

APPENDIX D. MATERIAL TEST RESULTS

Tensile coupon testing was used to characterize the steel plate used to make the five connection members, gusset plates, and splice plates. Testing was performed according to the ASTM E8-08 Specification. The coupons were CNC machined according to one of the two drawings shown in Figure D1. Sometimes etched or stamped identification marks on the material sample plates interfered with using the full-size Plate-types specimen and instead a Sheet-type specimen were used instead. According to ASTM E8, the sheet type specimen is valid for material thickness up to 0.75 inches thick. All pretest measurements and markings were also performed in accordance to ASTM E8.

Testing was performed on a MTS four-post testing machine with hydraulic wedge grips and a 220 kip capacity. As the project progressed through time, the lab benefitted from certain machine upgrades. Therefore, the testing machine was controlled with either an analog MTS 458.20 controller using an external command or a digital MTS Flex Test 60 controller running MTS Test Works software. The external command came from a personal computer with custom written software that collected load/displacement/strain data and provided a displacement command to the controller. The custom software allowed the user to increase the loading rate in the middle of the test, a function the 458 controller was not capable of performing. The MTS Test Works software was able to integrate the same functionality without an external computer providing the command signal.

Strain measurements were made using one of two extensometers, which depended on the coupon size. One was a clip-on extensometer with a 1 inch measurement range, but was fitted with an extension bar to measure strain over an 8.000 inch gauge length. The second extensometer was also clip-on but had a fixed 2.000 inch gauge length and a 1 inch range, it was used exclusively in testing the Sheet-type coupons.

Specimens were initially loaded at a rate of 0.0003 inch/sec. Once the specimen had yielded, the static yield was attained by pausing the loading for a period of 60-90 seconds in three locations along the yield plateau. Once strain hardening had begun, the loading rate was gradually increased to 0.01 inch/sec until the specimen fractured. Typically it took approximately 20 minutes to fracture a specimen.

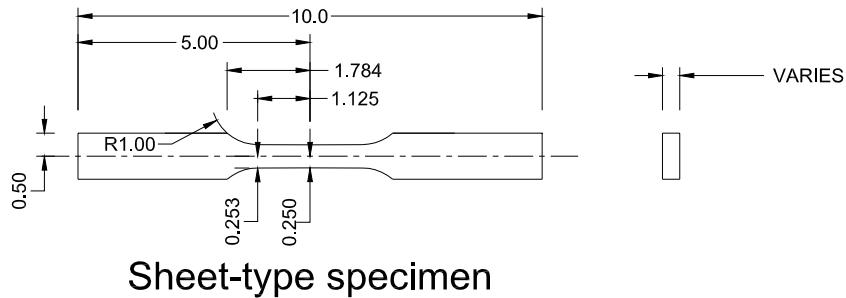
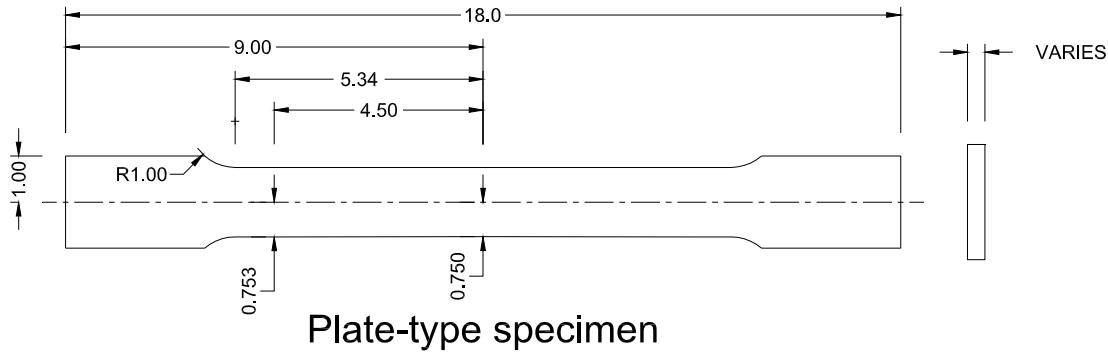


Figure D1. ASTM E8 specimens (units = inches).

GUSSET PLATE MATERIAL

The gusset and splice plates were all cut and drilled on a CNC plate processing machine. Figure D2 shows how the plates for each connection were cut from a single 4' x 20' steel plate. Notice four additional rectangular plates above and to the left of each gusset plate for material characterization. These plates were either etched or stamped with "Long1," "Long2," "Tran1," and "Tran2" proceeded by the specimen designation. Figure D3 shows how the individual coupons were labeled within each of the material characterization plates, note on some of the longitudinal plates location of the identification etch dictated whether a Plate- or Sheet-type coupon was used. In Figure D3 the "m" and the "n" are generic identifications which according to the following denote which plate and connection the coupon came from:

"m" is a capital letter signifying which connection the coupon comes from

- C for GP307SS3
- D for GP307LS3
- E for GP307SL3
- F for GP307SL4
- G for GP307SS3-1
- H for GP307SS3-2
- I for GP490LS3
- J for GP490SS3

- K for GP490SS3-1 South Plate
- L for GP490LS3-1
- M for GP490LS3-2
- N for GP490SS3-1 North plate (original North plate was lost in shipment)
- P for GP307SS3-3
- R for GP307SS3-4
- S for Shingle Plates

“n” is a number signifying which material characterization plate the coupon originated

- 1 for “Long1”
- 2 for “Long2”
- 3 for “Trans1”
- 4 for “Trans2”
- 5 for “Extra” (which is not shown in the figure)

As testing was performed, it was noted that in some of the specimens, there was no difference in the longitudinal or transverse material properties. It was hypothesized that the fabricator did not follow the provided cutting instructions and the material sampling plates were all cut from the same direction. In expectation of this, an extra plate (not shown in Figure D2) was also ordered for each connection with dimensions large enough such that coupons could be cut from two orthogonal directions. For some specimens, the “extra” plate was tested to reaffirm the material properties.

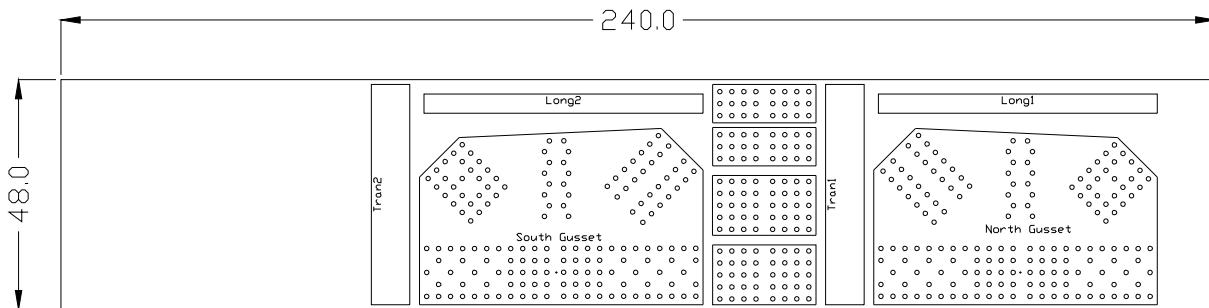


Figure D2. Sample gusset plate cutting pattern.

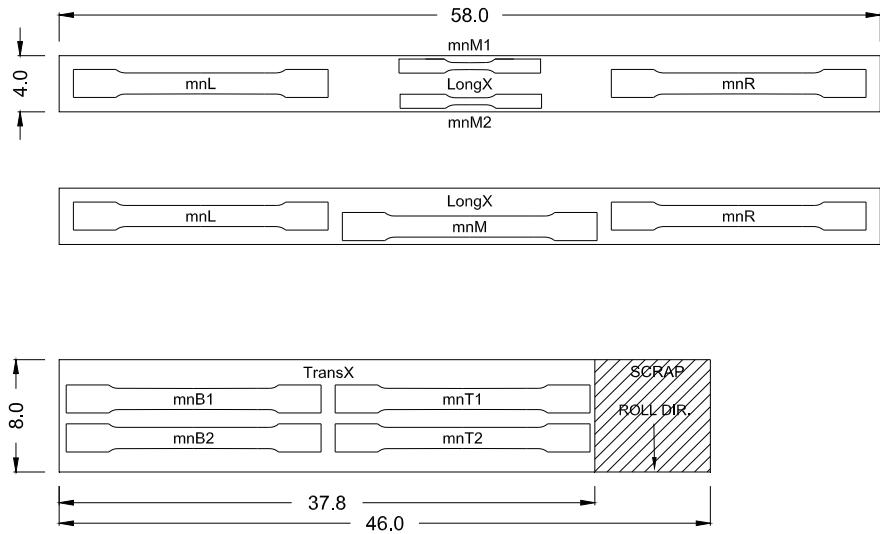


Figure D3. Coupon labeling scheme.

RESULTS

A summary of all the plate specimen properties is presented in Table D1. The data reported are modulus, 0.2% offset yield, static yield, tensile strength, elongation, and area reduction. The data for each batch of coupons is shown in Tables D2 through D15. The data statistics are reported three ways; in the longitudinal rolling direction, transverse rolling direction, and both rolling directions combined. Coupons are identified if they failed the ASTM acceptance criteria for not fracturing in the gauge length and these specimens are therefore not included in the statistical analysis.

Two graphs are presented following each table. The first shows all the engineering stress versus engineering strain data for all coupons, for that particular connection. Longitudinal coupons are plotted in black and transverse in red. The second figure plots the results in terms of true stress versus true plastic strain, this is the form the data must be in to input into the Abaqus finite element analysis. The plastic strain is the total strain with the elastic portion removed. Also shown in this second plot in light blue is the actual material model input into Abaqus. Note the material model was first fit to the average of all the data, then offset downward by the difference between the 0.2% yield and the static yield, therefore the curve represented a nonlinear static yield material model. The final Abaqus inputs for the nonlinear material plate properties for all the Phase 1 and Phase 2 specimens is shown in Table D16 and Table D17 respectively.

For some of the specimens, a smaller Sheet-type coupon was tested, and the 2.000 inch gauge length extensometer was used to monitor elongation. The advantage with this arrangement is the extensometer could remain on the specimen all the way through fracture. Contrast this with the Plate-type specimens that used a 1.000 inch stroke extensometer over an 8.000 inch gauge length that had to be removed prior to failure. As can be seen in the plots for the sheet-type specimens

appear to have more elongation capacity than the plate-type specimens. Because of this inherent difference, the results of the Sheet-type specimens were not included in any of the statistics for elongation. The difference is surely because the stroke of the testing machine was used to calculate strain after extensometer removal for the Plate-type specimens. This aberration would not affect any of the presented results beyond the plots of the stress versus strain data.

Table D1. *Summary of All Specimen Plate Properties*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|----------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| GP307SS3 | 27349 | 38.4 | 36.4 | 62.6 | 26 | 56 |
| GP307LS3 | 29894 | 51.4 | 48.2 | 67.4 | 25 | 66 |
| GP307SL3 | 27774 | 48.6 | 46.6 | 65.0 | 25 | 60 |
| GP307SL4 | 29569 | 35.2 | 33.2 | 61.8 | 23 | 61 |
| GP307SS3-1 | 29190 | 49.9 | 47.2 | 66.3 | 25 | 67 |
| GP307SS3-2 | 29579 | 49.6 | 47.8 | 66.5 | 21 | 64 |
| GP307SS3-3 | 28892 | 39.9 | 37.9 | 63.0 | 27 | 65 |
| GP307SS3-4 | 28984 | 40.2 | 38.0 | 63.0 | 27 | 65 |
| GP490LS3 | 27412 | 47.5 | 45.6 | 63.7 | 23 | 57 |
| GP490SS3 | 28222 | 48.6 | 46.4 | 65.2 | 25 | 66 |
| GP490SS3-1 | 29832 | 48.3 | 45.9 | 66.8 | 27 | 69 |
| GP490LS3-1 | 29825 | 48.7 | 46.2 | 67.3 | 28 | 69 |
| GP490LS3-2 | 29870 | 48.2 | 45.7 | 66.2 | 29 | 69 |
| Shingle plates | 30293 | 48.8 | 46.3 | 66.8 | 27 | 68 |
| Angles | 29725 | 50.8 | 47.1 | 74.3 | 24 | 55 |

NOTE
Shading dictates plates cut from the same parent material. The stiffening angles were hot rolled and obviously not from the same parent as the GP307SS3 plate.

Table D2. *Tensile Coupon Results from GP307SS3 plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|----------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| C1L ^a | 27048 | 38.5 | 36.3 | 63.1 | 25 | 57 |
| C1M | 26587 | 38.0 | 36.1 | 62.6 | 24 | 58 |
| C1R | 26954 | 37.9 | 35.9 | 61.8 | 26 | 57 |
| C2L | 27656 | 38.7 | 36.5 | 63.8 | 24 | 47 |
| C2M | 27117 | 36.4 | 34.6 | 60.3 | 25 | 57 |
| C2R | 28012 | 41.4 | 39.6 | 65.8 | 27 | 54 |
| Average ^b | 27265 | 38.5 | 36.5 | 62.9 | 25 | 54 |
| COV ^b | 0.021 | 0.048 | 0.051 | 0.033 | 0.050 | 0.084 |
| C3B1 ^a | 28692 | 36.8 | 34.0 | 62.6 | 23 | 57 |
| C3B2 | 27450 | 35.6 | 33.4 | 60.1 | 26 | 58 |
| C3T1 | 26852 | 40.2 | 37.9 | 64.1 | 26 | 58 |
| C3T2 | 26961 | 39.0 | 36.9 | 62.3 | 24 | 57 |
| C4B1 ^a | 27749 | 40.5 | 38.1 | 65.4 | 21 | 57 |
| C4B2 ^a | 28065 | 38.7 | 37.0 | 63.4 | 26 | 55 |
| C4T1 | 27684 | 38.4 | 36.8 | 62.9 | 25 | 58 |
| C4T2 | 28211 | 38.6 | 36.2 | 62.6 | 28 | 57 |
| Average ^b | 27432 | 38.4 | 36.2 | 62.4 | 26 | 57 |
| COV ^b | 0.020 | 0.044 | 0.046 | 0.023 | 0.055 | 0.015 |
| Average ^b | 27349 | 38.4 | 36.4 | 62.6 | 26 | 56 |
| COV ^b | 0.020 | 0.043 | 0.046 | 0.027 | 0.051 | 0.062 |

^a – Indicates specimens where fracture occurred outside the original gauge length marks or was located less than 25 % of the elongated gage length from either of the original gauge length marks

^b – Specimens failing ASTM acceptance criteria were not included in statistical analysis

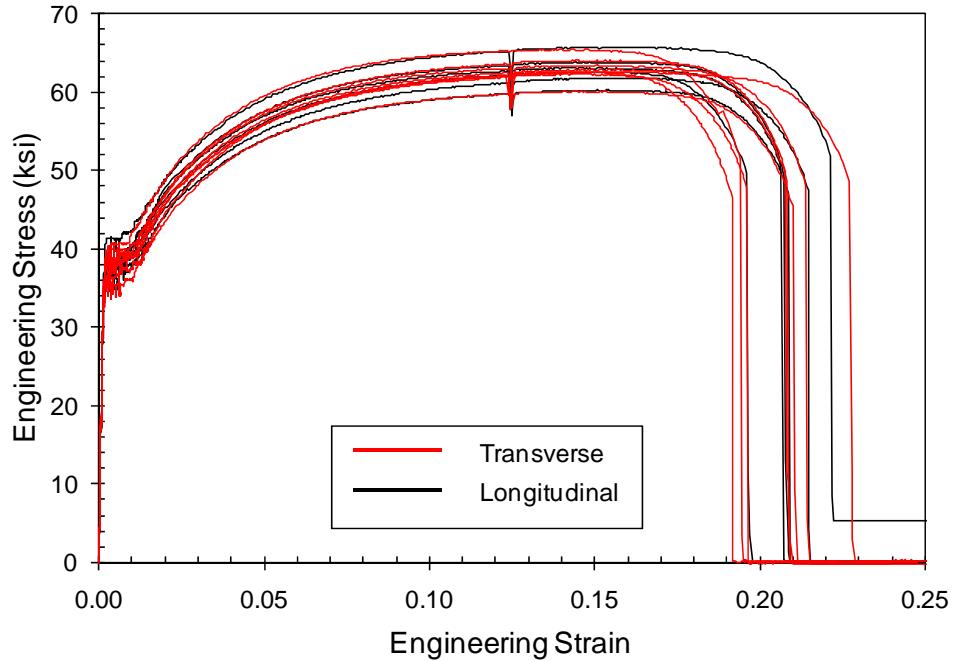


Figure D4. All GP307SS3 coupon engineering stress/engineering strain plots.

