

APPENDIX G

DESIGN EXAMPLES OF END ZONE REINFORCEMENT

Table of Contents

G.1	EXAMPLE I	G-1
	G.1.1 Design according to the AASHTO LRFD Specifications	G-1
	G.1.2 Design according to the Proposed Detail.....	G-3
G.2	EXAMPLE II	G-4
	G.2.1 Design according to the AASHTO LRFD Specifications	G-4
	G.2.2 Design according to the Proposed Detail.....	G-5

G.1 EXAMPLE I

Design the end zone reinforcement for a 45 in. deep Virginia bulb-T with 38-0.6 in. diameter strands in the bottom flange, and 14-0.6 in. diameter strands in the top portion of the web. The strands are 270 ksi low relaxation strands, tensioned to a stress of 0.75x270 ksi, or a force of 44 kips each. No debonded strands were used. This example is similar to the Virginia specimens used in this study, except that it does not have the extra 4 in. of top flange thickening needed for testing.

G.1.1 Design according to the AASHTO LRFD Specifications

The total prestressing force = $52 \times 44 = 2,288$ kips

The bursting force = $0.04 \times 2,288 = 91.52$ kips

The required steel area = $91.52/20 = 4.58 \text{ in}^2$

$(h/4) = 11.25 \text{ in.}$

Use 6 pairs of #6 bars at @ 2.0 in. spacing

The area of steel = $6*2*0.44 = 5.28 \text{ in}^2 > 4.58 \text{ in}^2$

Use a 1.5 in. space from the member end to the centerline of the first pair of bars. Thus, the clear cover is larger than 1 in. The distance from the end of the member to the centerline of the last pair of bars = $1.5 + (5*2) = 11.5 \text{ in.}$ This is close enough to $h/4 = 11.25 \text{ in.}$

Bottom flange confinement steel is required to be #3@3" for a distance of $1.5h = 67.5 \text{ in.}$ Use $67.5/3 = 23 \text{ #3 bars.}$

The reinforcement details are shown in [Figure G-1](#).

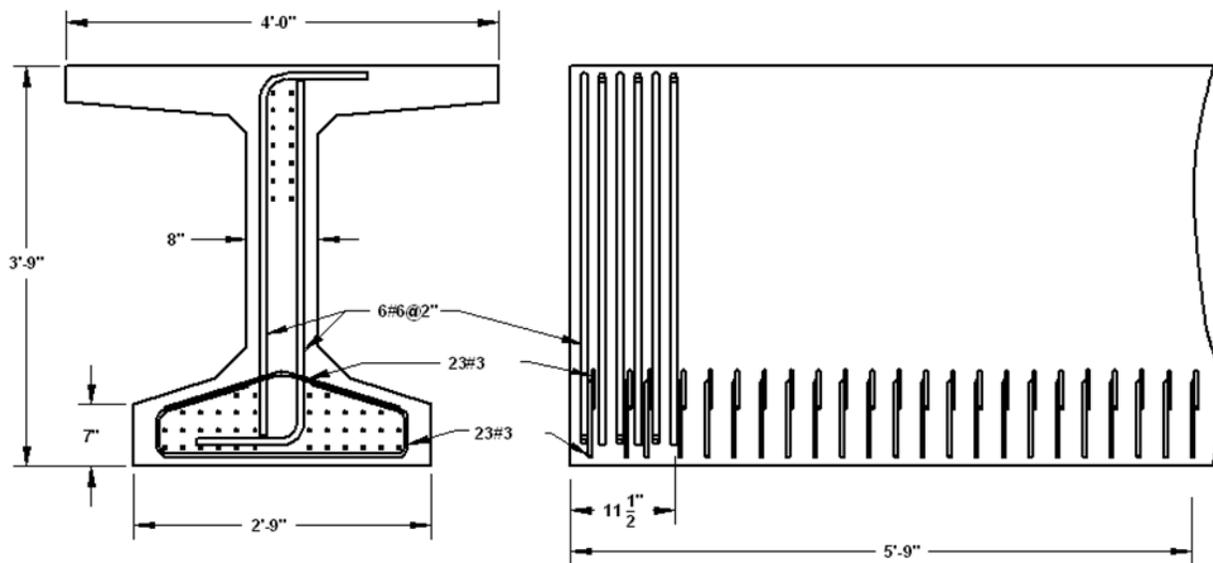


Figure G-1. Reinforcement Details according to the LRFD Specifications

G.1.2 Design according to the Proposed Detail

(1) Fifty percent of the bursting force requires reinforcement area = $0.50 \times 4.58 \text{ in}^2 = 2.29 \text{ in}^2$. It is recommended to be placed within $h/8 = 5.625 \text{ in.}$ from the girder end. Use a single #8 -C shaped bar at the centerline of the web whose centerline is 1.5 in. from the member end. In addition, use a pair of #5 bars on the two web faces at the same 1.5 in. distance from the end. Add one more pair of #5 bars at 3 in. spacing.

