural Unsignalized Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:35:06AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                11101  |
| Iterations completed                 18     |
| Log likelihood function               -6383.613 |
| Restricted log likelihood             -6722.546 |
| Chi squared                          677.8660 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.26837611  .31571662  -19.854  .0000
LNADTMAJ  .48977277   .03310012  14.797   .0000    8.08503918
LNADTMN   .12666425   .01475011  8.587    .0000    6.32364950
LIGHTING  .06996648   .06812609  1.027    .3044    .10143230
SKEW      .55383025   .06529190  8.482    .0000    .11503468
HIGHSP50  -.08174527  .05060805  -1.615   .1063    .71642194
PER       -.01813068  .00554350  -3.271   .0011    10.0868183
DEPRESS   .23539251   .07436200  3.165    .0015    .12908747
NOACCON   .03994523   .09814610  .407     .6840    .95297721
LSHPAV    -.46209866  .12834189  -3.601   .0003    .55373390
RSHPAV    .39037411   .13344562  2.925    .0034    .56904783
Dispersion parameter for count data model
Alpha     1.38431915  .09462971  14.629   .0000

```

Table B37. Day Crash Frequency Model for Rural Signalized Cross Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:36:30AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                248    |
| Iterations completed                  16     |
| Log likelihood function               -548.9494 |
| Restricted log likelihood             -572.3853 |
| Chi squared                           46.87185 |
| Degrees of freedom                    1     |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -7.62480421  .99757239      -7.643  .0000
LNADTMAJ  .66140687   .20467109       3.232  .0012  9.76727850
LNADTMN   .28661495   .20044155       1.430  .1527  9.37634801
LIGHTING  -.06067051  .19241721       -.315  .7525  .93145161
HIGHSP50  .05768318   .09924496        .581  .5611  .73790323
PER       .00929815   .01222893        .760  .4471  6.67048714
DEPRESS   .40214614   .12241355        3.285  .0010  .40725806
NOACCON   .04074145   .15218830        .268  .7889  .88709677
LSHPAV    -.54743803  .15229779       -3.595  .0003  .79435484
RSHPAV    -.08088256  .18122379       -.446  .6554  .89112903
Alpha     .17730429   .03997379        4.436  .0000
Dispersion parameter for count data model

```



Table B38. Night Crash Frequency Model for Rural Signalized Cross Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:36:50AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                248    |
| Iterations completed                 15     |
| Log likelihood function              -368.1396 |
| Restricted log likelihood            -375.1231 |
| Chi squared                          13.96693 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =              .1860540E-03 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.74207458  1.53458372   -4.393  .0000
LNADTMAJ  .45948960   .31045571    1.480  .1389  9.76727850
LNADTMN   .22637592   .30759109    .736  .4618  9.37634801
LIGHTING  -.08677737   .28744927   -.302  .7627  .93145161
HIGHSP50  .01866381   .15090402    .124  .9016  .73790323
PER       -.00141686   .01846008   -.077  .9388  6.67048714
DEPRESS   .38511447   .18411271    2.092  .0365  .40725806
NOACCON   .25516276   .23730393    1.075  .2823  .88709677
LSHPAV   -.14008851   .24528095   -.571  .5679  .79435484
RSHPAV    .14160699   .30223699    .469  .6394  .89112903
Alpha     .25703950   .09200732    2.794  .0052
Dispersion parameter for count data model

```

Table B39. Day Crash Frequency Model for Rural Signalized Skew Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:37:56AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                 48     |
| Iterations completed                  58     |
| Log likelihood function                -91.98571 |
+-----+

```

Variable	Coefficient	Standard Error	b/St.Er.	P[ Z >z]	Mean of X
Constant	-6.81242764	2.10636151	-3.234	.0012	
LNADTMAJ	.53089020	.28868242	1.839	.0659	9.56124093
LNADTMN	.40405124	.14366429	2.812	.0049	7.68419388
LIGHTING	.36156880	.50826781	.711	.4769	.91666667
HIGHSP50	.19688635	.17821716	1.105	.2693	.66666667
PER	.00216616	.02494018	.087	.9308	6.82521195
DEPRESS	-.86211819	.30369535	-2.839	.0045	.66666667
NOACCON	-.52077277	.20659650	-2.521	.0117	.79166667
LSHPAV	.19674821	.38646517	.509	.6107	.91666667
Dispersion parameter for count data model					
Alpha	.957824D-05	.00116501	.008	.9934	

Table B40. Night Crash Frequency Model for Rural Signalized Skew Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:38:20AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                48     |
| Iterations completed                 15     |
| Log likelihood function               -66.25534 |
| Restricted log likelihood             -67.39952 |
| Chi squared                          2.288361 |
| Degrees of freedom                   1      |
| Prob[ChiSqd > value] =               .1303475 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.86331278  4.06838030    -1.687  .0916
LNADTMAJ  .61492770   .57544274     1.069  .2852  9.56124093
LNADTMN   .21531288   .30821080     .699   .4848  7.68419388
LIGHTING  .25362187   .88992681     .285   .7757  .91666667
HIGHSP50  -.09266726  .35871052    -.258  .7961  .66666667
PER       .02368904   .04899638     .483   .6288  6.82521195
DEPRESS   -.26443916  .72726991    -.364  .7162  .66666667
NOACCON   -.49741939  .43666351    -1.139 .2546  .79166667
LSHPAV    -.47224220  .81676366    -.578  .5631  .91666667
Alpha     .31077963   .27172140     1.144  .2527
Dispersion parameter for count data model

```

Table B41. Day Crash Frequency Model for Rural Signalized Tee Minnesota Intersections

No model

Table B42. Night Crash Frequency Model for Rural Signalized Tee Minnesota Intersections

No model

Table B43. Day Crash Frequency Model for Rural Unsignalized Cross Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:40:02AM. |
| Dependent variable                   TOTAL_D |
| Weighting variable                   None    |
| Number of observations                4640   |
| Iterations completed                 16     |
| Log likelihood function               -4188.279 |
| Restricted log likelihood             -4804.002 |
| Chi squared                          1231.447 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =               .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.33419380  .38768677  -16.338  .0000
LNADTMAJ  -.47219334   .12821262  -3.683   .0002   7.83109979
LNADTMN   1.24959608  .13444778   9.294   .0000   7.30897383
LIGHTING  .00928775   .09825683   .095    .9247   .07176724
HIGHSP50  -.16276341  .06394054   -2.546   .0109   .74267241
PER       -.01549035  .00661182   -2.343   .0191  10.9241909
DEPRESS   .06027837   .09428972   .639    .5226   .12543103
NOACCON   .14984212   .13097998   1.144   .2526   .95732759
LSHPAV    -.18333464  .21398635   -.857   .3916   .47952586
RSHPAV    .37485760   .22081840   1.698   .0896   .48857759
Alpha     1.46843123  .09001232   16.314  .0000
Dispersion parameter for count data model

```

Table B44. Night Crash Frequency Model for Rural Unsignalized Cross Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:40:37AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                4640   |
| Iterations completed                 15     |
| Log likelihood function               -2456.970 |
| Restricted log likelihood             -2529.646 |
| Chi squared                          145.3523 |
| Degrees of freedom                   1     |
| Prob[ChiSqd > value] =              .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.68225789  .47946661  -13.937  .0000
LNADTMAJ  -.13907453   .16000452   -.869   .3847   7.83109979
LNADTMN   .83552464   .16516825   5.059   .0000   7.30897383
LIGHTING  -.12120814   .12309445   -.985   .3248   .07176724
HIGHSP50  -.08533633   .08054468   -1.059   .2894   .74267241
PER       -.01984652   .00850246   -2.334   .0196   10.9241909
DEPRESS   .18146563   .11333876   1.601   .1094   .12543103
NOACCON   .10257895   .14697005   .698    .4852   .95732759
LSHPAV    -.18559236   .24897449   -.745   .4560   .47952586
RSHPAV    .23337866   .25894821   .901    .3675   .48857759
Alpha     1.05570986   .13665772   7.725   .0000
Dispersion parameter for count data model

```

Table B45. Day Crash Frequency Model for Rural Unsignalized Skew Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:41:11AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                1277    |
| Iterations completed                  17      |
| Log likelihood function               -1502.168 |
| Restricted log likelihood              -1884.253 |
| Chi squared                           764.1711 |
| Degrees of freedom                    1      |
| Prob[ChiSqd > value] =                .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -6.59815229  .77408387  -8.524  .0000
LNADTMAJ  .55931979   .07693986  7.270   .0000   8.20155802
LNADTMN   .25842861   .04492172  5.753   .0000   5.65962294
LIGHTING  .53653769   .14461428  3.710   .0002   .11746280
HIGHSP50  -.05305462   .11421983  -.464   .6423   .75019577
PER       -.02666613   .01266776  -2.105  .0353   10.5355116
DEPRESS   .13497720   .17435722  .774    .4388   .13155834
NOACCON   .31169837   .23754535  1.312   .1895   .95301488
LSHPAV    .18766935   .33143748  .566    .5712   .62411903
RSHPAV    -.08867902   .33625060  -.264   .7920   .63899765
Alpha     1.49483788   .13484490  11.086  .0000
Dispersion parameter for count data model