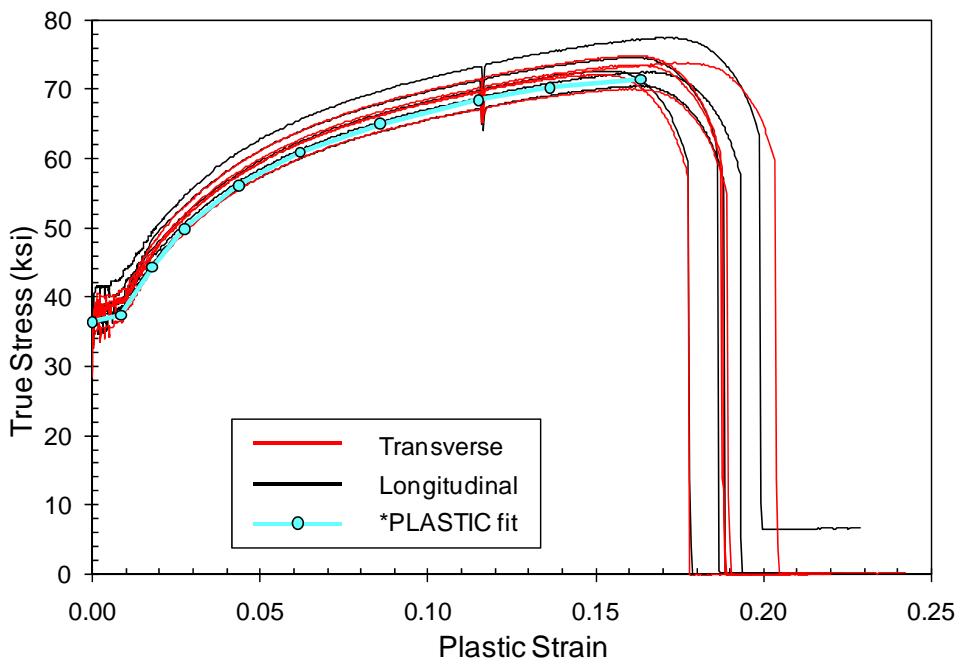


Figure D5. All GP307SS3 coupon true stress/true plastic strain plots (rejected specimens excluded).

Table D3. *Tensile Coupon Results from GP307LS3 plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|----------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| D1L | 29004 | 52.5 | 49.6 | 68.0 | 26 | 61 |
| D1M | 29242 | 53.4 | 50.7 | 69.3 | 27 | 68 |
| D1R | 28441 | 50.3 | 46.6 | 67.7 | 24 | 66 |
| D2L | 30083 | 53.4 | 50.0 | 68.7 | 24 | 66 |
| D2M | 29872 | 52.1 | 48.7 | 68.2 | 23 | 67 |
| D2R ^a | 30203 | 52.0 | 49.5 | 68.7 | 16 | 64 |
| Average ^b | 29328 | 52.3 | 49.1 | 68.4 | 25 | 65 |
| COV ^b | 0.023 | 0.024 | 0.032 | 0.009 | 0.065 | 0.043 |
| D3B1 | 30507 | 51.3 | 48.2 | 66.8 | 24 | 66 |
| D3B2 | 30636 | 51.0 | 46.8 | 66.9 | 25 | 67 |
| D3T1 | 30230 | 51.0 | 48.4 | 66.8 | 26 | 65 |
| D3T2 | 29777 | 51.0 | 47.5 | 66.8 | 24 | 66 |
| D4B1 | 30004 | 50.5 | 48.3 | 66.7 | 25 | 66 |
| D4B2 | 30654 | 50.6 | 47.4 | 66.7 | 25 | 66 |
| D4T1 | 30104 | 50.1 | 47.0 | 65.8 | 25 | 67 |
| D4T2 | 30068 | 51.4 | 47.5 | 67.4 | 26 | 67 |
| Average | 30248 | 50.9 | 47.6 | 66.7 | 25 | 66 |
| COV | 0.011 | 0.009 | 0.013 | 0.007 | 0.025 | 0.011 |
| Average ^b | 29894 | 51.4 | 48.2 | 67.4 | 25 | 66 |
| COV ^b | 0.022 | 0.021 | 0.026 | 0.014 | 0.042 | 0.026 |

^a –indicates specimens where fracture occurred outside the original gauge length marks or was located less than 25 % of the elongated gage length from either of the original gauge length marks.

^b – Specimens failing ASTM acceptance criteria were not included in statistical analysis

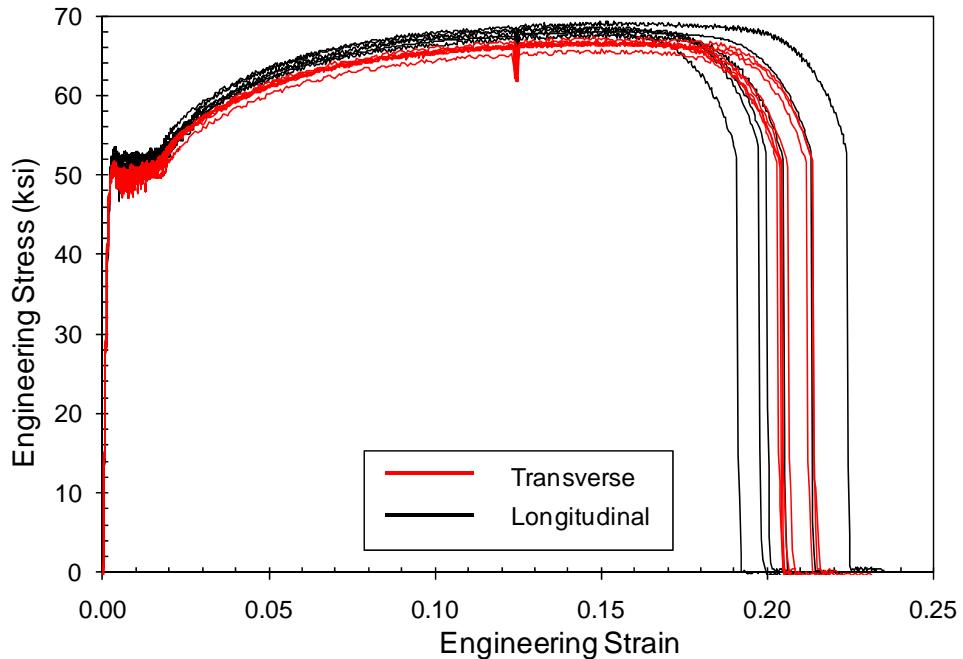


Figure D6. All GP307LS3 coupon engineering stress/engineering strain plots.

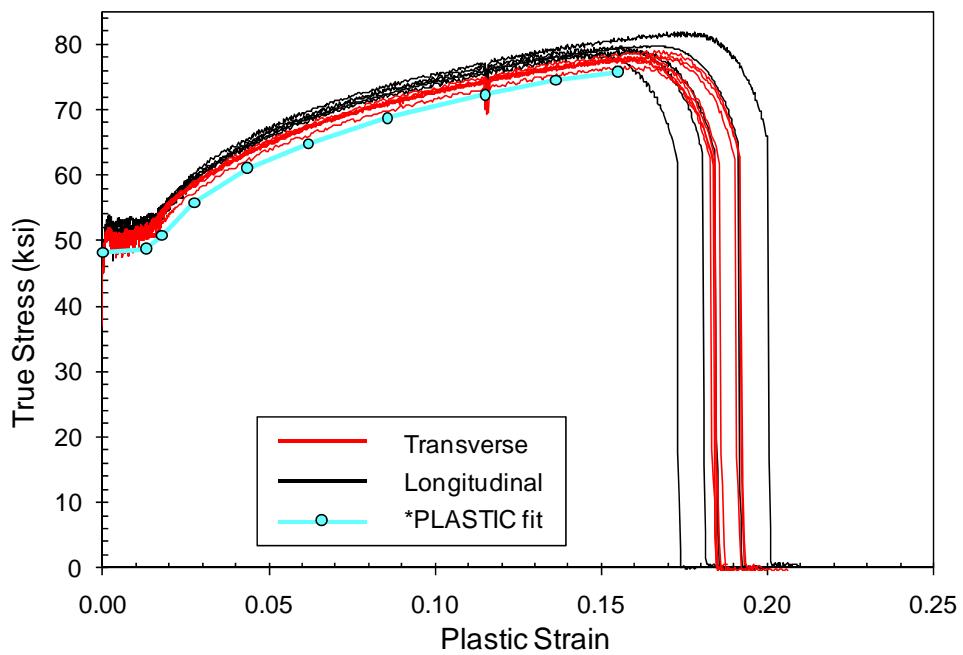


Figure D7. All GP307LS3 coupon true stress/true plastic strain plots.

Table D4. *Tensile Coupon Results from GP307SL3 plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|-----------------------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| E1L | 28138 | 50.1 | 47.0 | 66.7 | 24 | 60 |
| E1M | 28347 | 48.5 | 46.9 | 66.1 | 23 | 61 |
| E1R | 28439 | 50.8 | 48.3 | 67.3 | 25 | 60 |
| E2L | 28328 | 50.0 | 47.8 | 66.9 | 23 | 56 |
| E2M | 28937 | 49.8 | 48.4 | 67.3 | 26 | 61 |
| E2R | 28269 | 50.6 | 48.9 | 67.9 | 24 | 59 |
| <i>Average</i> | 28410 | 50.0 | 47.9 | 67.0 | 24 | 59 |
| <i>COV</i> | 0.010 | 0.016 | 0.017 | 0.009 | 0.050 | 0.031 |
| E3B1 | 26719 | 46.9 | 45.1 | 62.5 | 25 | 62 |
| E3B2 ^a | 27756 | 47.8 | 45.9 | 64.0 | 25 | 59 |
| E3T1 | 26832 | 47.0 | 45.2 | 62.7 | 26 | 60 |
| E3T2 | 27368 | 47.8 | 45.3 | 63.6 | 22 | 59 |
| E4B1 | 27211 | 47.4 | 45.6 | 62.7 | 26 | 58 |
| E4B2 ^a | 28191 | 48.2 | 45.8 | 63.9 | 23 | 60 |
| E4T1 | 27246 | 47.1 | 45.5 | 62.9 | 24 | 61 |
| E4T2 | 27452 | 47.6 | 45.8 | 64.0 | 27 | 63 |
| <i>Average^b</i> | 27138 | 47.3 | 45.4 | 63.1 | 25 | 61 |
| <i>COV^b</i> | 0.017 | 0.008 | 0.006 | 0.009 | 0.066 | 0.029 |
| <i>Average^b</i> | 29458 | 48.6 | 45.4 | 65.0 | 25 | 61 |
| <i>COV^b</i> | 0.011 | 0.008 | 0.006 | 0.009 | 0.066 | 0.029 |

^a –indicates specimens where fracture occurred outside the original gauge length marks or was located less than 25 % of the elongated gage length from either of the original gauge length marks.

^b – Specimens failing ASTM acceptance criteria were not included in statistical analysis

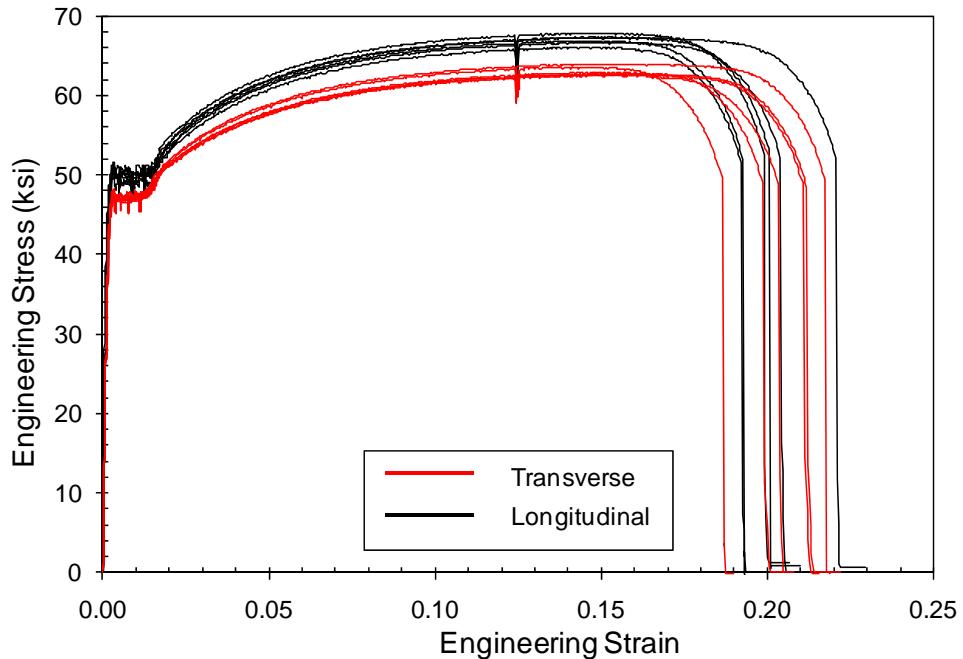


Figure D8. All GP307SL3 coupon engineering stress/engineering strain plots.

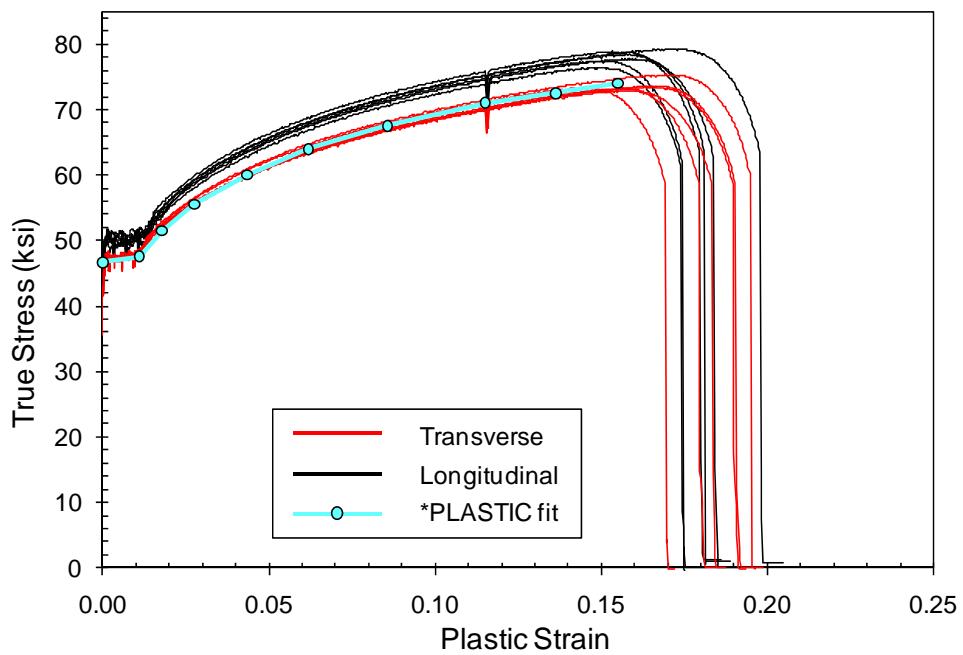


Figure D9. GP307SL3 coupon true stress/true plastic strain plots.