Thus, the total distance from the member end to the centerline of the second pair of #5 bars = $1.5 + 3 = 4.5 \text{ in.} < 6.625 \text{ in.}$ The area provide = $0.79 + 4 \times 0.31 = 2.03 \text{ in}^2 < 2.29 \text{ in}^2$. However, as will be shown, the next set of 2#5 bars at 3 inch would contribute more than the required amount of steel within the required $h/8$ distance.

(2) Provide at least 4.58 in^2 in the end $h/2 = 22.5 \text{ in.}$ Of this amount, 2.03 in^2 is already provided in the first 4.5 inch. The remainder is $4.58 - 2.03 = 2.55 \text{ in}^2$, or 5 pairs of #5 bars. Separate calculations, not shown here, for shear design indicate that #5@6 in. is required for shear at the nearest critical section. If 4 additional pairs of #5 are placed at 3 in. spacing and one pair at 6 in., then to total area of steel = $0.79 + (7 \times 0.62) = 5.13 \text{ in}^2 > 4.58 \text{ in}^2$, in a distance = $1.5 + (5 \times 3) + (1 \times 6) = 22.5 \text{ in.} = h/2$ as required.

(3) Use #5 @6 in. for a distance beyond $h/2$, determined by shear design.

(4) Use #3 @ 3 in. bottom flange confinement reinforcement for a distance = $60 \times 0.6 = 36 \text{ in.}$

Details of the end zone reinforcement are given in [Figure G-2](#).

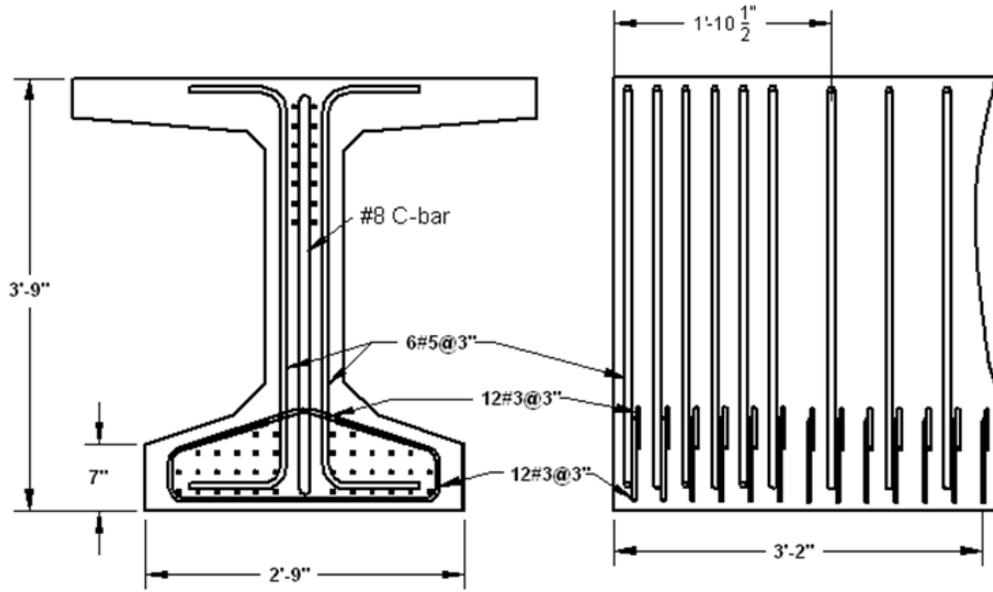


Figure G-2. Reinforcement details according to the proposed method

G.2 EXAMPLE II

Design the end zone reinforcement for the newly introduced Florida I-Beam (FIB). The beam is 45 in. deep. 72-0.6 in. diameter strands are placed in the bottom flange. Of these strands, 10 are debonded at 8 feet from the ends and another 8 strands are debonded at 16 feet from the ends. The strands are tensioned to 44 kips. All strands are straight.