```



Table B46. Night Crash Frequency Model for Rural Unsignalized Skew Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:41:37AM. |
| Dependent variable                   TOTAL_N |
| Weighting variable                   None    |
| Number of observations                1277   |
| Iterations completed                 15     |
| Log likelihood function               -925.2663 |
| Restricted log likelihood             -1045.876 |
| Chi squared                          241.2185 |
| Degrees of freedom                   1      |
| Prob[ChiSqd > value] =              .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -8.94407170  1.02727083    -8.707  .0000
LNADTMAJ  .72895668   .10527847     6.924  .0000  8.20155802
LNADTMN   .21649734   .05875543     3.685  .0002  5.65962294
LIGHTING  .32193137   .18724289     1.719  .0856  .11746280
HIGHSP50  -.04093812   .14902861     -.275  .7835  .75019577
PER       .00834383   .01649473     .506   .6130  10.5355116
DEPRESS   -.08602163   .23026975     -.374  .7087  .13155834
NOACCON   .50574385   .30219738     1.674  .0942  .95301488
LSHPAV    .76284838   .47636736     1.601  .1093  .62411903
RSHPAV    -.92120788   .47987242     -1.920 .0549  .63899765
Alpha     1.74433334   .24555074     7.104  .0000
Dispersion parameter for count data model

```

Table B47. Day Crash Frequency Model for Rural Unsignalized Tee Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates          |
| Model estimated: Jul 05, 2007 at 07:42:24AM. |
| Dependent variable                    TOTAL_D |
| Weighting variable                    None    |
| Number of observations                5184   |
| Iterations completed                  15     |
| Log likelihood function               -4563.699 |
| Restricted log likelihood              -5378.243 |
| Chi squared                           1629.089 |
| Degrees of freedom                    1      |
| Prob[ChiSq > value] =                 .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -4.71104839  .38497045  -12.237  .0000
LNADTMAJ  .44716633   .03908163   11.442   .0000   8.28362796
LNADTMN   .11827903   .01747617    6.768   .0000   5.60529630
LIGHTING  -.06484848   .08533172    -.760   .4473   .12403549
HIGHSP50  -.29378132   .06083001   -4.830   .0000   .68460648
PER        -.01702919   .00711901   -2.392   .0168   9.22678939
DEPRESS   .20669476   .09739275    2.122   .0338   .13175154
NOACCON   -.24410149   .12949943   -1.885   .0594   .94907407
LSHPAV    -.59759870   .14283099   -4.184   .0000   .60281636
RSHPAV    .59114813   .15016730    3.937   .0001   .62384259
Alpha     1.91177203   .10750994   17.782   .0000
Dispersion parameter for count data model

```

Table B48. Night Crash Frequency Model for Rural Unsignalized Tee Minnesota Intersections

```

+-----+
| Negative Binomial Regression          |
| Maximum Likelihood Estimates         |
| Model estimated: Jul 05, 2007 at 07:42:51AM. |
| Dependent variable                    TOTAL_N |
| Weighting variable                    None     |
| Number of observations                 5184    |
| Iterations completed                   16      |
| Log likelihood function                -2965.580 |
| Restricted log likelihood              -3098.281 |
| Chi squared                           265.4032 |
| Degrees of freedom                     1       |
| Prob[ChiSqd > value] =                 .0000000 |
+-----+
+-----+-----+-----+-----+-----+-----+
|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X|
+-----+-----+-----+-----+-----+-----+
Constant  -5.19290697  .45757004  -11.349  .0000
LNADTMAJ  .40115218   .04641249   8.643   .0000   8.28362796
LNADTMN   .10958480   .02099918   5.219   .0000   5.60529630
LIGHTING  .06060979   .09565357   .634    .5263   .12403549
HIGHSP50  -.09336677   .07192160   -1.298  .1942   .68460648
PER       -.01653396   .00829095   -1.994  .0461   9.22678939
DEPRESS   .33934040   .11063072   3.067   .0022   .13175154
NOACCON   -.11120055   .14197695   -.783   .4335   .94907407
LSHPAV    -.69540747   .15693949   -4.431  .0000   .60281636
RSHPAV    .53103600   .16546869   3.209   .0013   .62384259
Alpha     1.35965761   .14225196   9.558   .0000
Dispersion parameter for count data model

```

## **APPENDIX C**

### **MINNESOTA INTERCHANGE MODELING RESULTS**

Table C.1 Nighttime Crash Frequency at Urban Interchanges

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -1623.5861
Number of obs   =      586
LR chi2(10)    =     350.76
Prob > chi2    =      0.0000
Pseudo R2     =      0.0975
    
```

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
light	.5867927	.2124439	2.76	0.006	.1704104	1.003175
speed	.0039009	.0046664	0.84	0.403	-.005245	.0130468
lntotent	.1868157	.0288608	6.47	0.000	.1302495	.2433818
perhv	-.0951145	.0121908	-7.80	0.000	-.1190081	-.071221
fullacc	.5041879	.1464644	3.44	0.001	.217123	.7912529
paracc	.0680255	.1777824	0.38	0.702	-.2804216	.4164725
barrier	.2726549	.0822509	3.31	0.001	.1114461	.4338638
surf_typ	-.1441283	.0769424	-1.87	0.061	-.2949326	.006676
lnwdt13	-.0418096	.122657	-0.34	0.733	-.2822128	.1985936
nolanes5	.4270882	.0875003	4.88	0.000	.2555907	.5985857
_cons	-.8351119	.4304406	-1.94	0.052	-1.67876	.0085362
/lnalpha	-.6100133	.0816371			-.7700192	-.4500075
alpha	.5433436	.044357			.4630042	.6376234

Likelihood-ratio test of alpha=0: chibar2(01) = 1218.24 Prob>=chibar2 = 0.000

Table C.2 Daytime Crash Frequency at Urban Interchanges

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -2061.7647
Number of obs   =      586
LR chi2(10)    =     397.27
Prob > chi2    =      0.0000
Pseudo R2     =      0.0879
    
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
light	.6944077	.1878684	3.70	0.000	.3261923	1.062623
speed	.0016317	.0045698	0.36	0.721	-.007325	.0105884
lntotent	.164903	.0281489	5.86	0.000	.1097322	.2200739
perhv	-.1073809	.0110951	-9.68	0.000	-.1291269	-.0856348
fullacc	.4176206	.1376832	3.03	0.002	.1477665	.6874748
paracc	.1275491	.1633842	0.78	0.435	-.1926781	.4477762
barrier	.4349037	.0805808	5.40	0.000	.2769682	.5928392
surf_typ	-.1020716	.0753399	-1.35	0.175	-.2497351	.0455919
lnwdt13	-.2477663	.1169114	-2.12	0.034	-.4769084	-.0186242
nolanes5	.3413149	.0865674	3.94	0.000	.1716459	.510984
_cons	.331869	.4069203	0.82	0.415	-.4656802	1.129418
/lnalpha	-.5264352	.0669861			-.6577256	-.3951449
alpha	.590707	.0395692			.5180282	.6735825

Likelihood-ratio test of alpha=0: chibar2(01) = 3978.51 Prob>=chibar2 = 0.000

Table C.3 Nighttime Crash Frequency at Rural Interchanges

Negative binomial regression		Number of obs	=	1435
		LR chi2(10)	=	524.37
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -3429.1553	Pseudo R2	=	0.0710

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
light	.2886575	.0738712	3.91	0.000	.1438726	.4334424
speed	-.0089544	.003536	-2.53	0.011	-.0158848	-.0020239
lntotent	.1464587	.017816	8.22	0.000	.1115399	.1813775
perhv	-.0277927	.0056278	-4.94	0.000	-.038823	-.0167624
fullacc	.5747832	.0754821	7.61	0.000	.426841	.7227255
paracc	.0525896	.1059195	0.50	0.620	-.1550088	.260188
barrier	.0000767	.0578331	0.00	0.999	-.113274	.1134275
surf_typ	.0005942	.0471759	0.01	0.990	-.0918688	.0930572
lnwdt13	-.1680718	.0798577	-2.10	0.035	-.32459	-.0115536
nolanes5	.181286	.058061	3.12	0.002	.0674886	.2950834
_cons	.0984901	.2959619	0.33	0.739	-.4815846	.6785648
/lnalpha	-.8310014	.0627141			-.9539188	-.708084
alpha	.4356128	.0273191			.3852284	.4925871

Likelihood-ratio test of alpha=0: chibar2(01) = 1163.26 Prob>=chibar2 = 0.000

Table C.4 Daytime Crash Frequency at Rural Interchanges

Negative binomial regression		Number of obs	=	1435
		LR chi2(10)	=	933.07
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -4359.6032	Pseudo R2	=	0.0967

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
light	.3721704	.0722535	5.15	0.000	.2305561	.5137846
speed	-.0227364	.0035974	-6.32	0.000	-.0297872	-.0156857
lntotent	.1854693	.0174591	10.62	0.000	.1512501	.2196884
perhv	-.0499698	.0057152	-8.74	0.000	-.0611715	-.0387681
fullacc	.7551505	.0726938	10.39	0.000	.6126732	.8976277
paracc	.1997086	.1016152	1.97	0.049	.0005465	.3988706
barrier	.0307676	.0571023	0.54	0.590	-.0811508	.1426861
surf_typ	.0608123	.0467234	1.30	0.193	-.0307639	.1523886
lnwdt13	-.2894733	.0775884	-3.73	0.000	-.4415438	-.1374028
nolanes5	.2094159	.0567987	3.69	0.000	.0980926	.3207393
_cons	1.264104	.2934896	4.31	0.000	.6888751	1.839333
/lnalpha	-.62515	.0474863			-.7182214	-.5320786
alpha	.5351811	.0254138			.4876187	.5873828

Likelihood-ratio test of alpha=0: chibar2(01) = 5331.08 Prob>=chibar2 = 0.000

Table C.5 Nighttime Crash Frequency at Diamond Interchanges

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -3975.4573
Number of obs   =      1615
LR chi2(11)    =      719.88
Prob > chi2     =      0.0000
Pseudo R2      =      0.0830
    
```