Table D5. *Tensile Coupon Results from GP307SL4 plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|----------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| F1L ^a | 28406 | 35.0 | 32.9 | 62.0 | 29 | 64 |
| F1M | 29590 | 34.8 | 32.5 | 61.8 | 28 | 63 |
| F1R ^c | 28890 | 34.7 | 32.5 | 62.2 | 30 | 68 |
| F2L | 28760 | 35.0 | 33.2 | 61.7 | 30 | 68 |
| F2M | 28527 | 34.9 | 32.8 | 61.7 | 30 | 66 |
| F2R | 28764 | 34.6 | 32.7 | 61.5 | 33 | 64 |
| F5L1 | 28858 | 34.8 | 32.9 | 62.1 | 29 | 60 |
| F5L2 | 29987 | 33.9 | 31.8 | 61.2 | 30 | 63 |
| F5L3 | 28918 | 34.0 | 32.0 | 60.5 | 31 | 61 |
| F5L4 | 29402 | 34.2 | 32.3 | 60.9 | 29 | 64 |
| Average ^b | 29532 | 35.6 | 33.7 | 62.1 | 29 | 61 |
| COV ^b | 0.027 | 0.027 | 0.034 | 0.007 | 0.091 | 0.105 |
| F3B1 | 29986 | 36.0 | 34.0 | 62.1 | 30 | 63 |
| F3B2 | 29589 | 34.7 | 32.6 | 61.3 | 29 | 64 |
| F3T1 | 29676 | 36.1 | 34.1 | 62.0 | 30 | 65 |
| F3T2 | 28892 | 34.6 | 32.6 | 61.3 | 30 | 60 |
| F4B1 | 29739 | 35.9 | 33.9 | 62.6 | 28 | 60 |
| F4B2 | 28951 | 34.4 | 32.3 | 61.3 | 31 | 60 |
| F4T1 ^c | 30350 | 35.3 | 31.8 | 61.9 | 28 | 59 |
| F4T2 | 30824 | 34.8 | 32.7 | 62.3 | 29 | 63 |
| F5T1 | 30508 | 36.6 | 34.9 | 62.6 | 25 | 55 |
| F5T2 | 30307 | 36.5 | 34.8 | 62.7 | 27 | 50 |
| F5T3 | 30136 | 36.4 | 34.6 | 62.4 | 30 | 57 |
| F5T4 | 30301 | 36.9 | 35.2 | 62.6 | 25 | 56 |
| Average | 29598 | 34.9 | 32.8 | 61.6 | 30 | 62 |
| COV | 0.021 | 0.022 | 0.026 | 0.010 | 0.029 | 0.030 |
| Average ^b | 29569 | 35.2 | 33.2 | 61.8 | 29 | 61 |
| COV ^b | 0.023 | 0.026 | 0.032 | 0.010 | 0.063 | 0.070 |

^a –indicates specimens where fracture occurred outside the original gauge length marks or was located less than 25 % of the elongated gage length from either of the original gauge length marks.

^b – Specimens failing ASTM acceptance criteria were not included in statistical analysis

^c – Equipment failures resulted in load being released, then reloaded

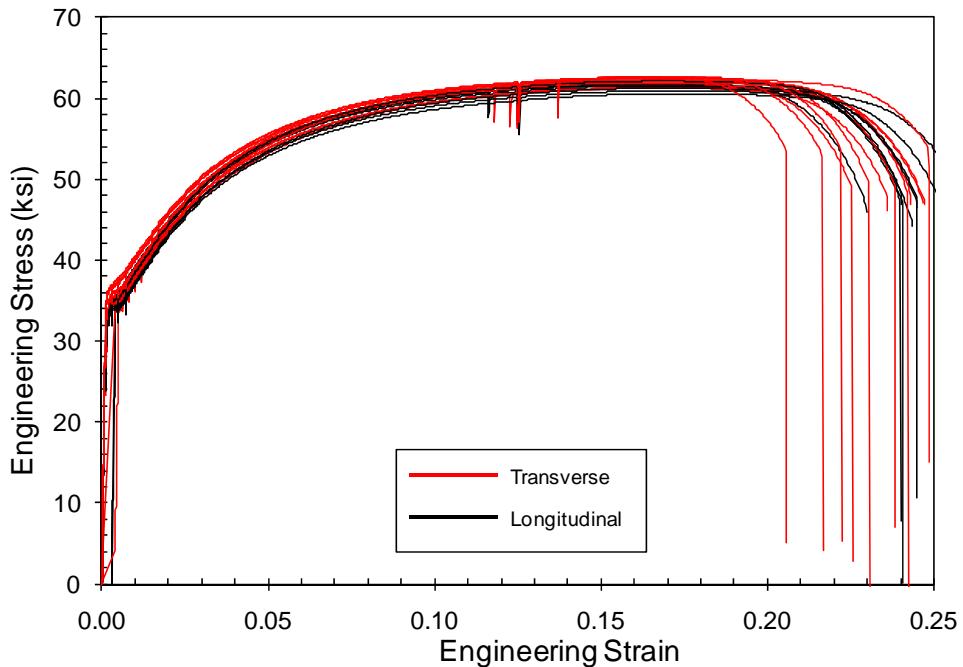


Figure D10. All GP307SL4 coupon engineering stress/engineering strain plots.

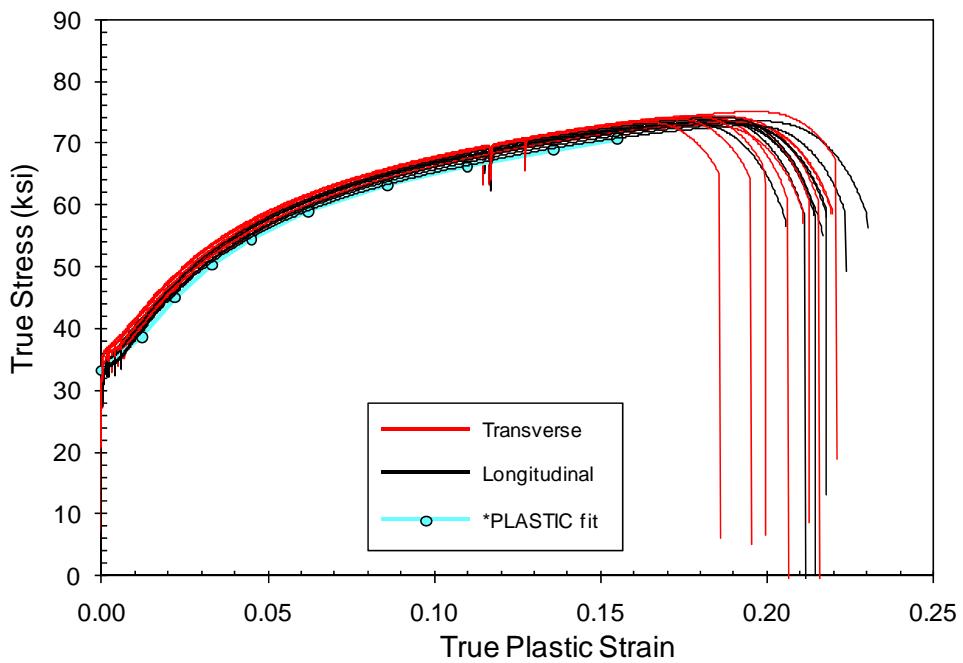


Figure D11. GP307SL4 coupon true stress/true plastic strain plots.

Table D6. *Tensile Coupon Results from GP307SS3-1 plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|-----------------------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| G1L | 29282 | 50.7 | 47.6 | 67.0 | 24 | 66 |
| G1M | 29238 | 50.8 | 48.1 | 66.9 | 23 | 66 |
| G1R ^a | 29406 | 51.0 | 48.4 | 51.1 | 25 | 66 |
| G2L | 29073 | 51.2 | 48.3 | 67.7 | 24 | 67 |
| G2M | 29091 | 50.8 | 49.0 | 68.3 | 26 | 66 |
| G2R | 29041 | 51.3 | 49.0 | 68.3 | 23 | 67 |
| <i>Average^b</i> | 29145 | 51.0 | 48.4 | 67.6 | 24 | 66 |
| <i>COV^b</i> | 0.004 | 0.005 | 0.012 | 0.010 | 0.050 | 0.007 |
| G3B1 | 29287 | 49.0 | 46.6 | 65.4 | 25 | 71 |
| G3B2 | 29124 | 49.1 | 46.5 | 65.0 | 26 | 67 |
| G3T1 ^a | 29098 | 48.4 | 46.3 | 65.3 | 20 | 47 |
| G3T2 | 29253 | 49.5 | 46.2 | 65.6 | 23 | 66 |
| G4B1 | 29418 | 49.2 | 46.4 | 65.3 | 26 | 69 |
| G4B2 | 29130 | 49.1 | 46.1 | 65.0 | 25 | 68 |
| G4T1 ^a | 29018 | 48.3 | 46.1 | 64.9 | 23 | 53 |
| G4T2 | 29159 | 48.7 | 45.7 | 64.7 | 27 | 68 |
| <i>Average^b</i> | 29228 | 49.1 | 46.2 | 65.2 | 25 | 68 |
| <i>COV^b</i> | 0.004 | 0.005 | 0.007 | 0.005 | 0.052 | 0.023 |
| <i>Average^b</i> | 29190 | 49.9 | 47.2 | 66.3 | 25 | 67 |
| <i>COV^b</i> | 0.004 | 0.020 | 0.026 | 0.021 | 0.057 | 0.023 |

^a –indicates specimens where fracture occurred outside the original gauge length marks or was located less than 25 % of the elongated gage length from either of the original gauge length marks.

^b – Specimens failing ASTM acceptance criteria were not included in statistical analysis

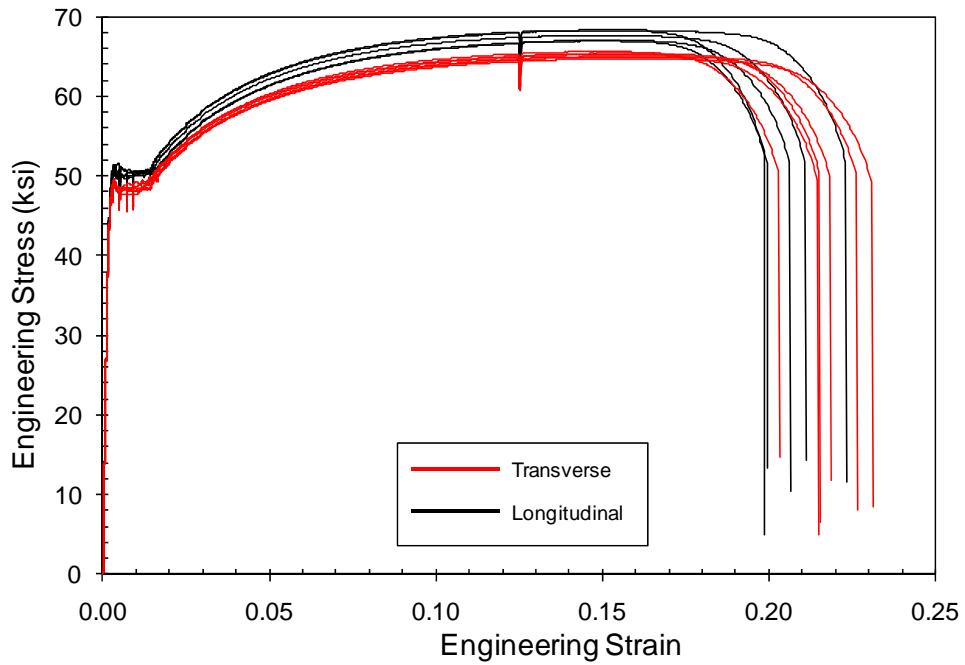


Figure D12. All GP307SS3-1 coupon engineering stress/engineering strain plots.

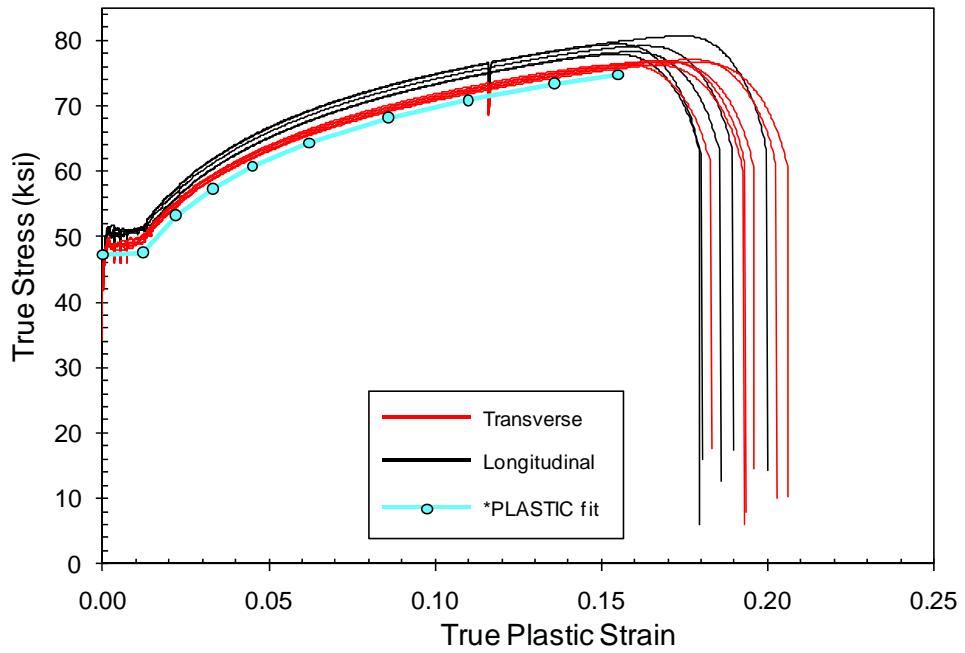


Figure D13. GP307SS3-1 coupon true stress/true plastic strain plots.

Table D7. *Tensile Coupon Results from GP307SS3-2 plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|-------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| H1L ^a | 29787 | 50.2 | 48.7 | 67.7 | 17 | 55 |
| H1M ^a | 29820 | 50.4 | 49.4 | 68.8 | 21 | 67 |
| H1R ^a | 29295 | 50.9 | 48.3 | 66.9 | 22 | 69 |
| H2L ^a | 30221 | 50.4 | 49.5 | 68.0 | 21 | 62 |
| H2M ^a | 29967 | 50.3 | 49.1 | 67.9 | 22 | 68 |
| H2R ^a | 30201 | 52.3 | 49.6 | 68.3 | 23 | 67 |
| <i>Average</i> | 29882 | 50.7 | 49.3 | 68.2 | 21 | 64 |
| <i>COV</i> | 0.011 | 0.017 | 0.007 | 0.006 | 0.115 | 0.085 |
| H3B1 ^a | 29274 | 49.0 | 47.5 | 65.9 | 21 | 62 |
| H3B2 ^a | 29639 | 48.8 | 47.2 | 65.9 | 21 | 65 |
| H3T1 ^a | 29013 | 47.8 | 46.2 | 64.0 | 20 | 43 |
| H3T2 ^a | 30247 | 49.6 | 47.8 | 66.2 | 21 | 65 |
| H4B1 ^a | 29641 | 48.9 | 46.9 | 66.0 | 22 | 67 |
| H4B2 ^a | 29383 | 48.0 | 46.4 | 65.2 | 21 | 67 |
| H4T1 ^a | 28812 | 48.8 | 46.4 | 64.9 | 26 | 65 |
| H4T2 ^a | 28811 | 48.6 | 46.4 | 64.8 | 22 | 68 |
| <i>Average</i> | 29352 | 48.7 | 46.9 | 65.4 | 22 | 63 |
| <i>COV</i> | 0.017 | 0.012 | 0.012 | 0.012 | 0.084 | 0.131 |
| Average | 29579 | 49.6 | 47.8 | 66.5 | 21 | 64 |
| COV | 0.017 | 0.024 | 0.026 | 0.021 | 0.075 | 0.061 |

a – Specimen was significant gouged while removing mill scale prior to testing, which likely initiated premature failure.

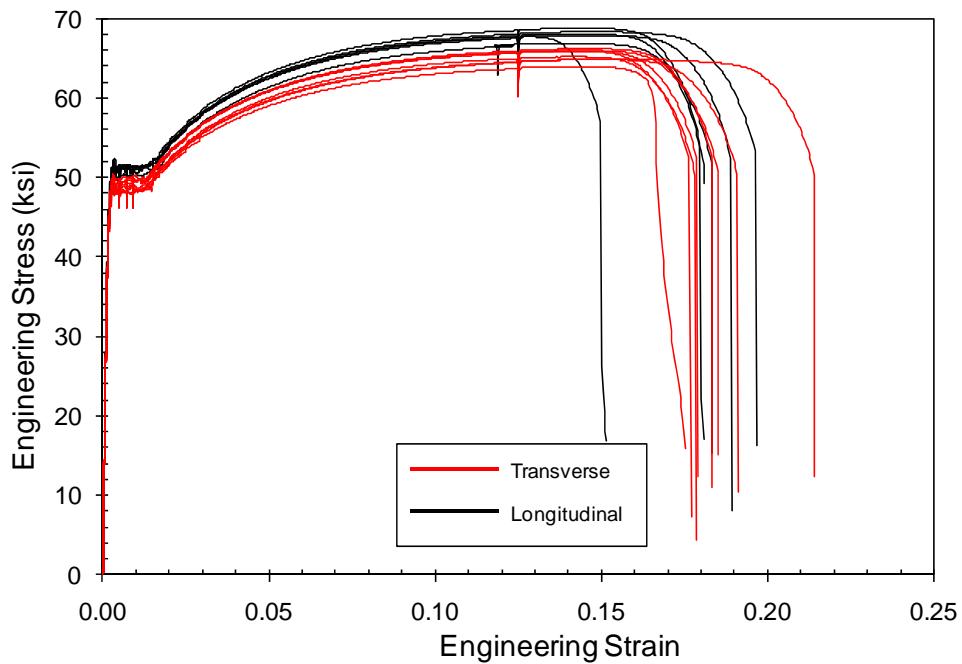


Figure D14. All GP307SS3-2 coupon engineering stress/engineering strain plots.