G.2.1 Design according to the AASHTO LRFD Specifications

The prestressing force at the end = $(72 - 10 - 8) * 44 = 2,376$ kips

The bursting force = $0.04 * 2,376 = 95.04$ kips

The required steel area = $95.04k / 20ksi = 4.75$ in²

$h/4 = 11.25$ in.

Use 6 pairs of #6 bars with a clear cover of 1 in. and a spacing of 2 in. Thus, steel area = $6 * 2 * 0.44 = 5.28$ in² over a distance = $1.375 + (5 * 2) = 11.375$ in.

G.2.2 Design according to the Proposed Detail

Use a pair of 1 in. diameter coil rods at 1 in. clear cover, followed by 7 pairs of #5 bars at 3 in. spacing. The pairs of #5 provide the equivalent of $0.62/3 = 0.207 \text{ in}^2/\text{in}$.

The area of bursting steel within a length of 5.625 in. = $2*0.79 + 0.207*(5.625-1.5) = 2.43 \text{ in}^2 > 2.375 \text{ in}^2$

The total area of bursting steel = $1.58 + (7*2*0.31) = 5.92 \text{ in}^2 > 4.75 \text{ in}^2$

It is placed over a distance = $1.5 + (7*3) = 22.5 \text{ in.} = h/2$.

Confinement steel should be provided for a distance of 60 strand diameters, or 36 in., from the end. A second set of confining steel should be provided starting at 8 feet and a third set starting at 16 feet. However, for simplicity, it is recommended to uniformly use #3 at 3 in. for a distance = $16 + (36/12) = 19 \text{ feet}$ from the ends. Details are shown in [Figure G-3](#).

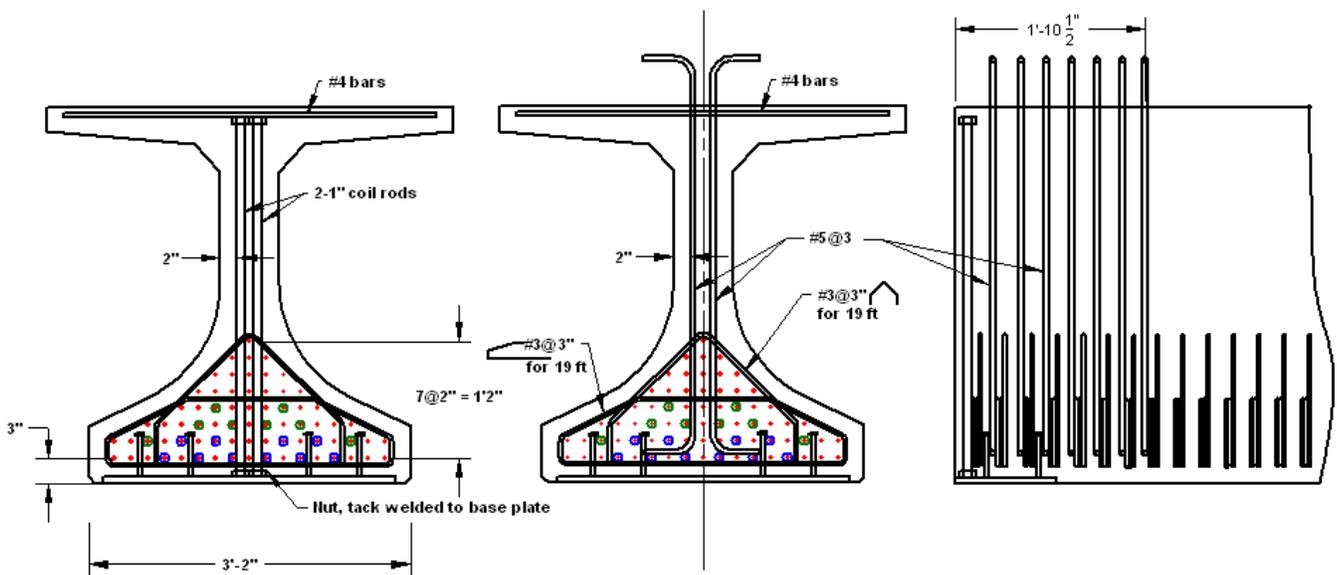


Figure D-3. Web End Reinforcement Details for Example 2