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
urbsub	.2193731	.0721004	3.04	0.002	.0780588	.3606873
light	.1454341	.0788446	1.84	0.065	-.0090986	.2999668
speed	-.003962	.0032708	-1.21	0.226	-.0103726	.0024486
lntotent	.1404026	.0204554	6.86	0.000	.1003108	.1804945
perhv	-.0349947	.0060323	-5.80	0.000	-.0468179	-.0231716
fullacc	.6143975	.0830741	7.40	0.000	.4515752	.7772198
paracc	.220536	.1081712	2.04	0.041	.0085244	.4325476
barrier	.0411261	.0539615	0.76	0.446	-.0646366	.1468888
surf_typ	-.0657381	.0473778	-1.39	0.165	-.1585969	.0271208
lnwdt13	-.1453685	.0737372	-1.97	0.049	-.2898908	-.0008461
nolanes5	.4460293	.0569015	7.84	0.000	.3345044	.5575542
_cons	-.1528953	.2778334	-0.55	0.582	-.6974387	.3916481
/lnalpha	-.695254	.0556197			-.8042667	-.5862413
alpha	.4989477	.0277513			.4474159	.5564148

Likelihood-ratio test of alpha=0: chibar2(01) = 1834.70 Prob>=chibar2 = 0.000

Table C.6 Daytime Crash Frequency at Diamond Interchanges

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -5024.2953
Number of obs   =      1615
LR chi2(11)    =     1162.18
Prob > chi2     =      0.0000
Pseudo R2      =      0.1037
    
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
urbsub	.3210806	.0671678	4.78	0.000	.1894342	.4527271
light	.2820434	.0744099	3.79	0.000	.1362028	.427884
speed	-.012723	.0032039	-3.97	0.000	-.0190025	-.0064434
lntotent	.1793995	.0195007	9.20	0.000	.1411788	.2176202
perhv	-.0505427	.0058873	-8.59	0.000	-.0620816	-.0390038
fullacc	.7037749	.0776261	9.07	0.000	.5516306	.8559193
paracc	.3089696	.10007	3.09	0.002	.1128361	.5051032
barrier	.0955495	.0518679	1.84	0.065	-.0061097	.1972087
surf_typ	.03421	.0460213	0.74	0.457	-.0559902	.1244101
lnwdt13	-.3374671	.0704481	-4.79	0.000	-.4755428	-.1993915
nolanes5	.3882963	.0546769	7.10	0.000	.2811315	.495461
_cons	.6124136	.2689089	2.28	0.023	.0853618	1.139465
/lnalpha	-.5945438	.0441946			-.6811635	-.507924
alpha	.5518143	.0243872			.5060279	.6017435

Likelihood-ratio test of alpha=0: chibar2(01) = 6852.38 Prob>=chibar2 = 0.000

Table C.7 Nighttime Crash Frequency at Non-diamond Interchanges

```
Negative binomial regression
Dispersion      = mean
Log likelihood = -1072.8337
Number of obs   =      406
LR chi2(11)    =      270.78
Prob > chi2     =      0.0000
Pseudo R2      =      0.1121
```

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
urbsub	.1296607	.1406268	0.92	0.357	-.1459628	.4052843
light	.1954161	.1725065	1.13	0.257	-.1426903	.5335226
speed	-.0085987	.0057192	-1.50	0.133	-.0198082	.0026107
lntotent	.6838169	.0802445	8.52	0.000	.5265406	.8410932
perhv	.0208956	.0143831	1.45	0.146	-.0072947	.0490859
fullacc	.3820624	.1247409	3.06	0.002	.1375748	.6265501
paracc	.1440984	.1676587	0.86	0.390	-.1845066	.4727034
barrier	.3636504	.0890573	4.08	0.000	.1891013	.5381994
surf_typ	-.0149644	.0813596	-0.18	0.854	-.1744263	.1444975
lnwdt13	.3068953	.1502972	2.04	0.041	.0123181	.6014725
nolanes5	-.1601787	.095884	-1.67	0.095	-.3481079	.0277504
_cons	-6.267433	.9545055	-6.57	0.000	-8.13823	-4.396637
/lnalpha	-.9883788	.1079593			-1.199975	-.7767825
alpha	.3721796	.0401802			.3012017	.4598833

Likelihood-ratio test of alpha=0: chibar2(01) = 477.42 Prob>=chibar2 = 0.000

Table C.8 Daytime Crash Frequency at Non-diamond Interchanges

```
Negative binomial regression
Dispersion      = mean
Log likelihood = -1343.382
Number of obs   =      406
LR chi2(11)    =      346.51
Prob > chi2     =      0.0000
Pseudo R2      =      0.1142
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
urbsub	.3829578	.1289768	2.97	0.003	.1301679	.6357476
light	.0158911	.1550926	0.10	0.918	-.2880848	.3198671
speed	-.0004376	.005595	-0.08	0.938	-.0114035	.0105283
lntotent	.7428129	.0722225	10.29	0.000	.6012595	.8843663
perhv	.0025853	.0130436	0.20	0.843	-.0229797	.0281504
fullacc	.2443714	.1171482	2.09	0.037	.0147651	.4739777
paracc	.1958816	.1483634	1.32	0.187	-.0949053	.4866686
barrier	.3921486	.084833	4.62	0.000	.225879	.5584182
surf_typ	-.018593	.0760622	-0.24	0.807	-.1676722	.1304862
lnwdt13	.2938539	.1364177	2.15	0.031	.0264802	.5612277
nolanes5	-.2159345	.0904153	-2.39	0.017	-.3931452	-.0387239
_cons	-6.43579	.8703579	-7.39	0.000	-8.14166	-4.72992
/lnalpha	-.9179204	.0879265			-1.090253	-.7455875
alpha	.3993487	.0351133			.3361314	.4744555

Likelihood-ratio test of alpha=0: chibar2(01) = 1438.60 Prob>=chibar2 = 0.000



Table C.9 Nighttime Crash Frequency at Urban Diamond Interchanges

Negative binomial regression		Number of obs	=	466
		LR chi2(10)	=	288.84
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -1233.4546	Pseudo R2	=	0.1048

nightttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
light	.6456998	.2133101	3.03	0.002	.2276197	1.06378
speed	.0049785	.0051087	0.97	0.330	-.0050343	.0149913
lntotent	.1761292	.0380121	4.63	0.000	.1016269	.2506315
perhv	-.0919834	.0128823	-7.14	0.000	-.1172322	-.0667346
fullacc	.4313385	.1564595	2.76	0.006	.1246835	.7379935
paracc	.1088033	.1948686	0.56	0.577	-.2731322	.4907388
barrier	.1331015	.0940993	1.41	0.157	-.0513298	.3175328
surf_typ	-.1218866	.0892679	-1.37	0.172	-.2968485	.0530752
lnwdt13	-.2065809	.1356517	-1.52	0.128	-.4724533	.0592914
nolanes5	.592187	.1073697	5.52	0.000	.3817462	.8026278
_cons	-.8120932	.4888005	-1.66	0.097	-1.770125	.1459381
/lnalpha	-.64899	.0982818			-.8416187	-.4563613
alpha	.5225733	.0513594			.4310123	.6335849

Likelihood-ratio test of alpha=0: chibar2(01) = 725.71 Prob>=chibar2 = 0.000

Table C.10 Daytime Crash Frequency at Urban Diamond Interchanges

Negative binomial regression		Number of obs	=	466
		LR chi2(10)	=	326.35
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -1589.6379	Pseudo R2	=	0.0931

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
light	.7382279	.1933234	3.82	0.000	.3593209	1.117135
speed	.0001808	.0050418	0.04	0.971	-.0097009	.0100624
lntotent	.1964347	.0376528	5.22	0.000	.1226366	.2702327
perhv	-.1050144	.0120387	-8.72	0.000	-.1286099	-.081419
fullacc	.3856521	.1516194	2.54	0.011	.0884836	.6828206
paracc	.1429716	.1841316	0.78	0.437	-.2179196	.5038628
barrier	.2841804	.09299	3.06	0.002	.1019233	.4664374
surf_typ	-.0085291	.0888369	-0.10	0.924	-.1826462	.1655881
lnwdt13	-.4735559	.1306141	-3.63	0.000	-.7295548	-.217557
nolanes5	.430548	.1081458	3.98	0.000	.2185862	.6425098
_cons	.1179226	.4775779	0.25	0.805	-.8181128	1.053958
/lnalpha	-.49451	.0768578			-.6451486	-.3438714
alpha	.6098697	.0468733			.5245846	.7090201

Likelihood-ratio test of alpha=0: chibar2(01) = 2863.90 Prob>=chibar2 = 0.000

Table C.11 Nighttime Crash Frequency at Urban Non-diamond Interchanges

Negative binomial regression		Number of obs	=	120
		LR chi2(9)	=	73.09
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -372.19094	Pseudo R2	=	0.0894

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
speed	-.0146038	.0103482	-1.41	0.158	-.0348858	.0056783
lntotent	.5450068	.2193566	2.48	0.013	.1150758	.9749377
perhv	.0651549	.0569456	1.14	0.253	-.0464564	.1767662
fullacc	1.095213	.3750625	2.92	0.003	.3601035	1.830321
paracc	.6010731	.4383883	1.37	0.170	-.2581521	1.460298
barrier	.4965469	.2125319	2.34	0.019	.079992	.9131018
surf_typ	-.2870485	.1516555	-1.89	0.058	-.5842878	.0101909
lnwdt13	.7384109	.2982454	2.48	0.013	.1538606	1.322961
nolan5	.0379337	.1622413	0.23	0.815	-.2800534	.3559209
_cons	-4.781607	2.509786	-1.91	0.057	-9.700698	.1374833
/lnalpha	-.8992467	.1700664			-1.232571	-.5659228
alpha	.406876	.0691959			.2915422	.5678359

Likelihood-ratio test of alpha=0: chibar2(01) = 239.05 Prob>=chibar2 = 0.000

Table C.12 Daytime Crash Frequency at Urban Non-diamond Interchanges

Negative binomial regression		Number of obs	=	120
		LR chi2(9)	=	117.80
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -437.18035	Pseudo R2	=	0.1187

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
speed	-.0025469	.0086126	-0.30	0.767	-.0194273	.0143335
lntotent	.7311727	.1717078	4.26	0.000	.3946317	1.067714
perhv	.0714641	.0450384	1.59	0.113	-.0168094	.1597377
fullacc	.6860883	.2703619	2.54	0.011	.1561888	1.215988
paracc	.6542017	.3312799	1.97	0.048	.004905	1.303498
barrier	.6453552	.1702445	3.79	0.000	.311682	.9790283
surf_typ	-.4257531	.1213291	-3.51	0.000	-.6635539	-.1879524
lnwdt13	.7783586	.2412997	3.23	0.001	.3054198	1.251297
nolan5	-.0893806	.132583	-0.67	0.500	-.3492386	.1704774
_cons	-6.508942	1.971371	-3.30	0.001	-10.37276	-2.645125
/lnalpha	-1.265993	.1581327			-1.575927	-.9560586
alpha	.2819592	.044587			.2068156	.384405

Likelihood-ratio test of alpha=0: chibar2(01) = 404.71 Prob>=chibar2 = 0.000

Table C.13 Nighttime Crash Frequency at Rural Diamond Interchanges

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -2705.8768
Number of obs   =      1149
LR chi2(10)    =      415.40
Prob > chi2    =      0.0000
Pseudo R2     =      0.0713
    
```