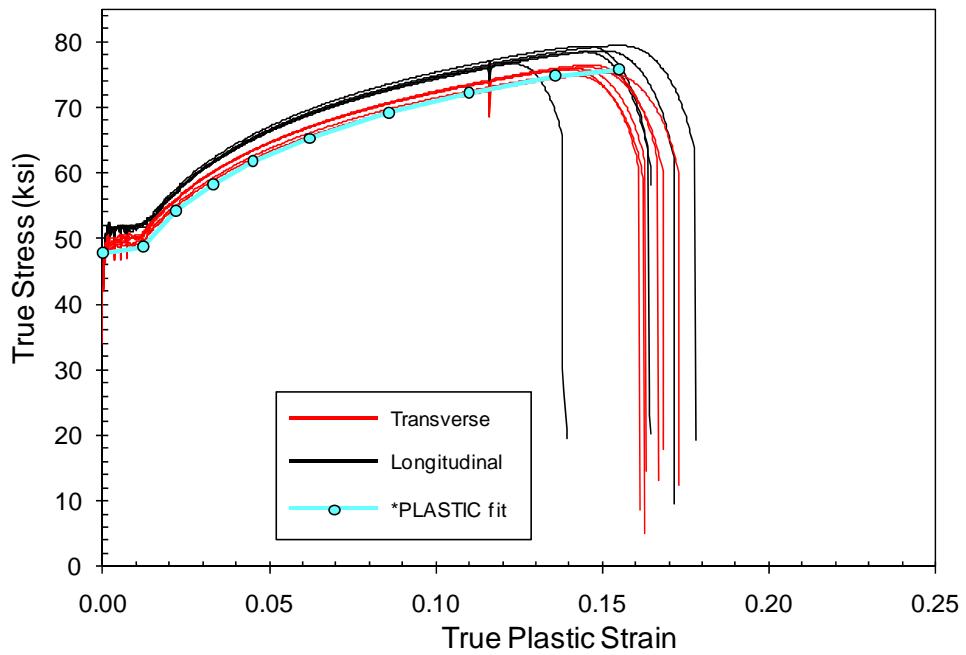


Figure D15. GP307SS3-2 coupon true stress/true plastic strain plots.

Table D8. *Tensile Coupon Results from GP307SS3-3 plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|-----------------------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| P1L | 28705 | 40.5 | 38.6 | 63.5 | 26 | 69 |
| P1M | 28637 | 40.7 | 38.8 | 63.1 | 27 | 69 |
| P1R | 28940 | 41.1 | 39.2 | 63.8 | 27 | 67 |
| P2L | 28734 | 40.6 | 38.3 | 63.0 | 27 | 68 |
| P2M | 28082 | 40.7 | 38.7 | 63.2 | 27 | 66 |
| P2R | 28700 | 40.3 | 39.1 | 64.2 | 29 | 64 |
| <i>Average</i> | 28633 | 40.7 | 38.8 | 63.5 | 27 | 67 |
| <i>COV</i> | 0.010 | 0.007 | 0.008 | 0.007 | 0.035 | 0.030 |
| P3B1 | 28742 | 38.4 | 37.5 | 61.0 | 25 | 61 |
| P3B2 | 28950 | 39.0 | 36.6 | 62.0 | 24 | 65 |
| P3T1 ^a | 29294 | 39.8 | 37.6 | 63.7 | 24 | 63 |
| P3T2 ^a | 28513 | 39.2 | 36.5 | 62.5 | 27 | 65 |
| P4B1 | 29957 | 40.0 | 37.8 | 64.6 | 26 | 63 |
| P4B2 | 29574 | 39.2 | 36.8 | 62.7 | 26 | 65 |
| P4T1 | 28806 | 39.1 | 36.7 | 62.1 | 30 | 60 |
| P4T2 | 28875 | 39.5 | 37.3 | 63.0 | 29 | 63 |
| <i>Average^b</i> | 29151 | 39.2 | 37.1 | 62.6 | 27 | 63 |
| <i>COV^b</i> | 0.017 | 0.014 | 0.013 | 0.019 | 0.078 | 0.034 |
| <i>Average^b</i> | 28892 | 39.9 | 37.9 | 63.0 | 27 | 65 |
| <i>COV^b</i> | 0.016 | 0.021 | 0.025 | 0.016 | 0.058 | 0.046 |

^a –indicates specimens where fracture occurred outside the original gauge length marks or was located less than 25 % of the elongated gage length from either of the original gauge length marks.

^b – Specimens failing ASTM acceptance criteria were not included in statistical analysis

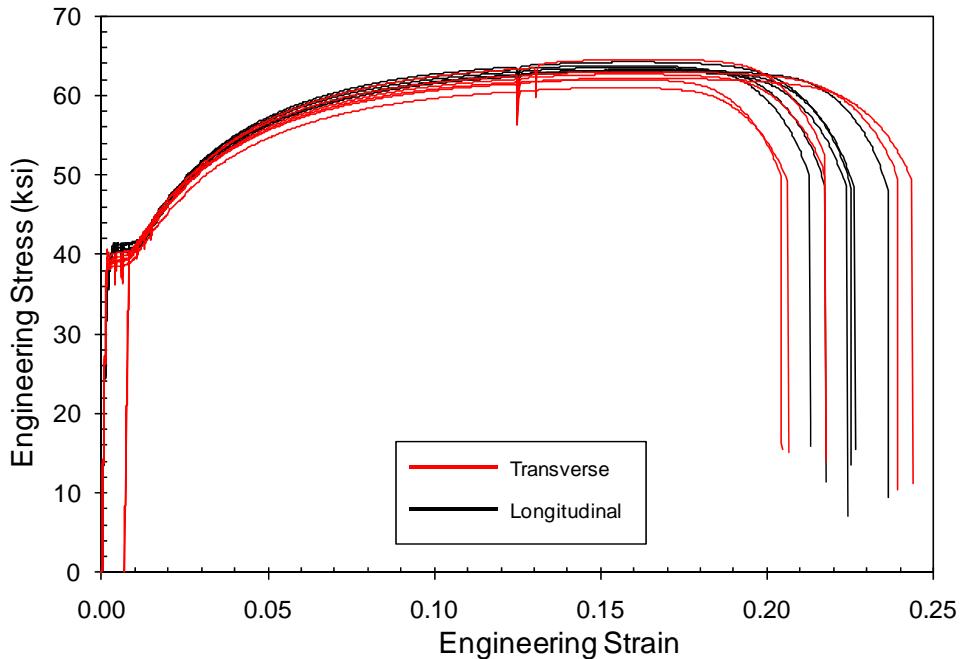


Figure D16. All GP307SS3-3 coupon engineering stress/engineering strain plots.

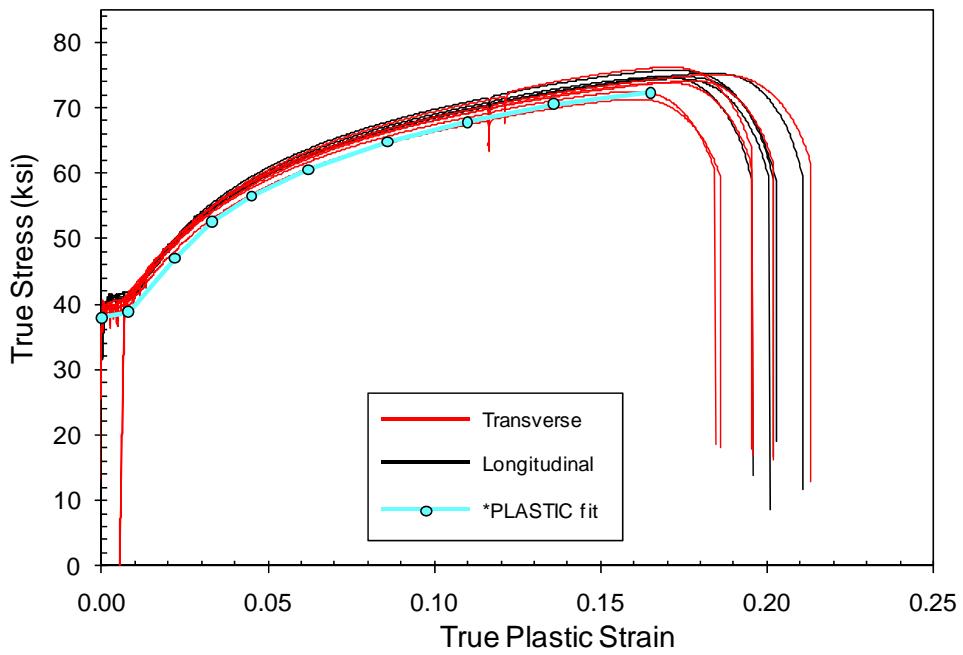


Figure D17. GP307SS3-3 coupon true stress/true plastic strain plots.

Table D9. *Tensile Coupon Results from GP307SS3-4 Gusset Plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|------------------------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| R1L | 28408 | 40.8 | 38.2 | 63.7 | 28 | 66 |
| R1M | 28338 | 39.6 | 37.1 | 62.0 | 26 | 65 |
| R1R | 28601 | 40.4 | 37.4 | 63.2 | 27 | 68 |
| R2L | 29201 | 40.9 | 39.3 | 63.4 | 28 | 64 |
| R2M | 28912 | 39.7 | 37.9 | 61.9 | 28 | 69 |
| R2R | 29319 | 41.3 | 39.5 | 64.0 | 30 | 63 |
| <i>Average</i> | 28796 | 40.5 | 38.4 | 63.0 | 28 | 65 |
| <i>COV</i> | 0.014 | 0.017 | 0.025 | 0.014 | 0.052 | 0.033 |
| R3B1 ^a | 29175 | 39.3 | 38.3 | 62.4 | 26 | 60 |
| R3B2 ^a | 28800 | 39.1 | 36.7 | 61.7 | 25 | 65 |
| R3T1 ^a | 29169 | 39.4 | 37.2 | 62.7 | 25 | 65 |
| R3T2 ^a | 30005 | 40.5 | 38.3 | 64.5 | 26 | 65 |
| R4B1 | 29555 | 40.5 | 38.3 | 64.3 | 30 | 65 |
| R4B2 ^a | 28885 | 39.3 | 37.3 | 62.6 | 25 | 62 |
| R4T1 | 29949 | 40.4 | 38.1 | 63.9 | 24 | 64 |
| R4T2 | 28575 | 38.4 | 35.9 | 60.8 | 24 | 61 |
| <i>Average</i> ^b | 29360 | 39.8 | 37.4 | 63.0 | 26 | 63 |
| <i>COV</i> ^b | 0.024 | 0.030 | 0.036 | 0.031 | 0.129 | 0.034 |
| <i>Average</i> ^b | 28984 | 40.2 | 38.0 | 63.0 | 27 | 65 |
| <i>COV</i> ^b | 0.019 | 0.022 | 0.029 | 0.019 | 0.082 | 0.038 |

^a –indicates specimens where fracture occurred outside the original gauge length marks or was located less than 25 % of the elongated gage length from either of the original gauge length marks.

^b – Specimens failing ASTM acceptance criteria were not included in statistical analysis

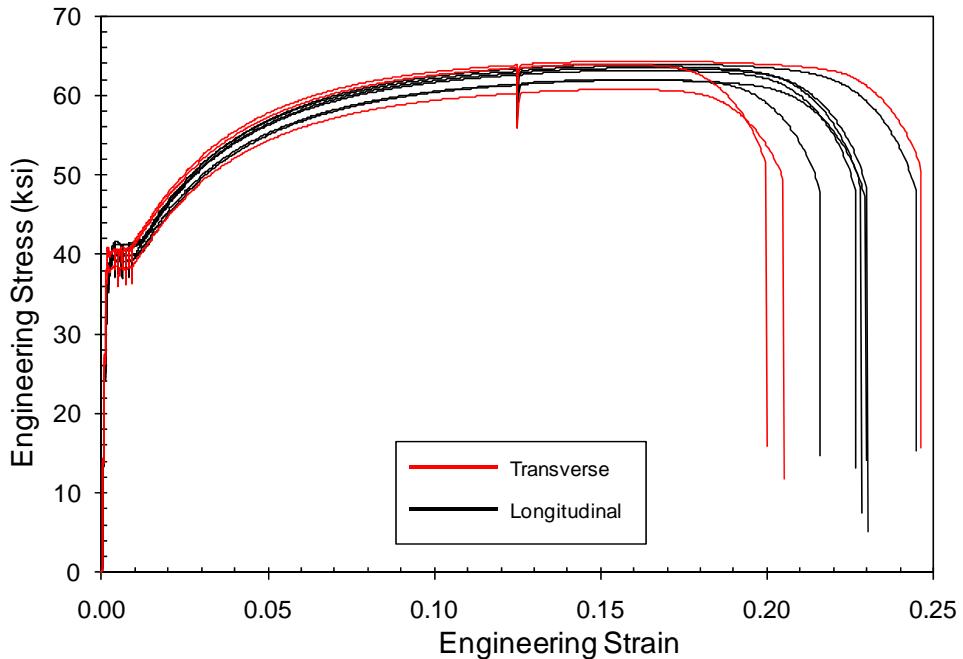


Figure D18. All GP307SS3-4 gusset coupon engineering stress/engineering strain plots.

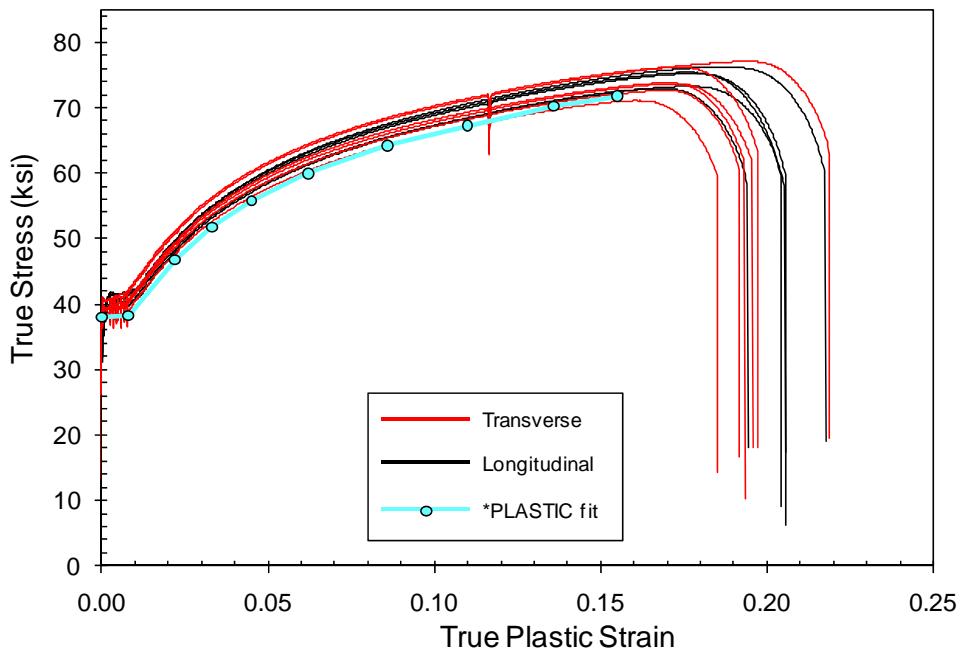


Figure D19. GP307SS3-4 gusset coupon true stress/true plastic strain plots.