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
light	.2736851	.0829569	3.30	0.001	.1110926	.4362775
speed	-.0108622	.0040795	-2.66	0.008	-.0188578	-.0028665
lntotent	.1531824	.0231243	6.62	0.000	.1078596	.1985051
perhv	-.025076	.006343	-3.95	0.000	-.0375081	-.012644
fullacc	.6000502	.096618	6.21	0.000	.4106825	.789418
paracc	.1782219	.1303735	1.37	0.172	-.0773055	.4337494
barrier	-.0722396	.066293	-1.09	0.276	-.2021715	.0576922
surf_typ	-.0638489	.0534455	-1.19	0.232	-.1686002	.0409024
lnwdt13	-.1649462	.0882052	-1.87	0.061	-.3378251	.0079328
nolanes5	.2719922	.0665963	4.08	0.000	.1414658	.4025186
_cons	.1720876	.3445188	0.50	0.617	-.5031569	.8473321
/lnalpha	-.832743	.0711814			-.972256	-.6932301
alpha	.4348548	.0309536			.3782288	.4999585

Likelihood-ratio test of alpha=0: chibar2(01) = 880.52 Prob>=chibar2 = 0.000

Table C.14 Daytime Crash Frequency at Rural Diamond Interchanges

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -3413.2482
Number of obs   =      1149
LR chi2(10)    =      818.95
Prob > chi2    =      0.0000
Pseudo R2     =      0.1071
    
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
light	.3834003	.0795557	4.82	0.000	.227474	.5393267
speed	-.0264689	.0040002	-6.62	0.000	-.0343091	-.0186287
lntotent	.2086921	.0222109	9.40	0.000	.1651595	.2522247
perhv	-.0424414	.0063088	-6.73	0.000	-.0548065	-.0300764
fullacc	.8223061	.0910953	9.03	0.000	.6437626	1.00085
paracc	.3464857	.1227203	2.82	0.005	.1059583	.5870132
barrier	-.0148906	.0634801	-0.23	0.815	-.1393093	.109528
surf_typ	-.0169043	.0519131	-0.33	0.745	-.1186522	.0848435
lnwdt13	-.3073003	.0851967	-3.61	0.000	-.4742827	-.1403179
nolanes5	.3423453	.0640221	5.35	0.000	.2168644	.4678262
_cons	1.206262	.3318764	3.63	0.000	.5557959	1.856727
/lnalpha	-.6876814	.0547565			-.7950021	-.5803607
alpha	.5027404	.0275283			.4515803	.5596965

Likelihood-ratio test of alpha=0: chibar2(01) = 3752.65 Prob>=chibar2 = 0.000

Table C.15 Nighttime Crash Frequency at Rural Non-diamond Interchanges

Negative binomial regression		Number of obs	=	286
		LR chi2(10)	=	180.21
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -683.2217	Pseudo R2	=	0.1165

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
light	.2288388	.1655554	1.38	0.167	-.0956437	.5533214
speed	-.0017687	.0064223	-0.28	0.783	-.0143561	.0108188
lntotent	.769023	.0821775	9.36	0.000	.607958	.9300881
perhv	.0310834	.0137215	2.27	0.023	.0041898	.057977
fullacc	.1484467	.1370569	1.08	0.279	-.1201798	.4170732
paracc	.0806542	.1791332	0.45	0.653	-.2704404	.4317488
barrier	.2003693	.1058127	1.89	0.058	-.0070198	.4077585
surf_typ	.0425087	.0952066	0.45	0.655	-.1440928	.2291102
lnwdt13	.1240215	.1776796	0.70	0.485	-.2242242	.4722671
nolanes5	-.141564	.1158089	-1.22	0.222	-.3685453	.0854173
_cons	-7.549688	1.07958	-6.99	0.000	-9.665625	-5.43375
/lnalpha	-1.332882	.1650967			-1.656466	-1.009298
alpha	.2637161	.0435387			.1908122	.3644746

Likelihood-ratio test of alpha=0: chibar2(01) = 126.28 Prob>=chibar2 = 0.000

Table C.16 Daytime Crash Frequency at Rural Non-diamond Interchanges

Negative binomial regression		Number of obs	=	286
		LR chi2(10)	=	207.44
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -895.49615	Pseudo R2	=	0.1038

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
light	.0810993	.1669421	0.49	0.627	-.2461011	.4082998
speed	-.0054637	.0072166	-0.76	0.449	-.0196079	.0086805
lntotent	.7810165	.0815988	9.57	0.000	.6210858	.9409472
perhv	-.0080572	.0140716	-0.57	0.567	-.035637	.0195225
fullacc	.1948116	.144446	1.35	0.177	-.0882975	.4779206
paracc	.1250202	.178962	0.70	0.485	-.2257389	.4757792
barrier	.1763627	.1144553	1.54	0.123	-.0479657	.400691
surf_typ	.1242483	.1001298	1.24	0.215	-.0720024	.320499
lnwdt13	.0959326	.169422	0.57	0.571	-.2361284	.4279936
nolanes5	-.2055231	.12197	-1.69	0.092	-.4445799	.0335337
_cons	-6.278309	1.096109	-5.73	0.000	-8.426643	-4.129975
/lnalpha	-.8522279	.1088904			-1.065649	-.6388067
alpha	.4264638	.0464378			.3445042	.527922

Likelihood-ratio test of alpha=0: chibar2(01) = 849.34 Prob>=chibar2 = 0.000

Table C.17 Nighttime Crash Frequency at Urban Interchanges (Lighting Type)

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -3529.7978
Number of obs   = 1245
LR chi2(13)    = 420.75
Prob > chi2     = 0.0000
Pseudo R2      = 0.0562
    
```

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
diamond	.1299719	.0729257	1.78	0.075	-.0129599	.2729037
full	.4977644	.1720527	2.89	0.004	.1605473	.8349815
partial	.4644382	.1721442	2.70	0.007	.1270417	.8018348
continuo	.6367349	.1801518	3.53	0.000	.2836438	.989826
speed	.0002781	.0031525	0.09	0.930	-.0059006	.0064569
Intotent	.1697101	.0245944	6.90	0.000	.1215059	.2179143
perhv	-.0651578	.0094855	-6.87	0.000	-.0837491	-.0465666
fullacc	.6152043	.0844129	7.29	0.000	.4497581	.7806505
paracc	.1852011	.1131457	1.64	0.102	-.0365604	.4069627
barrier	.2640473	.0553848	4.77	0.000	.1554952	.3725994
surf_typ	-.1095608	.0500379	-2.19	0.029	-.2076334	-.0114883
lnwdt13	-.2678678	.0941922	-2.84	0.004	-.4524811	-.0832544
nolanes5	.1827489	.0539085	3.39	0.001	.0770901	.2884076
_cons	-.713106	.3553065	-2.01	0.045	-1.409494	-.0167181
-----						
/lnalpha	-.699693	.0542203			-.8059628	-.5934232
-----						
alpha	.4967378	.0269333			.4466577	.5524329
-----						

Likelihood-ratio test of alpha=0: chibar2(01) = 2361.70 Prob>=chibar2 = 0.000

Table C.18 Daytime Crash Frequency at Urban Interchanges (Lighting Presence)

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -4551.1874
Number of obs   = 1245
LR chi2(13)    = 485.01
Prob > chi2     = 0.0000
Pseudo R2      = 0.0506
    
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
diamond	.2377835	.0699023	3.40	0.001	.1007775	.3747894
full	.4612353	.1461526	3.16	0.002	.1747814	.7476891
partial	.344851	.1465064	2.35	0.019	.0577037	.6319983
continuo	.5401067	.1549958	3.48	0.000	.2363205	.8438929
speed	-.0029923	.003079	-0.97	0.331	-.009027	.0030425
Intotent	.1780763	.0231643	7.69	0.000	.1326752	.2234774
perhv	-.0809848	.0089587	-9.04	0.000	-.0985435	-.063426
fullacc	.6214883	.0779469	7.97	0.000	.4687153	.7742614
paracc	.2124778	.1030702	2.06	0.039	.0104639	.4144918
barrier	.330481	.0527514	6.26	0.000	.2270902	.4338719
surf_typ	-.0592268	.0479074	-1.24	0.216	-.1531236	.03467
lnwdt13	-.3697781	.0873532	-4.23	0.000	-.5409873	-.1985689
nolanes5	.1315131	.0515782	2.55	0.011	.0304216	.2326046
_cons	.3292399	.3288924	1.00	0.317	-.3153772	.9738571
-----						
/lnalpha	-.6357816	.0444438			-.7228899	-.5486733
-----						
alpha	.5295214	.023534			.4853476	.5777157
-----						

Likelihood-ratio test of alpha=0: chibar2(01) = 8142.43 Prob>=chibar2 = 0.000

Table C.19 Nighttime Crash Frequency at Rural Interchanges (Lighting Type)

```
Negative binomial regression
Dispersion = mean
Log likelihood = -1511.4519
Number of obs = 776
LR chi2(13) = 173.47
Prob > chi2 = 0.0000
Pseudo R2 = 0.0543
```

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
diamond	.0495629	.1116904	0.44	0.657	-.1693463	.2684722
full	.050679	.1054561	0.48	0.631	-.1560112	.2573692
partial	.1199328	.0865097	1.39	0.166	-.0496231	.2894888
continuo	.8774836	.3702182	2.37	0.018	.1518691	1.603098
speed	-.0017407	.0070229	-0.25	0.804	-.0155053	.0120239
lntotent	.142472	.0333175	4.28	0.000	.0771708	.2077731
perhv	-.0079899	.0069776	-1.15	0.252	-.0216657	.0056859
fullacc	.5356503	.1256403	4.26	0.000	.2893997	.7819008
paracc	.0386781	.1530931	0.25	0.801	-.261379	.3387351
barrier	-.4162926	.1046254	-3.98	0.000	-.6213545	-.2112306
surf_typ	.0946816	.0742292	1.28	0.202	-.050805	.2401683
lnwdt13	-.0783337	.0898913	-0.87	0.384	-.2545174	.09785
nolanes5	.4583569	.1339467	3.42	0.001	.1958261	.7208877
_cons	-.6906927	.5856986	-1.18	0.238	-1.838641	.4572555
/lnalpha	-.9649466	.1207726			-1.201657	-.7282366
alpha	.3810036	.0460148			.3006957	.4827595

Likelihood-ratio test of alpha=0: chibar2(01) = 186.65 Prob>=chibar2 = 0.000

Table C.20 Daytime Crash Frequency at Rural Interchanges (Lighting Type)

```
Negative binomial regression
Dispersion = mean
Log likelihood = -1815.4653
Number of obs = 776
LR chi2(13) = 357.00
Prob > chi2 = 0.0000
Pseudo R2 = 0.0895
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
diamond	.251114	.1079995	2.33	0.020	.0394388	.4627892
full	-.0136433	.1041885	-0.13	0.896	-.2178489	.1905623
partial	.1693693	.0839384	2.02	0.044	.004853	.3338856
continuo	1.054558	.3880196	2.72	0.007	.2940538	1.815063
speed	-.0171668	.0065733	-2.61	0.009	-.0300503	-.0042833
lntotent	.2524002	.032255	7.83	0.000	.1891816	.3156189
perhv	-.0211035	.0069488	-3.04	0.002	-.0347229	-.0074841
fullacc	.7322125	.1211774	6.04	0.000	.4947092	.9697157
paracc	.2587625	.1446463	1.79	0.074	-.0247391	.5422641
barrier	-.3906584	.1007425	-3.88	0.000	-.5881101	-.1932067
surf_typ	.2379575	.0724395	3.28	0.001	.0959787	.3799364
lnwdt13	-.2472917	.0873613	-2.83	0.005	-.4185167	-.0760667
nolanes5	.3772514	.1336087	2.82	0.005	.1153831	.6391198
_cons	-.351644	.5578122	-0.63	0.528	-1.444936	.7416479
/lnalpha	-.7201592	.0847137			-.886195	-.5541234
alpha	.4866748	.041228			.4122213	.5745757

Likelihood-ratio test of alpha=0: chibar2(01) = 810.10 Prob>=chibar2 = 0.000

Table C.21 Nighttime Crash Frequency at Diamond Interchanges (Lighting Type)

```
Negative binomial regression
Dispersion      = mean
Log likelihood  = -3968.4534
Number of obs   =      1615
LR chi2(13)    =      733.89
Prob > chi2     =      0.0000
Pseudo R2      =      0.0846
```

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
urbsub	.2125802	.0726168	2.93	0.003	.070254	.3549065
full	.1559083	.0855143	1.82	0.068	-.0116967	.3235133
partial	.1455504	.0810008	1.80	0.072	-.0132082	.3043091
continuo	.4176826	.1075653	3.88	0.000	.2068584	.6285068
speed	-.0035751	.0032585	-1.10	0.273	-.0099617	.0028114
lntotent	.1301624	.0205571	6.33	0.000	.0898712	.1704536
perhv	-.0341892	.0060722	-5.63	0.000	-.0460904	-.0222879
fullacc	.6228469	.0830713	7.50	0.000	.4600303	.7856636
paracc	.2292486	.1079074	2.12	0.034	.017754	.4407433
barrier	.0047306	.0546888	0.09	0.931	-.1024575	.1119186
surf_typ	-.0763703	.0474733	-1.61	0.108	-.1694163	.0166757
lnwdt13	-.1481807	.0737065	-2.01	0.044	-.2926428	-.0037185
nolanes5	.423604	.056806	7.46	0.000	.3122663	.5349417
_cons	-.1061979	.2768938	-0.38	0.701	-.6488997	.4365039
/lnalpha	-.7098989	.0559341			-.8195276	-.6002701
alpha	.4916939	.0275024			.4406397	.5486634

Likelihood-ratio test of alpha=0: chibar2(01) = 1799.77 Prob>=chibar2 = 0.000

Table C.22 Daytime Crash Frequency at Diamond Interchanges (Lighting Type)

```
Negative binomial regression
Dispersion      = mean
Log likelihood  = -5019.5691
Number of obs   =      1615
LR chi2(13)    =     1171.63
Prob > chi2     =      0.0000
Pseudo R2      =      0.1045
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
urbsub	.3051294	.0681999	4.47	0.000	.1714601	.4387987
full	.3128049	.0811578	3.85	0.000	.1537386	.4718712
partial	.2676838	.0765427	3.50	0.000	.1176628	.4177048
continuo	.495613	.1031926	4.80	0.000	.2933593	.6978667
speed	-.0123486	.0031986	-3.86	0.000	-.0186178	-.0060794
lntotent	.170865	.0196581	8.69	0.000	.1323358	.2093942
perhv	-.0507671	.0059383	-8.55	0.000	-.0624059	-.0391283
fullacc	.7133024	.0776562	9.19	0.000	.5610989	.8655058
paracc	.3174688	.0999074	3.18	0.001	.1216539	.5132837
barrier	.068438	.0523944	1.31	0.191	-.0342532	.1711292
surf_typ	.028891	.0463215	0.62	0.533	-.0618974	.1196794
lnwdt13	-.3398784	.0704617	-4.82	0.000	-.4779807	-.201776
nolanes5	.3717906	.0546911	6.80	0.000	.2645981	.4789831
_cons	.6581536	.269108	2.45	0.014	.1307116	1.185596
/lnalpha	-.6019253	.0442839			-.6887201	-.5151305
alpha	.547756	.0242568			.5022185	.5974226

Likelihood-ratio test of alpha=0: chibar2(01) = 6793.88 Prob>=chibar2 = 0.000

Table C.23 Nighttime Crash Frequency at Non-diamond Interchanges (Lighting Type)