Table D10. *Tensile Coupon Results from GP307SS3-4 Shingle Plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|------------------------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| S5L1 | 30361 | 49.2 | 46.6 | 67.0 | 27 | 66 |
| S5L2 | 30390 | 48.6 | 46.2 | 67.1 | 27 | 66 |
| S5L3 | 29919 | 49.3 | 46.9 | 67.4 | 27 | 64 |
| S5L4 | 30541 | 49.0 | 46.5 | 66.8 | 27 | 66 |
| <i>Average</i> | 30303 | 49.0 | 46.5 | 67.1 | 27 | 66 |
| <i>COV</i> | 0.009 | 0.006 | 0.006 | 0.004 | 0.005 | 0.015 |
| S5T1 | 30172 | 48.0 | 45.4 | 65.7 | 28 | 70 |
| S5T2 | 29801 | 48.6 | 46.1 | 66.9 | 27 | 69 |
| S5T3 | 30850 | 48.7 | 45.9 | 67.2 | 27 | 71 |
| S5T4 | 30313 | 48.9 | 46.5 | 66.6 | 27 | 70 |
| <i>Average</i> ^b | 30284 | 48.6 | 46.0 | 66.6 | 27 | 70 |
| <i>COV</i> ^b | 0.014 | 0.008 | 0.010 | 0.010 | 0.019 | 0.010 |
| <i>Average</i> ^b | 30293 | 48.8 | 46.3 | 66.8 | 27 | 68 |
| <i>COV</i> ^b | 0.011 | 0.008 | 0.010 | 0.008 | 0.015 | 0.038 |

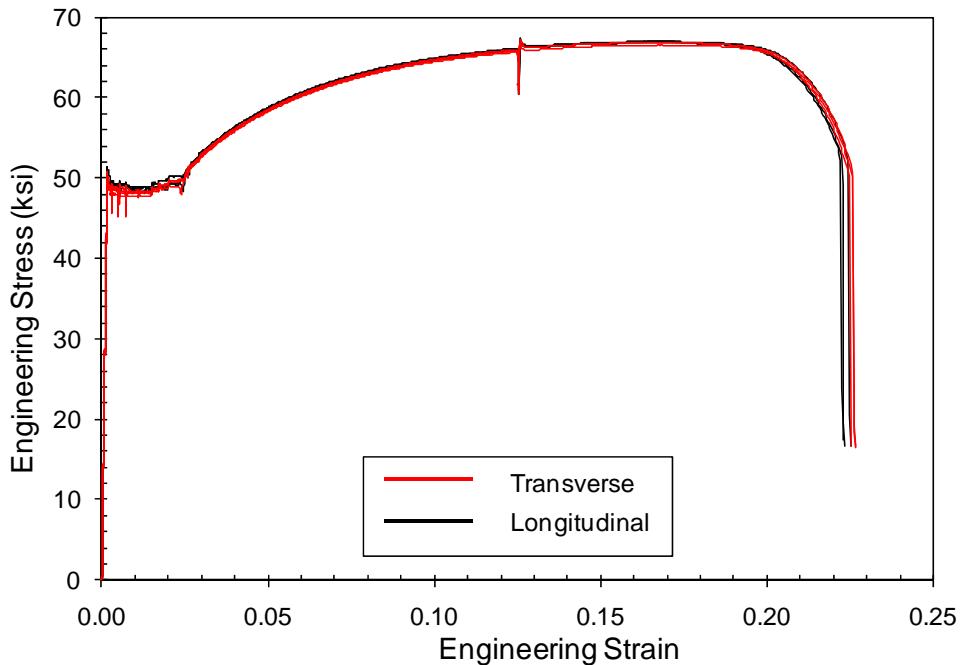


Figure D20. All shingle plate coupon engineering stress/engineering strain plots.

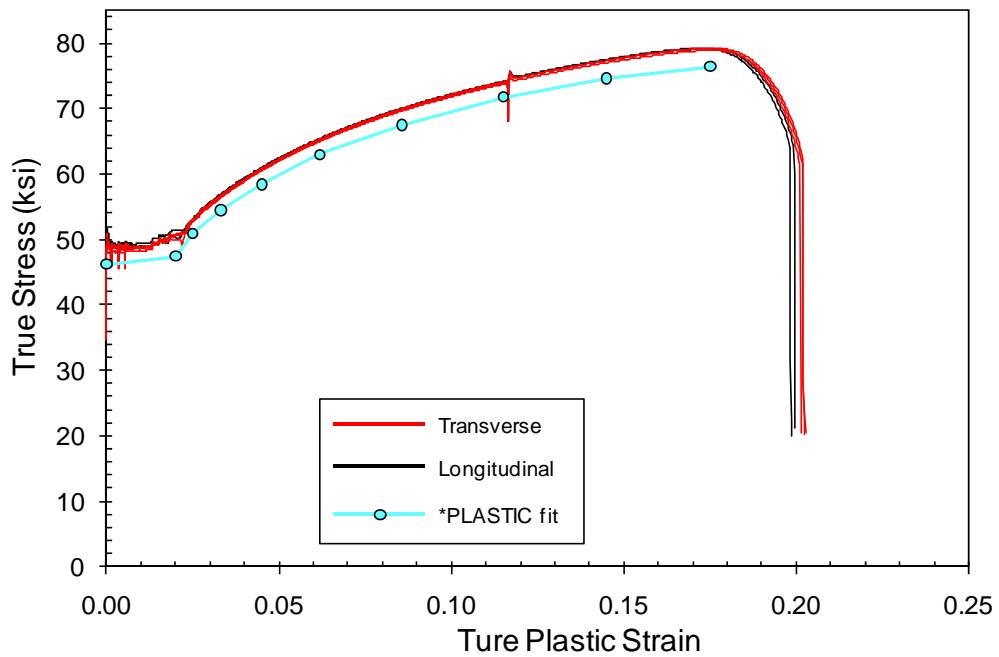


Figure D21. Shingle plate coupon true stress/true plastic strain plots.

Table D11. *Tensile Coupon Results from GP490LS3 plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|-----------------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| I1L ^a | 27950 | 50.2 | 47.3 | 67.1 | 25 | 60 |
| I1M | 28609 | 49.5 | 47.5 | 66.7 | 22 | 63 |
| I1R | 28358 | 50.3 | 48.6 | 67.7 | 21 | 58 |
| I2L | 28029 | 49.3 | 47.1 | 66.0 | 24 | 60 |
| I2M ^a | 27902 | 49.6 | 47.0 | 66.1 | 25 | 58 |
| I2R | 28057 | 49.6 | 47.0 | 66.2 | 24 | 61 |
| <i>Average</i> ^b | 28263 | 49.7 | 47.5 | 66.6 | 23 | 61 |
| <i>COV</i> ^b | 0.011 | 0.007 | 0.016 | 0.011 | 0.078 | 0.039 |
| I3B1 | 26468 | 46.3 | 44.7 | 61.6 | 25 | 61 |
| I3B2 | 27518 | 46.5 | 44.5 | 62.4 | 24 | 61 |
| I3T1 | 27005 | 46.2 | 44.5 | 62.1 | 20 | 34 |
| I3T2 | 27580 | 46.5 | 44.6 | 62.6 | 24 | 58 |
| I4B1 | 26175 | 45.9 | 44.2 | 61.4 | 24 | 56 |
| I4B2 | 27456 | 46.9 | 45.2 | 63.2 | 22 | 62 |
| I4T1 | 26440 | 46.7 | 45.0 | 62.2 | 22 | 55 |
| I4T2 | 27246 | 46.8 | 44.5 | 62.4 | 25 | 58 |
| <i>Average</i> | 26986 | 46.5 | 44.7 | 62.2 | 23 | 56 |
| <i>COV</i> | 0.021 | 0.007 | 0.007 | 0.009 | 0.073 | 0.163 |
| <i>Average</i> ^b | 27412 | 47.5 | 45.6 | 63.7 | 23 | 57 |
| <i>COV</i> ^b | 0.029 | 0.034 | 0.033 | 0.035 | 0.068 | 0.135 |

^a –indicates specimens where fracture occurred outside the original gauge length marks or was located less than 25 % of the elongated gage length from either of the original gauge length marks.
^b – Specimens failing ASTM acceptance criteria were not included in statistical analysis

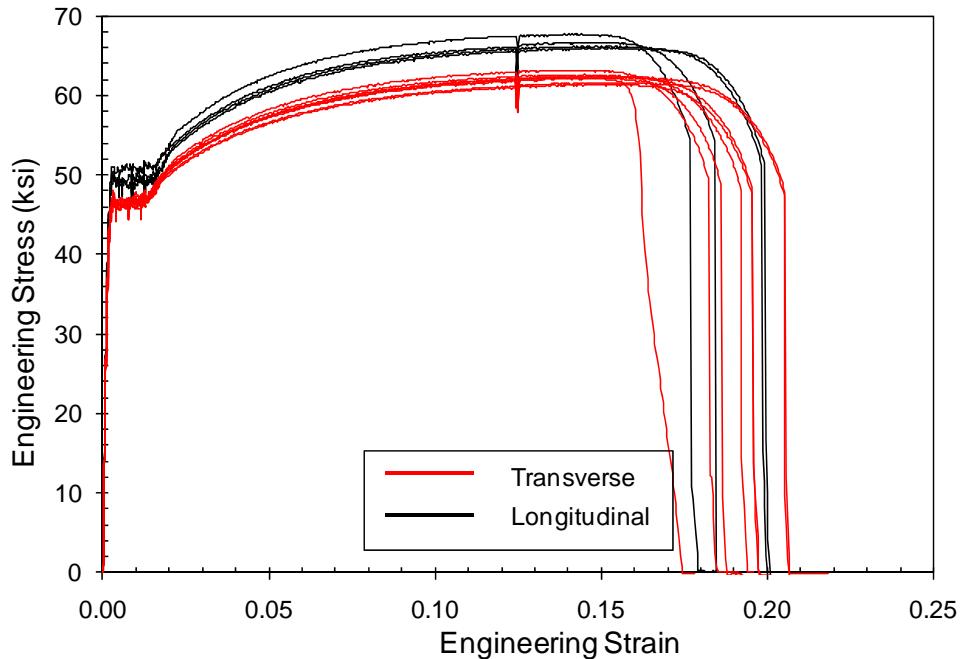


Figure D22. All GP490LS3 coupon engineering stress/engineering strain plots.

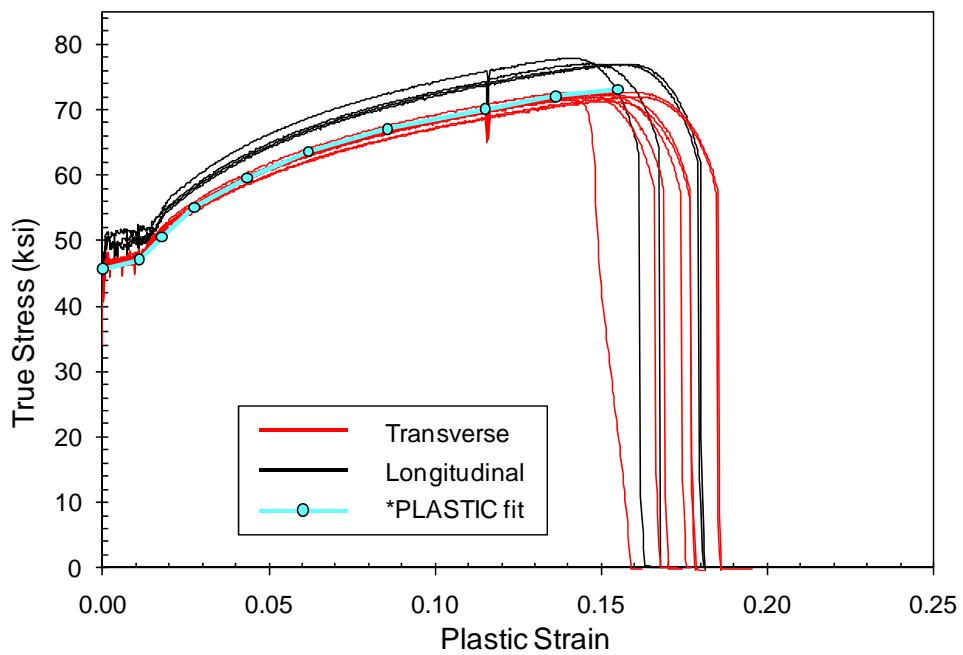


Figure D23. GP490LS3 coupon true stress/true plastic strain plots.

Table D12. *Tensile Coupon Results from GP490SS3 Plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|-----------------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| J1L | 28538 | 50.1 | 47.6 | 67.4 | 25 | 66 |
| J1M | 28382 | 50.9 | 47.8 | 68.0 | 25 | 65 |
| J1R | 28404 | 50.2 | 47.9 | 67.2 | 27 | 64 |
| J2L | 28413 | 49.6 | 47.3 | 66.9 | 24 | 68 |
| J2M ^a | 28619 | 49.3 | 48.1 | 67.4 | 24 | 59 |
| J2R | 28165 | 51.1 | 48.3 | 67.5 | 25 | 63 |
| <i>Average</i> ^b | 28380 | 50.4 | 47.8 | 67.4 | 25 | 65 |
| <i>COV</i> ^b | 0.005 | 0.012 | 0.008 | 0.006 | 0.042 | 0.029 |
| J3B1 | 28091 | 48.0 | 45.9 | 64.4 | 26 | 66 |
| J3B2 | 28278 | 47.5 | 46.0 | 64.2 | 25 | 65 |
| J3T1 | 27606 | 45.6 | 43.7 | 61.6 | 24 | 65 |
| J3T2 | 28267 | 47.5 | 45.3 | 64.0 | 24 | 65 |
| J4B1 | 28041 | 47.0 | 45.3 | 63.2 | 24 | 69 |
| J4B2 | 27968 | 47.8 | 45.3 | 63.7 | 25 | 66 |
| J4T1 | 28347 | 48.5 | 46.8 | 65.2 | 22 | 65 |
| J4T2 | 28391 | 48.5 | 46.4 | 64.9 | 25 | 66 |
| <i>Average</i> | 28123 | 47.6 | 45.6 | 63.9 | 24 | 66 |
| <i>COV</i> | 0.009 | 0.020 | 0.021 | 0.018 | 0.058 | 0.019 |
| <i>Average</i> ^b | 28222 | 48.6 | 46.4 | 65.2 | 25 | 66 |
| <i>COV</i> ^b | 0.009 | 0.034 | 0.029 | 0.030 | 0.053 | 0.023 |

^a –indicates specimens where fracture occurred outside the original gauge length marks or was located less than 25 % of the elongated gage length from either of the original gauge length marks.
^b – Specimens failing ASTM acceptance criteria were not included in statistical analysis

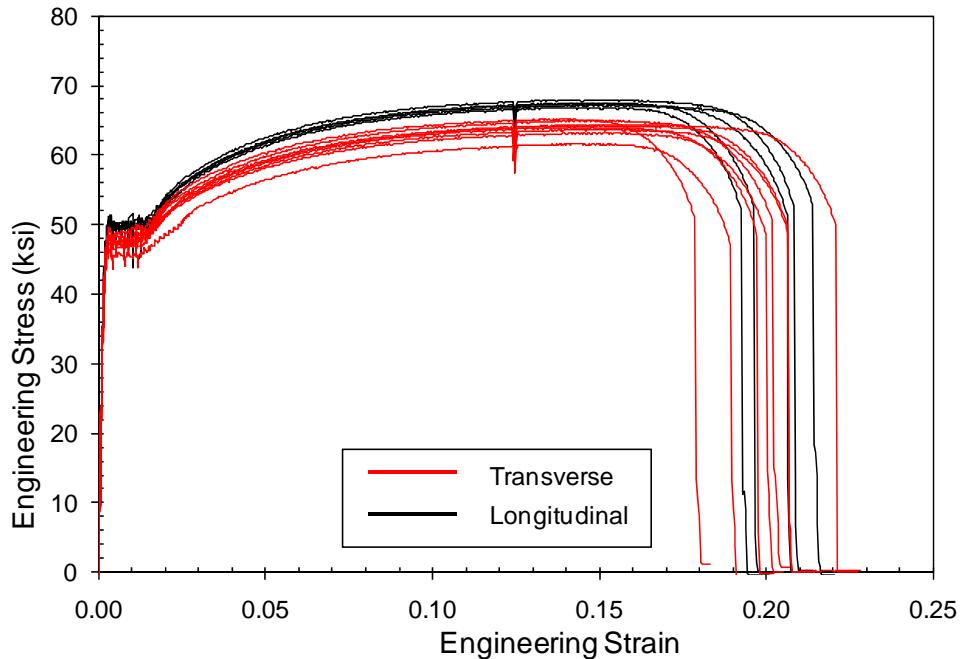


Figure D24. All GP490SS3 coupon engineering stress/engineering strain plots.