```

Negative binomial regression
Dispersion      = mean
Log likelihood = -1072.7903
Number of obs   =      406
LR chi2(13)    =      270.87
Prob > chi2    =      0.0000
Pseudo R2     =      0.1121
    
```

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
urbsub	.1248347	.1484617	0.84	0.400	-.1661449	.4158143
full	.2035552	.1841166	1.11	0.269	-.1573067	.5644172
partial	.1878414	.1765698	1.06	0.287	-.158229	.5339118
continuo	.1700752	.2191404	0.78	0.438	-.2594322	.5995825
speed	-.0086179	.005717	-1.51	0.132	-.0198231	.0025873
lntotent	.6849858	.0821675	8.34	0.000	.5239404	.8460312
perhv	.0204653	.0148336	1.38	0.168	-.008608	.0495387
fullacc	.3790001	.1295413	2.93	0.003	.1251039	.6328964
paracc	.1406452	.1700513	0.83	0.408	-.1926493	.4739397
barrier	.363226	.0928127	3.91	0.000	.1813165	.5451355
surf_typ	-.0117255	.0821484	-0.14	0.886	-.1727334	.1492824
lnwdt13	.3016958	.1514532	1.99	0.046	.004853	.5985387
nolanes5	-.1619467	.0961415	-1.68	0.092	-.3503805	.0264872
_cons	-6.26873	.9754592	-6.43	0.000	-8.180595	-4.356865
-----						
/lnalpha	-.9891551	.1080902			-1.201008	-.7773021
-----						
alpha	.3718908	.0401978			.3008908	.4596444
-----						

Likelihood-ratio test of alpha=0: chibar2(01) = 470.86 Prob>=chibar2 = 0.000

Table C.24 Daytime Crash Frequency at Non-diamond Interchanges (Lighting Type)

```

Negative binomial regression
Dispersion      = mean
Log likelihood = -1342.6007
Number of obs   =      406
LR chi2(13)    =      348.08
Prob > chi2    =      0.0000
Pseudo R2     =      0.1148
    
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
urbsub	.3271697	.1356175	2.41	0.016	.0613642	.5929752
full	.0906225	.165918	0.55	0.585	-.2345708	.4158157
partial	-.0255347	.1588141	-0.16	0.872	-.3368046	.2857352
continuo	.0864141	.2012844	0.43	0.668	-.3080961	.4809243
speed	-.0005987	.0055803	-0.11	0.915	-.0115359	.0103384
lntotent	.7283955	.0735428	9.90	0.000	.5842543	.8725368
perhv	-.0016569	.0134777	-0.12	0.902	-.0280727	.0247589
fullacc	.2757798	.1218686	2.26	0.024	.0369217	.5146378
paracc	.2158403	.1509708	1.43	0.153	-.0800571	.5117377
barrier	.363756	.0878199	4.14	0.000	.1916323	.5358798
surf_typ	-.0162186	.0763145	-0.21	0.832	-.1657923	.1333551
lnwdt13	.2938381	.1374394	2.14	0.033	.0244618	.5632144
nolanes5	-.2153681	.0908847	-2.37	0.018	-.3934988	-.0372373
_cons	-6.242172	.884343	-7.06	0.000	-7.975452	-4.508891
-----						
/lnalpha	-.920495	.087857			-1.092691	-.7482985
-----						
alpha	.3983218	.0349953			.3353128	.473171
-----						

Likelihood-ratio test of alpha=0: chibar2(01) = 1420.72 Prob>=chibar2 = 0.000



Table C.25 Nighttime Crash Frequency at Urban Diamond Interchanges (Lighting Type)

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -1231.5924
Number of obs   =      466
LR chi2(12)    =      292.56
Prob > chi2    =      0.0000
Pseudo R2     =      0.1062
    
```

nightttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
full	.5600503	.2180803	2.57	0.010	.1326208	.9874797
partial	.7344886	.2179416	3.37	0.001	.3073309	1.161646
continuo	.7270632	.2419297	3.01	0.003	.2528897	1.201237
speed	.0035578	.0051365	0.69	0.489	-.0065097	.0136252
lntotent	.1772599	.0388581	4.56	0.000	.1010994	.2534204
perhv	-.0875188	.0130346	-6.71	0.000	-.1130661	-.0619714
fullacc	.4184602	.1564349	2.67	0.007	.1118533	.725067
paracc	.1255205	.194602	0.65	0.519	-.2558925	.5069334
barrier	.1130591	.0953088	1.19	0.236	-.0737427	.2998608
surf_typ	-.1132147	.088925	-1.27	0.203	-.2875046	.0610752
lnwdt13	-.173215	.1367571	-1.27	0.205	-.441254	.094824
nolan5	.598687	.1071284	5.59	0.000	.3887192	.8086548
_cons	-.7833711	.4942474	-1.58	0.113	-1.752078	.185336
/lnalpha	-.6597377	.0986081			-.853006	-.4664694
alpha	.5169869	.0509791			.4261321	.6272128

Likelihood-ratio test of alpha=0: chibar2(01) = 713.20 Prob>=chibar2 = 0.000

Table C.26 Daytime Crash Frequency at Urban Diamond Interchanges (Lighting Type)

```

Negative binomial regression
Dispersion      = mean
Log likelihood  = -1589.2177
Number of obs   =      466
LR chi2(12)    =      327.19
Prob > chi2    =      0.0000
Pseudo R2     =      0.0933
    
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
full	.7000366	.1981071	3.53	0.000	.3117538	1.088319
partial	.782898	.1997471	3.92	0.000	.3914008	1.174395
continuo	.775838	.2248789	3.45	0.001	.3350835	1.216592
speed	-.0004519	.0050899	-0.09	0.929	-.0104279	.0095241
lntotent	.1950326	.0386205	5.05	0.000	.1193377	.2707274
perhv	-.1025425	.0123189	-8.32	0.000	-.126687	-.078398
fullacc	.3802499	.1518463	2.50	0.012	.0826366	.6778633
paracc	.1532543	.1845147	0.83	0.406	-.208388	.5148965
barrier	.2757623	.0936338	2.95	0.003	.0922435	.4592811
surf_typ	-.0066816	.0886592	-0.08	0.940	-.1804504	.1670871
lnwdt13	-.454892	.1323436	-3.44	0.001	-.7142807	-.1955033
nolan5	.4382126	.1087254	4.03	0.000	.2251146	.6513105
_cons	.1419965	.4866766	0.29	0.770	-.811872	1.095865
/lnalpha	-.4968215	.0769223			-.6475864	-.3460566
alpha	.6084616	.0468042			.5233073	.7074724

Likelihood-ratio test of alpha=0: chibar2(01) = 2840.05 Prob>=chibar2 = 0.000

Table C.27 Nighttime Crash Frequency at Urban Non-diamond Interchanges  
(Lighting Type)

```
Negative binomial regression      Number of obs =      120
LR chi2(11) =      76.34
Dispersion = mean                Prob > chi2 =      0.0000
Log likelihood = -370.56565      Pseudo R2 =      0.0934
```

nightttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]
full	.4545781	.2465339	1.84	0.065	-.0286195 .9377757
partial	.4337998	.2754187	1.58	0.115	-.1060109 .9736105
speed	-.0152856	.0101833	-1.50	0.133	-.0352445 .0046732
lntotent	.5448123	.2230273	2.44	0.015	.1076868 .9819378
perhv	.078321	.0563747	1.39	0.165	-.0321715 .1888134
fullacc	1.174483	.371772	3.16	0.002	.4458229 1.903142
paracc	.6371858	.4356302	1.46	0.144	-.2166337 1.491005
barrier	.6055226	.2191533	2.76	0.006	.1759901 1.035055
surf_typ	-.2456323	.1539256	-1.60	0.111	-.5473209 .0560563
lnwdt13	.623976	.303799	2.05	0.040	.0285409 1.219411
nolanes5	-.010661	.1624301	-0.07	0.948	-.3290182 .3076962
_cons	-5.337056	2.550683	-2.09	0.036	-10.3363 -.33781
/lnalpha	-.9372173	.1724746			-1.275261 -.5991733
alpha	.3917164	.0675611			.279358 .5492655

Likelihood-ratio test of alpha=0: chibar2(01) = 222.16 Prob>=chibar2 = 0.000

Table C.28 Daytime Crash Frequency at Urban Non-diamond Interchanges  
(Lighting Type)

```
Negative binomial regression      Number of obs =      120
LR chi2(11) =      123.30
Dispersion = mean                Prob > chi2 =      0.0000
Log likelihood = -434.43032      Pseudo R2 =      0.1243
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]
full	.4734692	.1953083	2.42	0.015	.0906719 .8562664
partial	.3988096	.2198603	1.81	0.070	-.0321087 .8297278
speed	-.0022131	.0083227	-0.27	0.790	-.0185252 .0140991
lntotent	.7188654	.1718031	4.18	0.000	.3821376 1.055593
perhv	.0844686	.0439908	1.92	0.055	-.0017518 .170689
fullacc	.733237	.2636334	2.78	0.005	.216525 1.249949
paracc	.6437047	.327587	1.96	0.049	.001646 1.285763
barrier	.7450055	.1742896	4.27	0.000	.4034043 1.086607
surf_typ	-.3780411	.1211872	-3.12	0.002	-.6155635 -.1405186
lnwdt13	.6597441	.2419108	2.73	0.006	.1856076 1.133881
nolanes5	-.1425303	.1320049	-1.08	0.280	-.401255 .1161945
_cons	-6.942101	1.985387	-3.50	0.000	-10.83339 -3.050814
/lnalpha	-1.329501	.1617878			-1.6466 -1.012403
alpha	.2646092	.0428106			.1927041 .3633449

Likelihood-ratio test of alpha=0: chibar2(01) = 357.46 Prob>=chibar2 = 0.000

Table C.29 Nighttime Crash Frequency at Rural Diamond Interchanges (Lighting Type)

```

Negative binomial regression
Dispersion      = mean
Log likelihood = -2691.7711
Number of obs   =      1149
LR chi2(12)    =      443.61
Prob > chi2    =      0.0000
Pseudo R2     =      0.0761
    
```

nighttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
full	.4022339	.0907031	4.43	0.000	.2244591	.5800087
partial	.1805795	.0855958	2.11	0.035	.0128148	.3483442
continuo	.6680329	.1250235	5.34	0.000	.4229912	.9130745
speed	-.0081448	.0040414	-2.02	0.044	-.0160659	-.0002238
lntotent	.1389713	.0230366	6.03	0.000	.0938203	.1841222
perhv	-.025811	.006278	-4.11	0.000	-.0381157	-.0135063
fullacc	.6692238	.0970382	6.90	0.000	.4790324	.8594151
paracc	.209954	.1297849	1.62	0.106	-.0444198	.4643277
barrier	-.1529727	.0674982	-2.27	0.023	-.2852668	-.0206786
surf_typ	-.0468044	.054372	-0.86	0.389	-.1533715	.0597627
lnwdt13	-.1782746	.0868645	-2.05	0.040	-.3485259	-.0080234
nolan5	.2481416	.0659828	3.76	0.000	.1188177	.3774655
_cons	.0604212	.3409122	0.18	0.859	-.6077544	.7285969
/lnalpha	-.879225	.0726006			-1.021519	-.7369305
alpha	.4151045	.0301368			.3600474	.4785807

Likelihood-ratio test of alpha=0: chibar2(01) = 823.12 Prob>=chibar2 = 0.000

Table C.30 Daytime Crash Frequency at Rural Diamond Interchanges (Lighting Type)

```

Negative binomial regression
Dispersion      = mean
Log likelihood = -3396.894
Number of obs   =      1149
LR chi2(12)    =      851.66
Prob > chi2    =      0.0000
Pseudo R2     =      0.1114
    