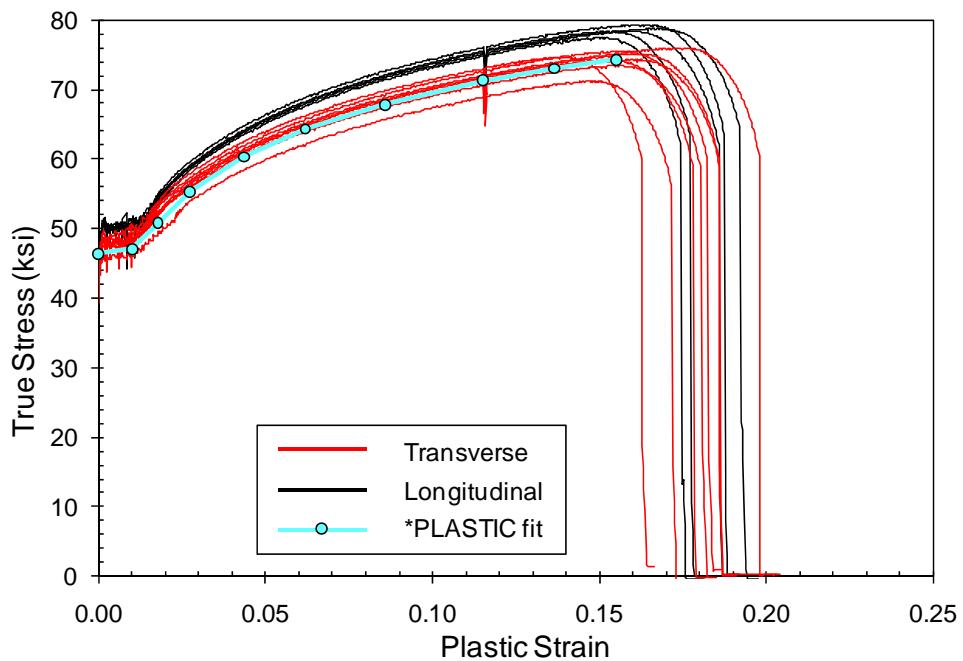


Figure D25. All GP490SS3 coupon true stress/true plastic strain plots (rejected specimens excluded).

Table D13. *Tensile Coupon Results from GP490SS3-1 plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|-------------|--------------------------------------|--------------------------------|---------------------------|------------------------|--------------------|--------------------|
| K1L | 29917 | 48.2 | 45.5 | 66.4 | 27 | 70 |
| K1M1 | 28923 | 46.5 | 44.9 | 66.7 | 36 ^a | 76 |
| K1M2 | 29522 | 48.0 | 44.6 | 67.3 | 36 ^a | 76 |
| K1R | 29787 | 47.6 | 45.0 | 66.2 | 28 | 69 |
| K2L | 29776 | 48.5 | 46.1 | 66.8 | 29 | 72 |
| K2M1 | 28915 | 47.2 | 45.3 | 67.4 | 36 ^a | 76 |
| K2M2 | 28839 | 46.9 | 45.2 | 67.2 | 37 ^a | 76 |
| K2R | 29746 | 48.7 | 45.8 | 66.9 | 27 | 73 |
| N1L | 30010 | 48.7 | 46.1 | 66.6 | 27 | 72 |
| N1M1 | 29112 | 48.7 | 46.6 | 67.1 | 37 ^a | 77 |
| N1M2 | 28962 | 46.4 | 44.8 | 66.9 | 36 ^a | 74 |
| N1R | 29901 | 48.7 | 46.1 | 66.5 | 28 | 70 |
| K5L1 | 30088 | 49.5 | 46.8 | 68.1 | 28 | 66 |
| K5L2 | 30256 | 49.9 | 47.3 | 67.9 | 26 | 68 |
| K5L3 | 30457 | 49.6 | 46.9 | 67.7 | 27 | 64 |
| K5L4 | 30565 | 49.5 | 47.1 | 67.6 | 26 | 67 |
| Average | 29674 | 48.3 | 45.9 | 67.1 | 28 ^a | 72 |
| COV | 0.019 | 0.023 | 0.019 | 0.008 | 0.029 ^a | 0.057 |
| K3B1 | 29981 | 48.2 | 45.6 | 66.3 | 27 | 69 |
| K3B2 | 30025 | 47.8 | 45.3 | 66.4 | 28 | 68 |
| K3T1 | 29861 | 46.9 | 44.4 | 65.7 | 27 | 70 |
| K3T2 | 29902 | 48.1 | 45.7 | 66.2 | 27 | 70 |
| K4B1 | 29811 | 48.4 | 46.1 | 66.5 | 30 | 69 |
| K4B2 | 29859 | 48.2 | 45.7 | 66.6 | 28 | 68 |
| K4T1 | 29838 | 48.2 | 45.8 | 66.4 | 27 | 71 |
| K4T2 | 29618 | 47.8 | 45.2 | 66.2 | 26 | 69 |
| N3B1 | 30146 | 48.7 | 46.2 | 66.3 | 27 | 64 |
| N3B2 | 30036 | 48.5 | 46.1 | 66.4 | 27 | 67 |
| N3T1 | 30000 | 48.6 | 46.1 | 66.7 | 27 | 62 |
| N3T2 | 30021 | 48.3 | 45.7 | 66.4 | 27 | 63 |
| K5T1 | 30244 | 48.7 | 46.3 | 67.7 | 28 | 61 |
| K5T2 | 30251 | 49.0 | 46.6 | 67.6 | 27 | 67 |
| K5T3 | 30146 | 48.5 | 46.1 | 67.0 | 27 | 69 |
| K5T4 | 30100 | 48.7 | 46.3 | 67.2 | 27 | 70 |
| Average | 29990 | 48.3 | 45.8 | 66.6 | 27 | 67 |
| COV | 0.006 | 0.010 | 0.012 | 0.008 | 0.029 | 0.044 |
| Average | 29832 | 48.3 | 45.9 | 66.8 | 27 ^a | 69 |
| COV | 0.015 | 0.017 | 0.016 | 0.009 | 0.029 ^a | 0.060 |

^a –ASTM “Sheet-Type” specimens were not included in statistical analysis

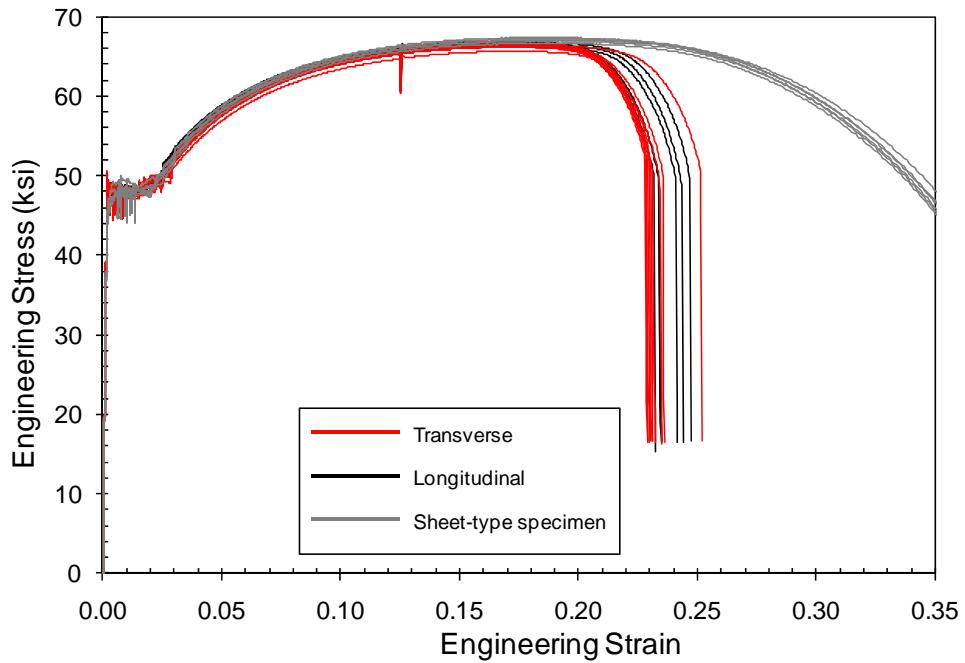


Figure D26. All GP490SS3-1 coupon engineering stress/engineering strain plots.

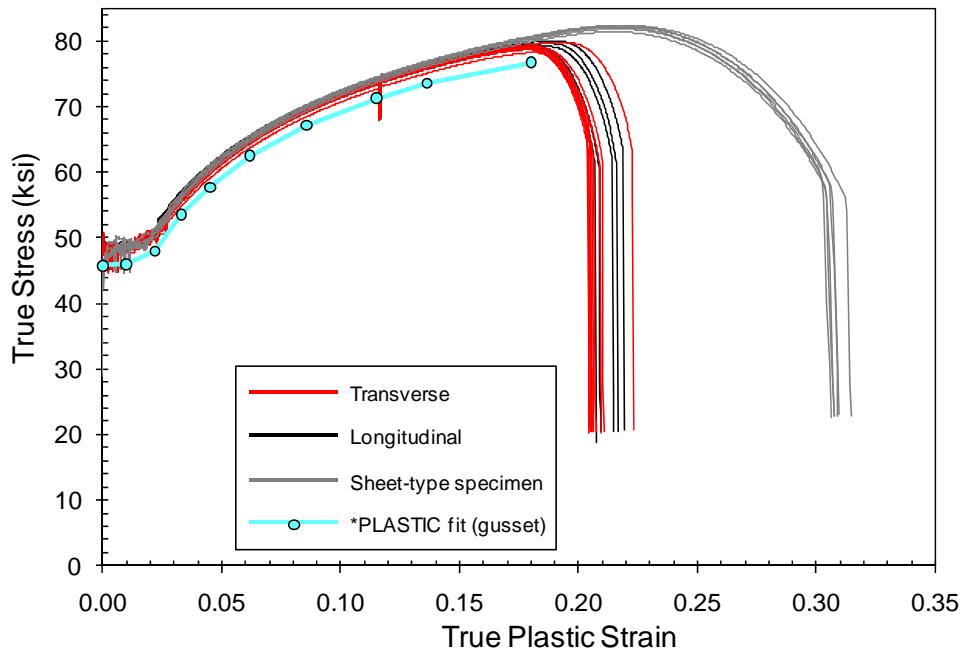


Figure D27. GP490SS3-1 coupon true stress/true plastic strain plots.

Table D14. *Tensile Coupon Results from GP490LS3-1 Plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|----------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|--------------------|--------------------|
| L1L | 29593 | 48.4 | 46.1 | 66.4 | 28 | 71 |
| L1M1 | 28962 | 46.1 | 45.1 | 67.4 | 36 ^a | 75 |
| L1M2 | 28729 | 46.3 | 45.0 | 67.3 | 36 ^a | 76 |
| L1R | 29378 | 48.3 | 45.7 | 66.3 | 27 | 68 |
| L2L | 29762 | 49.0 | 46.5 | 66.8 | 28 | 72 |
| L2M1 | 29281 | 47.9 | 45.9 | 68.1 | 37 ^a | 76 |
| L2M2 | 29046 | 49.7 | 46.1 | 67.8 | 34 ^a | 66 |
| L2R | 30144 | 48.7 | 46.4 | 66.7 | 27 | 72 |
| L5L1 | 30613 | 50.0 | 47.4 | 68.4 | 29 | 68 |
| L5L2 | 30687 | 49.7 | 47.2 | 68.0 | 30 | 69 |
| L5L3 ^b | 30911 | 49.9 | 47.4 | 68.1 | 29 | 65 |
| L5L4 | 30868 | 49.8 | 47.1 | 67.8 | 30 | 67 |
| Average | 29733 | 48.5 | 46.2 | 67.4 | 28 ^a | 71 |
| COV | 0.025 | 0.028 | 0.018 | 0.011 | 0.042 ^a | 0.053 |
| L3B1 | 29466 | 48.4 | 45.6 | 66.7 | 27 | 65 |
| L3B2 | 29732 | 48.3 | 45.4 | 66.6 | 28 | 66 |
| L3T1 | 29663 | 48.1 | 45.5 | 66.7 | 28 | 69 |
| L3T2 | 29273 | 49.0 | 46.4 | 66.8 | 28 | 68 |
| L4B1 | 29935 | 48.6 | 45.9 | 66.8 | 27 | 69 |
| L4B2 | 29791 | 48.7 | 46.2 | 67.1 | 28 | 69 |
| L4T1 | 29807 | 48.3 | 45.8 | 67.0 | 27 | 69 |
| L4T2 | 29637 | 48.3 | 45.5 | 66.8 | 27 | 71 |
| L5T1 | 30339 | 49.5 | 47.1 | 68.3 | 29 | 67 |
| L5T2 | 30503 | 50.0 | 47.2 | 68.3 | 28 | 66 |
| L5T3 | 30422 | 49.8 | 47.2 | 68.0 | 28 | 64 |
| L5T4 | 30338 | 49.4 | 46.9 | 67.7 | 27 | 70 |
| Average | 29909 | 48.9 | 46.2 | 67.2 | 28 | 68 |
| COV | 0.013 | 0.013 | 0.015 | 0.010 | 0.025 | 0.033 |
| Average ^c | 29825 | 48.7 | 46.2 | 67.3 | 28 ^a | 69 |
| COV ^c | 0.020 | 0.021 | 0.016 | 0.010 | 0.033 ^a | 0.049 |

^a -These smaller ASTM E8 sheet-type specimens demonstrated different ductility and strength than the larger plate-type coupons

^b - Indicates specimens where fracture occurred outside the original gauge length marks or was located less than 25 % of the elongated gage length from either of the original gauge length marks.

^c -Rejectable specimens were not included in statistical analysis

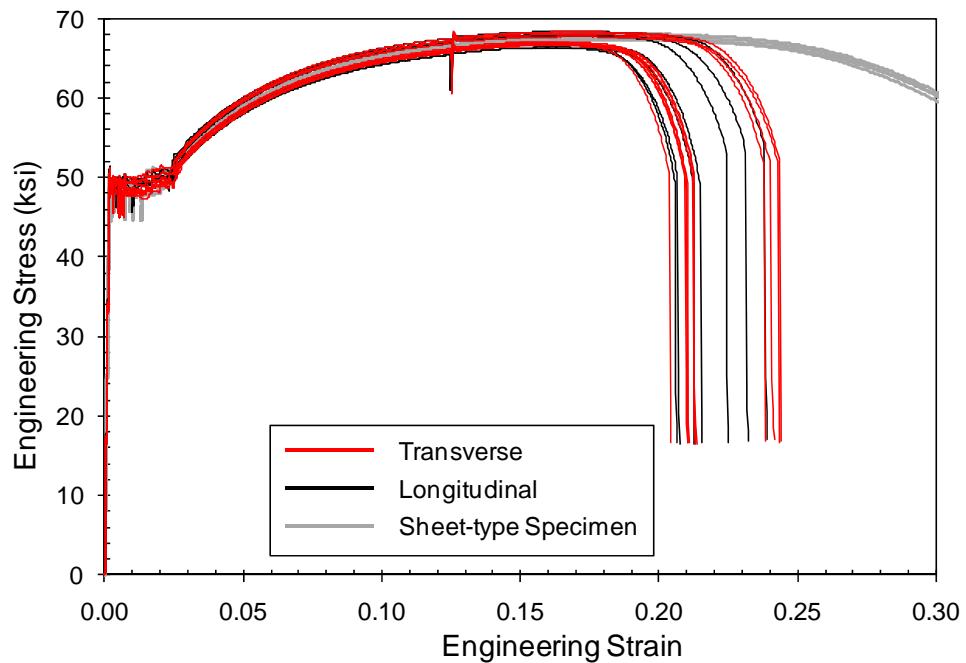


Figure D28. All GP490LS3-1 coupon engineering stress/engineering strain plots.

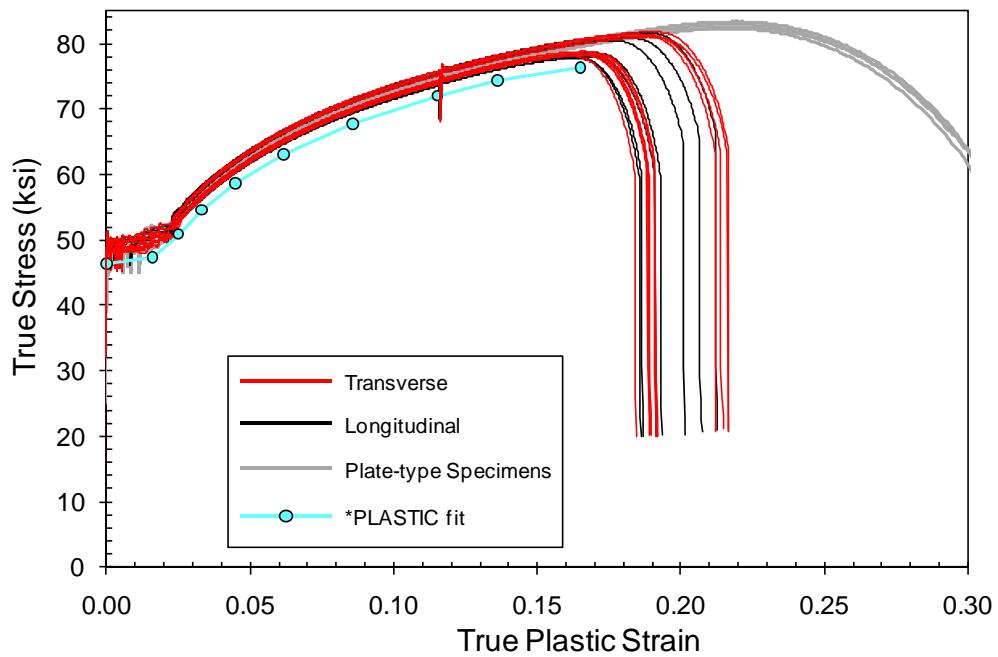


Figure D29. GP490LS3-1 coupon true stress/true plastic strain plots.

Table D15. *Tensile Coupon Results from GP490LS3-2 Plate*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|-------------------|--------------------------------------|--------------------------------|---------------------------|------------------------|--------------------------|--------------------|
| M1L | 29728 | 48.5 | 45.9 | 66.3 | 28 | 68 |
| M1M1 | 29337 | 46.2 | 45.3 | 67.2 | 37 ^a | 75 |
| M1M2 | 29140 | 47.5 | 45.3 | 67.6 | 36 ^a | 75 |
| M1R | 29724 | 47.9 | 45.5 | 66.3 | 27 | 69 |
| M2L | 29557 | 47.7 | 45.3 | 66.1 | 28 | 70 |
| M2M1 | 28868 | 47.1 | 44.6 | 68.2 | 36 ^a | 75 |
| M2M2 | 29045 | 46.2 | 44.9 | 67.4 | 36 ^a | 76 |
| M2R | 29735 | 48.1 | 45.1 | 50.1 | 27 | 69 |
| M5L1 | 30709 | 49.5 | 47.0 | 68.2 | 27 | 67 |
| M5L2 | 30741 | 49.1 | 46.9 | 68.0 | 27 | 65 |
| M5L3 | 30667 | 49.7 | 47.2 | 67.9 | 25 | 62 |
| M5L4 | 30641 | 49.0 | 46.5 | 67.4 | 26 | 68 |
| Average | 29824 | 48.0 | 45.8 | 65.9 | 27 ^a | 70 |
| COV | 0.023 | 0.024 | 0.020 | 0.076 | 0.042 ^a | 0.064 |
| M3B1 | 29716 | 48.2 | 45.7 | 66.2 | 27 | 70 |
| M3B2 | 29562 | 48.0 | 45.5 | 66.1 | 28 | 71 |
| M3T1 | 29658 | 48.2 | 45.5 | 66.0 | 27 | 69 |
| M3T2 | 29961 | 47.8 | 45.4 | 66.1 | 28 | 71 |
| M4B1 ^b | | | | | | |
| M4B2 | 29984 | 48.1 | 45.7 | 66.8 | 28 | 66 |
| M4T1 | 29858 | 47.9 | 45.5 | 66.3 | 27 | 70 |
| M4T2 | 29813 | 47.5 | 45.1 | 66.3 | 27 | 69 |
| M5T1 | 30206 | 48.6 | 46.2 | 67.1 | 28 | 68 |
| M5T2 | 30212 | 48.4 | 46.0 | 66.9 | 28 | 70 |
| M5T3 | 30067 | 50.1 | | 66.4 | 27 | 64 |
| M5T4 | 30068 | 48.6 | 46.2 | 67.0 | 27 | 70 |
| Average | 29919 | 48.3 | 45.7 | 66.5 | 27 | 69 |
| COV | 0.007 | 0.014 | 0.008 | 0.006 | 0.018 | 0.030 |
| Average | 29870 | 48.2 | 45.7 | 66.2 | 29^a | 69 |
| COV | 0.017 | 0.020 | 0.015 | 0.054 | 0.128^a | 0.051 |
| MA1 ^c | 29556 | 49.9 | 46.9 | 73.9 | 24 | 54 |
| MA2 ^c | 29895 | 51.7 | 47.2 | 74.6 | 23 | 55 |
| Average | 29725 | 50.8 | 47.1 | 74.3 | 24 | 55 |

^a – Sheet-type specimens were not included in statistical analysis

^b – This specimen was accidentally destroyed

^c – Longitudinal coupons from stiffening angles

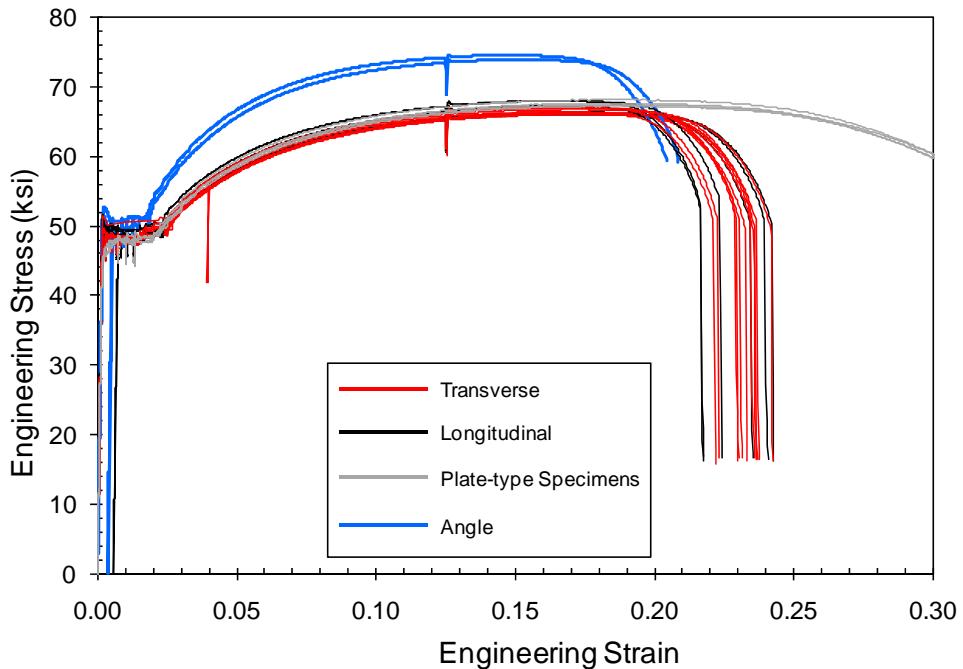


Figure D30. All GP490LS3-2 coupon engineering stress/engineering strain plots.

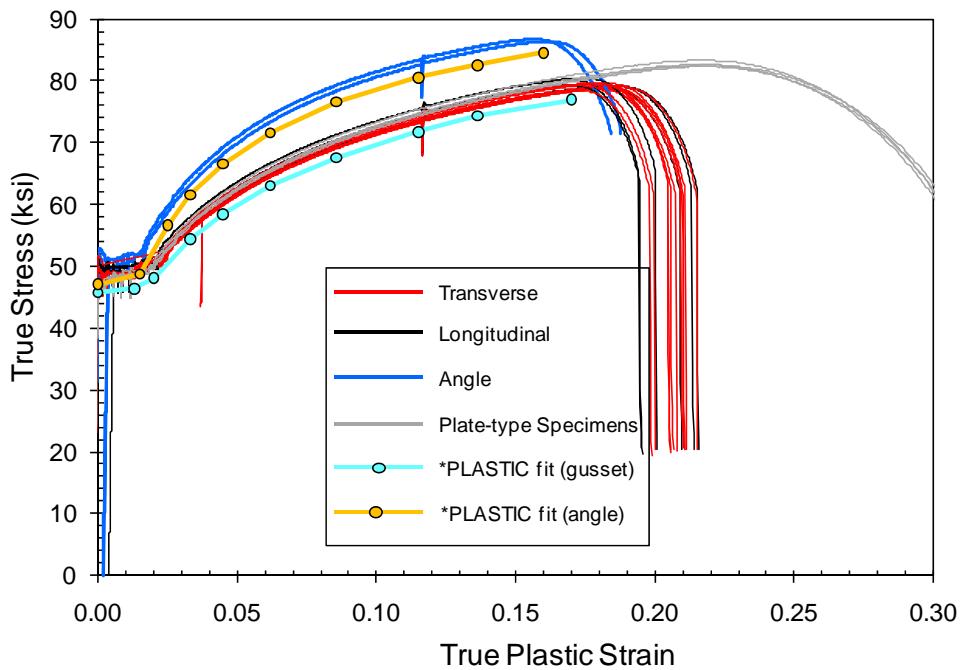


Figure D31. GP490LS3-2 coupon true stress/true plastic strain plots.

Table D16. *Abaqus *PLASTIC Input Data for Phase 1 Specimens*

| | 307SS3 | | 307LS3 | | 307SL3 | | 307SL4 | | 490SS3 | | 490LS3 | | 490LS-1 | |
|---------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|
| | True Stress (ksi) | True Plastic Strain |
| Line 1 | 36.38 | 0 | 48.20 | 0 | 46.65 | 0 | 33.16 | 0 | 46.42 | 0 | 45.62 | 0 | 46.42 | 0 |
| Line 2 | 37.38 | 0.0084 | 48.77 | 0.013 | 47.51 | 0.011 | 34.47 | 0.005 | 47.08 | 0.01 | 47.08 | 0.011 | 47.41 | 0.016 |
| Line 3 | 44.31 | 0.0178 | 50.77 | 0.0178 | 51.51 | 0.0178 | 42.97 | 0.018 | 50.78 | 0.0178 | 50.58 | 0.0178 | 50.91 | 0.025 |
| Line 4 | 49.86 | 0.0274 | 55.77 | 0.0274 | 55.51 | 0.0274 | 50.27 | 0.034 | 55.28 | 0.0274 | 55.08 | 0.0274 | 54.61 | 0.033 |
| Line 5 | 56.09 | 0.0435 | 61.07 | 0.0435 | 60.01 | 0.0435 | 54.47 | 0.046 | 60.28 | 0.0435 | 59.58 | 0.0435 | 58.71 | 0.045 |
| Line 6 | 60.87 | 0.0618 | 64.77 | 0.0618 | 64.01 | 0.0618 | 58.47 | 0.062 | 64.28 | 0.0618 | 63.58 | 0.0618 | 63.11 | 0.0618 |
| Line 7 | 65.02 | 0.0857 | 68.77 | 0.0857 | 67.51 | 0.0857 | 62.67 | 0.086 | 67.78 | 0.0857 | 67.08 | 0.0857 | 67.81 | 0.0857 |
| Line 8 | 68.41 | 0.1151 | 72.27 | 0.1151 | 71.01 | 0.1151 | 65.77 | 0.11 | 71.28 | 0.1151 | 70.08 | 0.1151 | 72.01 | 0.1151 |
| Line 9 | 70.26 | 0.1363 | 74.47 | 0.1363 | 72.51 | 0.1363 | 68.97 | 0.143 | 73.03 | 0.1363 | 72.08 | 0.1363 | 74.41 | 0.1363 |
| Line 10 | 36.38 | 0 | 75.77 | 0.155 | 74.01 | 0.155 | 70.97 | 0.17 | 74.28 | 0.155 | 73.08 | 0.155 | 76.41 | 0.165 |

Table D17. *Abaqus *PLASTIC Input Data for Phase 2 Specimens*

| | 490SS3-1 | | 490LS3-2 | | 307SS3-1 | | 307SS3-2 | | 307SS3-3 | | 307SS3-4 gusset | | 307SS3-4 shingle | |
|---------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|-------------------|---------------------|
| | True Stress (ksi) | True Plastic Strain |
| Line 1 | 46.01 | 0 | 45.74 | 0 | 47.22 | 0 | 47.81 | 0 | 37.94 | 0 | 37.97 | 0 | 46.25 | 0 |
| Line 2 | 46.49 | 0.01 | 46.37 | 0.013 | 47.57 | 0.012 | 48.74 | 0.012 | 38.77 | 0.008 | 38.25 | 0.008 | 47.46 | 0.02 |
| Line 3 | 48.49 | 0.022 | 48.07 | 0.02 | 53.27 | 0.022 | 54.24 | 0.022 | 47.02 | 0.022 | 46.75 | 0.022 | 50.96 | 0.025 |
| Line 4 | 53.99 | 0.033 | 54.37 | 0.033 | 57.27 | 0.033 | 58.24 | 0.033 | 52.52 | 0.033 | 51.75 | 0.033 | 54.46 | 0.033 |
| Line 5 | 58.29 | 0.045 | 58.47 | 0.045 | 60.77 | 0.045 | 61.74 | 0.045 | 56.52 | 0.045 | 55.75 | 0.045 | 58.46 | 0.045 |
| Line 6 | 62.99 | 0.0618 | 63.07 | 0.0618 | 64.27 | 0.062 | 65.24 | 0.062 | 60.52 | 0.062 | 60.00 | 0.062 | 62.96 | 0.0618 |
| Line 7 | 67.49 | 0.0857 | 67.57 | 0.0857 | 68.17 | 0.086 | 69.24 | 0.086 | 64.77 | 0.086 | 64.25 | 0.086 | 67.56 | 0.0857 |
| Line 8 | 71.69 | 0.1151 | 71.77 | 0.1151 | 70.87 | 0.11 | 72.24 | 0.11 | 67.77 | 0.11 | 67.25 | 0.11 | 71.76 | 0.1151 |
| Line 9 | 75.29 | 0.15 | 74.37 | 0.1363 | 73.37 | 0.136 | 74.84 | 0.136 | 70.52 | 0.136 | 70.25 | 0.136 | 74.66 | 0.145 |
| Line 10 | 76.99 | 0.18 | 76.97 | 0.17 | 74.77 | 0.155 | 75.74 | 0.155 | 72.27 | 0.165 | 71.75 | 0.155 | 76.46 | 0.175 |

A514 CONNECTION MEMBER MATERIAL

The five reusable connection members for the full-scale testing were constructed from A514 Grade B material in three plate sizes of $\frac{1}{2}$, $\frac{3}{4}$, and 1 inch thicknesses. Unfortunately, the fabricator was not able to provide extra $\frac{3}{4}$ inch material for characterization. From the remnants of the one inch thick plate, four transverse and two longitudinal coupons were made. The remnant of $\frac{1}{2}$ inch thick plate could not facilitate a transverse Plate-type coupon and only four longitudinal coupons were made.

The results from the tensile coupon testing of the 1 inch and $\frac{1}{2}$ inch thickness plate are shown in Tables D18 and D19 respectively. The plots of the engineering stress versus engineering strain for each plate thickness is represented in Figure D32 and Figure D33. The true stress versus plastic and associated curve fit needed in an Abaqus analysis are shown in Figure D34.

Table D18. *A514 Results (1 inch plate)*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|----------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| T1 | 29879 | 111.8 | 110.0 | 118.9 | 15 | 54 |
| T2 | 30462 | 112.1 | 110.0 | 119.0 | 15 | 55 |
| T3 | 30518 | 111.2 | 109.2 | 118.6 | 15 | 54 |
| T4 | 30054 | 109.7 | 107.5 | 117.3 | 15 | 55 |
| L1 | 30126 | 110.6 | 108.8 | 117.8 | 17 | 66 |
| L2 | 30654 | 110.0 | 108.2 | 117.3 | 17 | 66 |
| Average | 30282 | 110.9 | 108.9 | 118.1 | 16 | 58 |
| COV | 0.010 | 0.009 | 0.009 | 0.007 | 0.058 | 0.103 |

Table D19. *A514 Results (0.5 inch plate)*

| Specimen ID | Measured Modulus of Elasticity (ksi) | 0.2% Offset Yield Stress (ksi) | Static Yield Stress (ksi) | Tensile Strength (ksi) | Elongation (%) | Area Reduction (%) |
|----------------|--------------------------------------|--------------------------------|---------------------------|------------------------|----------------|--------------------|
| L1 | 27920 | 104.3 | 102.1 | 109.6 | 13 | 56 |
| L2 | 28069 | 104.3 | 102.0 | 109.0 | 13 | 55 |
| L3 | 27973 | 104.0 | 101.6 | 109.4 | 12 | 52 |
| L4 | 28210 | 103.7 | 101.4 | 109.0 | 12 | 53 |
| Average | 28043 | 104.1 | 101.8 | 109.3 | 12 | 54 |
| COV | 0.005 | 0.003 | 0.003 | 0.002 | 0.019 | 0.032 |

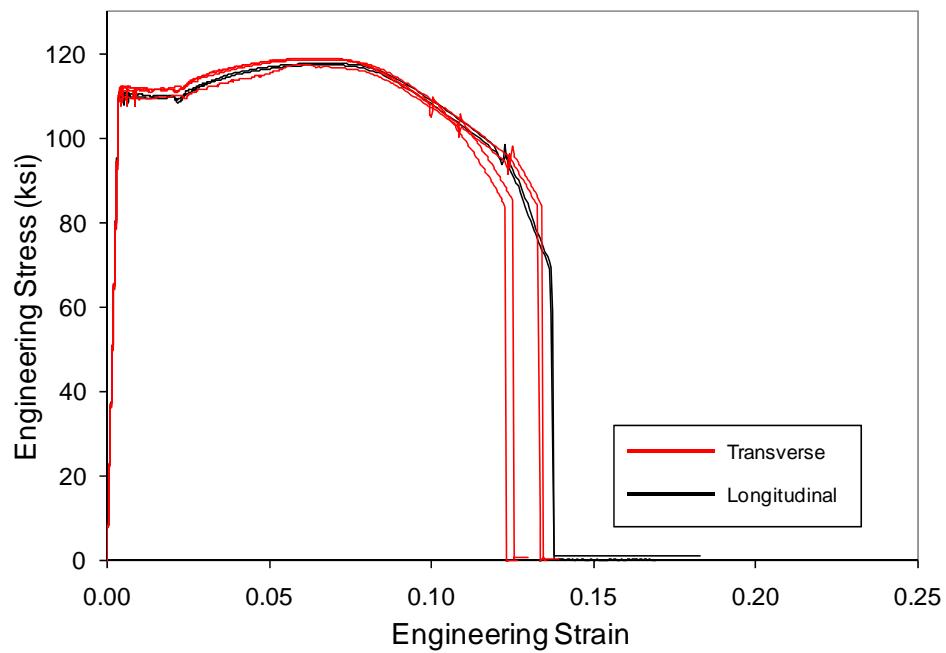


Figure D32. A514 Gr. B one inch thick coupon engineering stress/engineering strain plots.