```

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
full	.5352535	.0876326	6.11	0.000	.3634967	.7070103
partial	.2806184	.0815224	3.44	0.001	.1208375	.4403994
continuo	.7688094	.1213595	6.33	0.000	.5309492	1.00667
speed	-.0233217	.0039565	-5.89	0.000	-.0310763	-.0155672
lntotent	.1940611	.0221872	8.75	0.000	.150575	.2375472
perhv	-.0434733	.0062153	-6.99	0.000	-.0556551	-.0312915
fullacc	.8891747	.0914814	9.72	0.000	.7098744	1.068475
paracc	.3817694	.1217049	3.14	0.002	.1432323	.6203066
barrier	-.1017126	.0646759	-1.57	0.116	-.2284752	.0250499
surf_typ	.0055046	.053035	0.10	0.917	-.0984422	.1094513
lnwdt13	-.3118469	.0835229	-3.73	0.000	-.4755487	-.1481451
nolan5	.3275902	.0632632	5.18	0.000	.2035966	.4515839
_cons	1.068946	.3292504	3.25	0.001	.4236272	1.714265
/lnalpha	-.7281015	.0554411			-.8367641	-.619439
alpha	.4828247	.0267683			.4331098	.5382463

Likelihood-ratio test of alpha=0: chibar2(01) = 3569.16 Prob>=chibar2 = 0.000

**Table C.31 Nighttime Crash Frequency at Rural Non-diamond Interchanges  
(Lighting Type)**

Negative binomial regression		Number of obs	=	286
		LR chi2(12)	=	184.69
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -680.98324	Pseudo R2	=	0.1194

nightttim	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
full	.2586021	.1757134	1.47	0.141	-.0857899	.6029941
partial	.246244	.1715155	1.44	0.151	-.0899202	.5824082
continuo	.5259468	.2183847	2.41	0.016	.0979206	.9539731
speed	-.0003231	.006417	-0.05	0.960	-.0129001	.012254
lntotent	.7319519	.0858068	8.53	0.000	.5637738	.9001301
perhv	.0315855	.0137803	2.29	0.022	.0045766	.0585944
fullacc	.2104543	.1412358	1.49	0.136	-.0663628	.4872713
paracc	.1425024	.1819403	0.78	0.433	-.2140939	.4990988
barrier	.143729	.1116889	1.29	0.198	-.0751772	.3626353
surf_typ	.0408278	.0943689	0.43	0.665	-.1441318	.2257874
lnwdt13	.1418625	.1764717	0.80	0.421	-.2040157	.4877407
nolanes5	-.120154	.1156918	-1.04	0.299	-.3469058	.1065978
_cons	-7.330818	1.091274	-6.72	0.000	-9.469676	-5.191959
/lnalpha	-1.366836	.1677465			-1.695613	-1.038059
alpha	.2549123	.0427606			.1834867	.3541415

Likelihood-ratio test of alpha=0: chibar2(01) = 119.51 Prob>=chibar2 = 0.000

**Table C.32 Daytime Crash Frequency at Rural Non-diamond Interchanges  
(Lighting Type)**

Negative binomial regression		Number of obs	=	286
		LR chi2(12)	=	215.39
Dispersion	= mean	Prob > chi2	=	0.0000
Log likelihood	= -891.51911	Pseudo R2	=	0.1078

daytime	Coef.	Std. Err.	z	P> z	[95% Conf. Interval]	
full	.237724	.1767991	1.34	0.179	-.1087959	.5842439
partial	-.006474	.1725206	-0.04	0.970	-.3446083	.3316602
continuo	.4430714	.226901	1.95	0.051	-.0016464	.8877891
speed	-.0024781	.0070494	-0.35	0.725	-.0162947	.0113386
lntotent	.7055969	.0848468	8.32	0.000	.5393003	.8718934
perhv	-.0122576	.0141763	-0.86	0.387	-.0400426	.0155275
fullacc	.3287317	.1492835	2.20	0.028	.0361414	.6213221
paracc	.2392197	.1806743	1.32	0.185	-.1148955	.5933349
barrier	.0771245	.1186562	0.65	0.516	-.1554374	.3096864
surf_typ	.1227255	.0983114	1.25	0.212	-.0699613	.3154124
lnwdt13	.1283808	.167984	0.76	0.445	-.2008618	.4576234
nolanes5	-.1824885	.1205776	-1.51	0.130	-.4188163	.0538393
_cons	-5.766343	1.09359	-5.27	0.000	-7.909739	-3.622947
/lnalpha	-.8880867	.109885			-1.103457	-.6727161
alpha	.4114422	.0452113			.3317222	.5103206

Likelihood-ratio test of alpha=0: chibar2(01) = 820.95 Prob>=chibar2 = 0.000

Table C.33 Log-linear Regression Model of Urban Interchanges

Source	SS	df	MS	Number of obs = 1139		
Model	12.4272795	11	1.12975268	F( 11, 1127)	=	2.77
Residual	460.277195	1127	.408409224	Prob > F	=	0.0015
				R-squared	=	0.0263
				Adj R-squared	=	0.0168
Total	472.704474	1138	.415381788	Root MSE	=	.63907

lnntoday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
diamond	-.1277896	.0585071	-2.18	0.029	-.2425847	-.0129945
light	-.2306861	.1328849	-1.74	0.083	-.4914156	.0300435
speed	.0018104	.0024822	0.73	0.466	-.0030599	.0066808
lntotent	-.0288369	.0206638	-1.40	0.163	-.0693807	.0117069
perhv	.0215339	.0071606	3.01	0.003	.0074842	.0355835
paracc	-.0275371	.0888615	-0.31	0.757	-.2018897	.1468155
fullacc	-.0385467	.0675241	-0.57	0.568	-.1710337	.0939404
barrier	-.0258315	.0444998	-0.58	0.562	-.1131432	.0614802
surf_typ	-.0484136	.0403932	-1.20	0.231	-.127668	.0308408
lnwdt13	.0283369	.0752873	0.38	0.707	-.1193822	.1760561
nolanes5	.0157572	.0445332	0.35	0.724	-.0716202	.1031346
_cons	-.4270475	.2867746	-1.49	0.137	-.9897196	.1356246

Table C.34 Log-linear Regression Model of Rural Interchanges

Source	SS	df	MS	Number of obs = 540		
Model	37.1319621	11	3.37563292	F( 11, 528)	=	5.61
Residual	317.899786	528	.602082929	Prob > F	=	0.0000
				R-squared	=	0.1046
				Adj R-squared	=	0.0859
Total	355.031748	539	.65868599	Root MSE	=	.77594

lnntoday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
diamond	-.2663474	.1136009	-2.34	0.019	-.4895127	-.0431821
light	.1221284	.0793937	1.54	0.125	-.0338378	.2780947
speed	.0094993	.007342	1.29	0.196	-.0049239	.0239224
lntotent	-.1425275	.0336019	-4.24	0.000	-.2085374	-.0765176
perhv	.0156582	.0067593	2.32	0.021	.0023798	.0289367
paracc	-.0878803	.1531726	-0.57	0.566	-.3887829	.2130222
fullacc	-.1639949	.125753	-1.30	0.193	-.4110324	.0830427
barrier	.0894413	.1097379	0.82	0.415	-.1261352	.3050178
surf_typ	-.1574963	.0749011	-2.10	0.036	-.304637	-.0103556
lnwdt13	.2165555	.0906839	2.39	0.017	.0384099	.3947011
nolanes5	-.0116052	.1330552	-0.09	0.931	-.2729878	.2497774
_cons	.3341513	.5993671	0.56	0.577	-.8432856	1.511588

Table C.35 Log-linear Regression Model of Diamond Interchanges

Source	SS	df	MS	Number of obs = 1315		
Model	125.303878	11	11.3912616	F( 11, 1303)	=	24.02
Residual	617.896043	1303	.474210317	Prob > F	=	0.0000
				R-squared	=	0.1686
				Adj R-squared	=	0.1616
Total	743.199921	1314	.565601157	Root MSE	=	.68863

lnntoday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
urbsub	-.213694	.060704	-3.52	0.000	-.3327823	-.0946057
light	-.0324865	.0659919	-0.49	0.623	-.1619485	.0969755
speed	.0044613	.0027853	1.60	0.109	-.0010029	.0099256
lntotent	-.0715767	.0181825	-3.94	0.000	-.1072469	-.0359065
perhv	.0193533	.0049325	3.92	0.000	.0096767	.0290299
paracc	-.032899	.0941285	-0.35	0.727	-.2175589	.1517609
fullacc	-.0819577	.0718943	-1.14	0.255	-.222999	.0590835
barrier	.0159106	.0481889	0.33	0.741	-.0786258	.110447
surf_typ	-.1221316	.041329	-2.96	0.003	-.2032102	-.0410529
lnwdt13	.1826476	.0611144	2.99	0.003	.0627542	.3025409
nolanes5	.0090661	.0500098	0.18	0.856	-.0890424	.1071745
_cons	-.2098914	.238285	-0.88	0.379	-.6773556	.2575728

Table C.36 Log-linear Regression Model of Non-diamond Interchanges

Source	SS	df	MS	Number of obs = 364		
Model	19.6642047	11	1.78765497	F( 11, 352)	=	3.86
Residual	162.843429	352	.462623377	Prob > F	=	0.0000
				R-squared	=	0.1077
				Adj R-squared	=	0.0799
Total	182.507633	363	.50277585	Root MSE	=	.68016

lnntoday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
urbsub	-.2136579	.1252144	-1.71	0.089	-.4599203	.0326044
light	.1086375	.150848	0.72	0.472	-.1880393	.4053142
speed	.0015166	.0050659	0.30	0.765	-.0084467	.0114798
lntotent	-.1633519	.0758218	-2.15	0.032	-.3124726	-.0142313
perhv	.0127651	.0126003	1.01	0.312	-.0120163	.0375464
paracc	-.206686	.1409019	-1.47	0.143	-.4838015	.0704294
fullacc	-.00316	.1116985	-0.03	0.977	-.2228403	.2165203
barrier	-.0329334	.0867688	-0.38	0.705	-.2035838	.1377171
surf_typ	.0579744	.0752334	0.77	0.441	-.0899891	.2059378
lnwdt13	-.1866263	.1410135	-1.32	0.187	-.4639613	.0907086
nolanes5	.0132089	.0929819	0.14	0.887	-.169661	.1960789
_cons	1.030769	.9022968	1.14	0.254	-.7438022	2.80534

Table C.37 Log-linear Regression Model of Urban Diamond Interchanges

Source	SS	df	MS	Number of obs = 874		
Model	13.3906757	10	1.33906757	F( 10, 863)	=	3.30
Residual	350.041654	863	.405610259	Prob > F	=	0.0003
				R-squared	=	0.0368
				Adj R-squared	=	0.0257
Total	363.432329	873	.416302783	Root MSE	=	.63688

lnntoday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
light	-.2250823	.140891	-1.60	0.111	-.5016115	.0514468
speed	.0031459	.0028252	1.11	0.266	-.0023992	.0086909
lntotent	-.0287067	.0214944	-1.34	0.182	-.0708942	.0134807
perhv	.0210535	.007623	2.76	0.006	.0060917	.0360153
paracc	-.0358858	.1068343	-0.34	0.737	-.2455714	.1737997
fullacc	-.0618309	.0822548	-0.75	0.452	-.2232737	.099612
barrier	-.0029985	.0515564	-0.06	0.954	-.1041891	.0981921
surf_typ	-.1318887	.0466347	-2.83	0.005	-.2234194	-.040358
lnwdt13	.1286007	.0831545	1.55	0.122	-.0346081	.2918095
nolanes5	.0343464	.0508729	0.68	0.500	-.0655028	.1341956
_cons	-.6019637	.2789425	-2.16	0.031	-1.149449	-.0544786

Table C.38 Log-linear Regression Model of Urban Non-diamond Interchanges

Source	SS	df	MS	Number of obs = 265		
Model	6.24433639	10	.624433639	F( 10, 254)	=	1.55
Residual	102.447777	254	.403337703	Prob > F	=	0.1228
				R-squared	=	0.0574
				Adj R-squared	=	0.0203
Total	108.692113	264	.411712549	Root MSE	=	.63509

lnntoday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
light	-.3722796	.4348493	-0.86	0.393	-1.228649	.4840897
speed	-.0042373	.0053472	-0.79	0.429	-.0147678	.0062932
lntotent	-.0814159	.0921319	-0.88	0.378	-.2628557	.1000239
perhv	.0214624	.0244337	0.88	0.381	-.026656	.0695808
paracc	-.154575	.1752647	-0.88	0.379	-.4997322	.1905821
fullacc	.0513421	.1280509	0.40	0.689	-.2008347	.3035188
barrier	-.0606219	.093055	-0.65	0.515	-.2438794	.1226357
surf_typ	.215198	.0832542	2.58	0.010	.0512415	.3791546
lnwdt13	-.4020498	.1821883	-2.21	0.028	-.7608419	-.0432578
nolanes5	-.0210153	.0975534	-0.22	0.830	-.2131318	.1711013
_cons	.5407038	1.142283	0.47	0.636	-1.708849	2.790257

Table C.39 Log-linear Regression Model of Rural Diamond Interchanges

Source	SS	df	MS	Number of obs =		
				441		
Model	32.2806687	10	3.22806687	F( 10, 430)	=	5.30
Residual	261.654111	430	.608497933	Prob > F	=	0.0000
				R-squared	=	0.1098
				Adj R-squared	=	0.0891
Total	293.93478	440	.668033591	Root MSE	=	.78006

lnntoday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
light	.0821958	.0891911	0.92	0.357	-.093109	.2575005
speed	.0064064	.0092051	0.70	0.487	-.0116861	.024499
lntotent	-.1348812	.0355562	-3.79	0.000	-.2047669	-.0649956
perhv	.0169776	.0074324	2.28	0.023	.0023694	.0315859
paracc	.0213879	.1923734	0.11	0.912	-.3567213	.3994971
fullacc	-.1382005	.1589182	-0.87	0.385	-.4505537	.1741526
barrier	.1102506	.1248885	0.88	0.378	-.1352173	.3557186
surf_typ	-.102286	.0852856	-1.20	0.231	-.2699146	.0653426
lnwdt13	.2211673	.0998911	2.21	0.027	.0248316	.4175029
nolanes5	-.0854514	.1685862	-0.51	0.613	-.4168069	.2459041
_cons	.1570541	.6543593	0.24	0.810	-1.129087	1.443195

Table C.40 Log-linear Regression Model of Rural Non-diamond Interchanges

Source	SS	df	MS	Number of obs =		
				99		
Model	7.82859818	10	.782859818	F( 10, 88)	=	1.30
Residual	52.9527489	88	.601735783	Prob > F	=	0.2425
				R-squared	=	0.1288
				Adj R-squared	=	0.0298
Total	60.7813471	98	.620217828	Root MSE	=	.77572

lnntoday	Coef.	Std. Err.	t	P> t	[95% Conf. Interval]	
light	.3112015	.2053023	1.52	0.133	-.0967938	.7191968
speed	.0136779	.0141793	0.96	0.337	-.0145004	.0418562
lntotent	-.2007786	.1697885	-1.18	0.240	-.5381976	.1366404
perhv	.0108193	.0184307	0.59	0.559	-.0258079	.0474465
paracc	-.1763366	.2780215	-0.63	0.528	-.7288459	.3761728
fullacc	-.110433	.2778528	-0.40	0.692	-.6626072	.4417411
barrier	-.1033108	.2579074	-0.40	0.690	-.6158476	.4092261
surf_typ	-.3166209	.1683	-1.88	0.063	-.6510818	.01784
lnwdt13	.1304911	.24477	0.53	0.595	-.3559378	.61692
nolanes5	.1300752	.2703075	0.48	0.632	-.407104	.6672545
_cons	.6609799	2.189874	0.30	0.763	-3.690935	5.012894