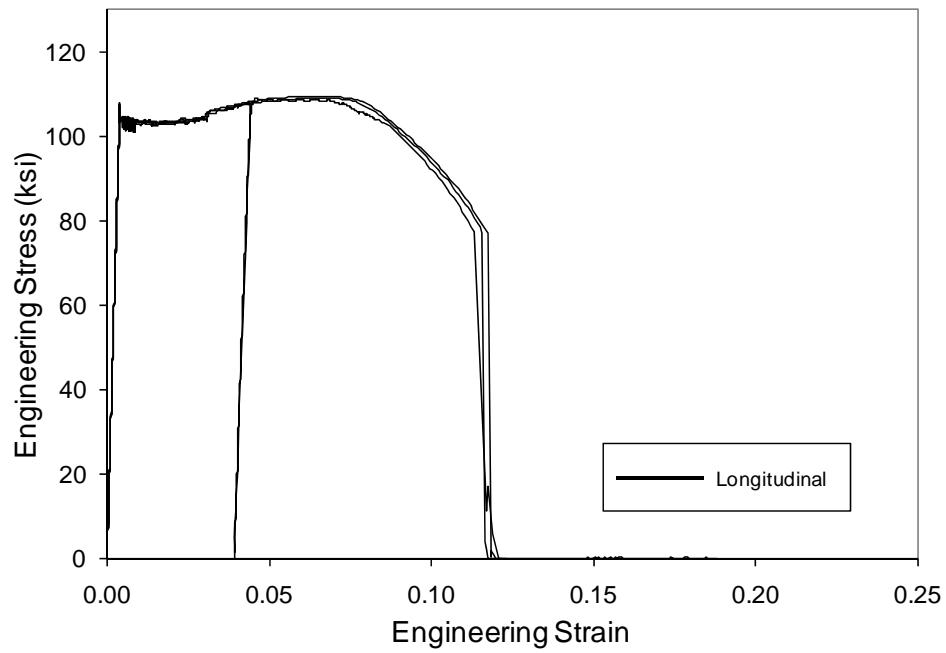


Figure D33. A514 Gr. B half inch thick coupon engineering stress/engineering strain plots.

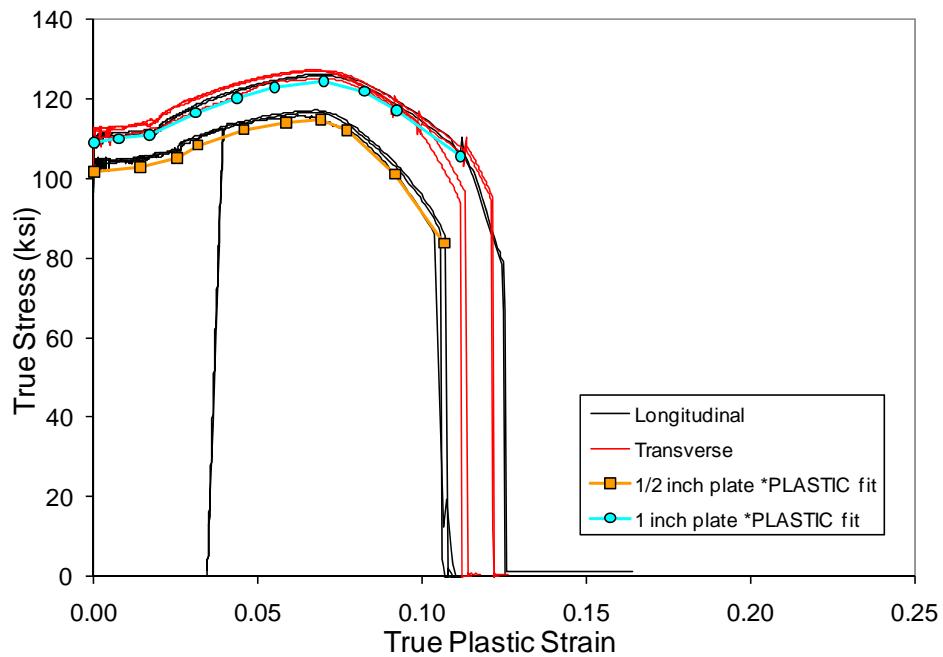


Figure D34. A514 Gr. B coupon true stress/true plastic strain plots.

MILL CERTIFICATIONS

Figures 35 through 38 show the mill certifications for the gusset plate received from the fabricator. A mill certification was never received for connection GP307SS3.

Severstal Sparrows Point, LLC
 QUALITY & CUSTOMER TECHNICAL SERVICES
REPORT OF TEST AND ANALYSIS

| | | | |
|---|--|--|------------------------------|
| REF. JOB CONTRACT NO. | | PURCHASE ORDER DATE 06/23/09 | PURCHASE ORDER NO. 090634 |
| VENDOR SEVERSTAL SPARROWS POINT, LLC SPARROWS POINT PLANT SPARROWS POINT, MARYLAND 21219 | | SHIPPER ID. 405-08616 | BILL ORDER NO. 41630476F |
| | | VEHICLE IDENTIFICATION | INVOICE NO. 405-08616 |
| | | | DATE SHIPPED 09/23/09 |
| SOLD TO | SHERWOOD INDUSTRIES INC CERTIFIED STEEL CO DIV 1333 BRUNSWICK PK STE 200 LAWRENCEVILLE NJ 08648 | SHIP TO SHERWOOD INDUSTRIES INC CERTIFIED STEEL CO DIV 199 WHITEHEAD ROAD TRENTON NJ 08610 | |

THICKNESS TYPE WIDTH LENGTH
 .365 M 60.00
 SPECIFICATION
 STEEL CHAR: HOT ROLLED STRUCTURAL STEEL DRY COILS-ME
 SPEC CODE : 36000 PSI MIN YIELD 58000-60000 PSI TENSILE ELONG 23% IN 2 "

| NOTE | QUANTITY | | MATERIAL Serial No. | Heat Number and/or Test Identification | Yield | Tensile Strength | ELONG | | Bend | |
|------|----------|----------|------------------------|--|----------|---------------------|--------|--------|------|-------|
| | Pieces | Packages | | | | | In. | in. | | |
| | 1 | | 46370 | 261043T | 402P7541 | 50,100 | 69,100 | 2 33.0 | | FRONT |

MELTED & MANUFACTURED IN THE USA

37643

NOTES

| Heat Number | CHEMICAL ANALYSIS | | | | | | | | | | |
|----------------|-------------------|-----|------|------|------|------|-------|-------|------|------|--|
| | C | Mn | P | S | Si | Cr | Ni | Mo | V | CB | |
| 402P7541 | .13 | .59 | .014 | .013 | .016 | .020 | .0.01 | .0.02 | .001 | .018 | |

I certify that the above results are true and correct.
 These test results contained in records maintained by
 severstal sparrow's plant and are in full compliance with the
 requirements of the specification cited. This test report
 cannot be altered and will be transmitted intact, with
 any subsequent third party test results, if required.

MANUFACTURER: QUALITY/CUSTOMER TECHNICAL SERVICES
 J. P. ECKSTEIN

DATE
09/30/09 R14:35 PAGE
PER

Figure D35. MTR for $\frac{3}{8}$ inch gusset material for specimen GP307LS3, GP307SL3, GP490SS3, GP490LS3.

ISG SPARROWS POINT, INC.
QUALITY & CUSTOMER TECHNICAL SERVICES
REPORT OF TEST AND ANALYSIS

| REF. JOB CONTRACT NO. | | PURCHASE ORDER DATE | PURCHASE ORDER NO. | | | | | | | |
|---|--|-------------------------|---|--|--------|------------------|-------|------|-------|------|
| | | 01/21/08 | 080057 | | | | | | | |
| VENDOR | | SHIPMENT NO. | MILL ORDER NO. | | | | | | | |
| ISG SPARROWS POINT INC SPARROWS POINT PLANT SPARROWS POINT, MARYLAND 21219 | | 405-05027 | 416 32411 J | | | | | | | |
| | | VERTICAL IDENTIFICATION | INVOICE NO. | | | | | | | |
| | | | 405-05027 | | | | | | | |
| | | | DATE SHIPPED | | | | | | | |
| | | | 04/17/08 | | | | | | | |
| SOLD TO | SHERWOOD INDUSTRIES INC CERTIFIED STEEL CO DIV 1333 BRUNSWICK PK STE 200 LAWRENCEVILLE NJ 08648 | | SHERWOOD INDUSTRIES INC CERTIFIED STEEL CO DIV 199 WHITEHEAD ROAD TRENTON NJ 08610 | | | | | | | |
| <small>ADDRESS</small> <small>TYPE</small> <small>WEIGHT</small> <small>LENGTH</small> 480 M 60.00 STEEL CHAR: HOT ROLLED STRUCTURAL STEEL DRY COILS-ME SPEC CODE : 36000 PSI MIN YIELD 58000-80000 PSI TENSILE ELONG 23% IN 2 " | | | | | | | | | | |
| <small>SPECIFICATIONS REQUESTED</small> | | | | | | | | | | |
| ROLL | QUANTITY | | GROSS WT. SERIAL NO. | Heat Number Product Identification | Yield | Tensile Strength | ELONG | | TEMP | TEST |
| | Pieces | Packages | | | | | IN | IN | | |
| | 1 | 47420 | 135619T | 412K9661 | 49,500 | 72,700 | 2 | 28.0 | FRONT | |
| MELTED & MANUFACTURED IN THE USA | | | | | | | | | | |

36920

NOTES

Material to be used for conversion to ASTM A36/ASME SA36. Statement added to test report 07/20/09.

| Heat Number | CHEMICAL ANALYSIS | | | | | | | | | | | CB |
|--|-------------------|-----|------|------|------|------|-------|----------------|------|------|------|----|
| | C | Mn | N | S | Si | Cr | Ni | Cr | Mo | V | | |
| 412K9661 | .22 | .85 | .011 | .014 | .009 | .040 | .0.02 | .0.02 | .002 | .002 | .001 | |
| I certify that the above results are true and correct. All of actual results contained in reports submitted by this laboratory, however, are in full compliance with the requirements of the specification ASTM A36. This test report cannot be altered and must be transmitted intact with any subsequent third party test reports, if required. | | | | | | | | | | | | |
| MANAGER, QUALITY CONTROL TECHNOLOGY SERVICES | | | | | | | DATE | 04/17/08 15:00 | | | | |
| J. P. ECKSTEIN | | | | | | | PER | | | | | |

Figure D36. MTR for $\frac{1}{2}$ inch gusset material for specimen GP307SL4.



Mill Test Report

Page 2

P.O. Box 279
Winton, NC 27986
(252) 356-3700

Issuing Date : 11/01/2010 Bill. No. : 276330
Vehicle No.: RICKY GARDNER 767
Specification: 0.3750" X 98.000" X 240.000"
ASTM A36-08/ABS Grade A/ASME SA36-03a/ASTM A109 Grade 36-Q9a

Marking : Load No. : 277813 Our Order No. : 8503601

Cust. Order No. : MA-23388
Ship To : INFRA-METALS CO.
600 MIDDLETON BLVD
SUITE D-100
410-355-9355
BALTIMORE, MD 21225
LANGHORNE PA 19047

Marking :

~~0507505-08~~

0507506-03

0507507-09

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|--|---|--|
| *** S E V E R S T A L *** | | 886603 |
| SEVERSTAL WARREN, INC. 1040 FINE AVE. SE WARREN, OHIO 44483-6328 | | |
| MELTED AND MANUFACTURED IN USA | | PURCHASE ORDER: 11/24/10 6304886-MID |
| C E R T I F I C A T E O F T E S T S | | DATE/INVOICE: 01/17/11 690663224 ORDER: 217 19 35235 03 |
| SOLD TO: NAMASCO CORP MIDDLETOWN 500 COLONIAL CENTER PARKWAY SUITE 500 ROSWELL GA 30076 | | SHIP TO: NAMASCO CORPORATION MIDDLETOWN 760 NEWFIELD STREET MIDDLETOWN CT 06457 |
| I certify that the properties of the items tested are true and accurate. Material was sampled, tested and found to be in accordance with the methods prescribed in the governing specifications. Subject material also conforms to the requirements of the governing specifications. This report shall not be reproduced except in full. | | D.L. Moore <i>D.L. Moore</i> |
| All tests are conducted in-house unless noted with an asterisk. | | |
| Item | Specification and Description | |
| 03:15:10 | | |
| HR SHEET SS + GRADE 36 TYPE 2 ASTM-A-1018-08A TYPE B SNA 36 SK NON-TEMPER ROLLED DRY NO OIL | | |
| 3 | .361M X 48.000 ME X COILS COIL WGT 38400MN/48000MX | |
| | HEAT-NO | COIL NUMBERS |
| | 2148194 | L110304 |
| | HEAT-NO | C MN P S SI CU NI CR |
| | 2148194 | .19 .75 .008 .005 .013 .03 .01 .03 MO SN AL V CB B TI ZR .01 .002 .058 .000 .000 .0000 .001 CA CE SB H N O .0030 .000 .000 .0040 |
| EU CONVERSION TO A36 - SHEETS/FLATNESS IMPORTANT NO COIL BREAKS | | |
| TI 01 C R/A FAX NBR: 866 598 1572 ATTENTION OF: | | |
| CHIC 25MX MN 1.35MX P 035MX S 040MX NI 20MX CR 15MX MO 06MX CU 20MX CB 008MX TI 025MX V 008MX | | |
| . | | |
| . | | |
| . | | |

NAMASCO

klöckner & co multi metal distribution

New Castle Division
20 Davidson Lane
New Castle DE 19720

NAMASCO CORPORATION
ATTENTION: KENT WINCHELL

DATE: February 18, 2011
PO # VERBAL

MATERIAL: CARBON STEEL

SPECIFICATION: ASTM A36-08 / ASME SA36-07 EDITION / ASTM A709-07 GR 36

SAMPLE DESIGNATION: 2 SAMPLES, # 618, SIZE 3/8 X 48.00, MILL. COIL ID. L110303
HEAT # 2148194

MECHANICAL PROPERTIES (per ASTM A370-09A)

| | # 1 HEAD | # 2 CENTER |
|-----------------------------------|----------|------------|
| WIDTH (inches): | .491 | .519 |
| THICKNESS (inches): | .373 | .374 |
| AREA (square inches): | .183 | .194 |
| YIELD STRENGTH (ksi) 0.2% offset: | 41.6 | 42.5 |
| TENSILE STRENGTH (ksi) | 65.8 | 65.9 |
| ELONGATION (%) IN 2" | 33.5 | 33.5 |

Based on the above testing this material meets the tensile requirements of ASTM A36-08 / ASME SA36-07 EDITION / ASTM A709-07 GR 36.


Daniel J. Iadisernia, Quality Manager

Figure D38. MTR for $\frac{3}{8}$ inch gusset material for specimen GP307SS3-3, GP307SS3-4, and Shingle plates.